

***Generation Interconnection
Feasibility Study Report***

For

***PJM Generation Interconnection Request
Queue Position AC1-162***

***Briery – Farmville 230kV
168.9 MW Capacity / 240 MW Energy***

May / 2017

Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

Preface

The intent of the Feasibility Study is to determine a plan, with high level estimated cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the IC. The IC may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the IC may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the Impact Study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by ITO, the costs may be included in the study.

General

The IC has proposed a solar generating facility located in Prince Edward County, VA. The installed facilities will have a total capability of 240 MW with 168.9 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is 10/01/2019.

This study does not imply an ITO commitment to this in-service date.

Point of Interconnection

AC1-162 will interconnect with the ITO transmission system via a new three breaker ring bus switching station that connects on the Briery DP – Farmville 230kV line #235.

Cost Summary

The AC1-162 project will be responsible for the following costs:

Description	Total Cost
Attachment Facilities	\$1,800,000
Direct Connection Network Upgrades	\$6,500,000
Non Direct Connection Network Upgrades	\$1,000,000
Total Costs	\$9,300,000

In addition, the AC1-162 project may be responsible for a contribution to the following costs:

Description	Total Cost
New System Upgrades	\$0
Previously Identified Upgrades	\$250,000
Total Costs	\$250,000

Cost allocations for these upgrades will be provided in the System Impact Study Report.

Note: PJM Open Access Transmission Tariff (OATT) section 217.3A outline cost allocation rules. The rules are further clarified in PJM Manual 14A Attachment B. For New System Upgrades, the cost allocation rule differ depending on whether the minimum amount of upgrades to resolve a single reliability criteria violation will cost less than \$5,000,000. For upgrades estimated to cost less than \$5,000,000 the allocation of costs will not occur outside of the Queue in which the need for the Network Upgrade was identified. Cost allocation within the Queue will be contingent each Queue projects Distribution Factor on the overloaded facility. For upgrades estimated to cost \$5,000,000 or greater the allocation of costs will start with the first Queue project to cause the need for the upgrade. Later queue projects will receive cost allocation contingent on their contribution to the violation and are allocated to the queues that have not closed less than 5 years following the execution of the first Interconnection Service Agreement which identifies the need for this upgrade.

Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost \$600,000.

Transmission: Build approximately 0.5 miles of 230 kV Line. Estimated Cost \$1,200,000

The estimated total cost of the Attachment Facilities is \$1,800,000. It is estimated to take 10-12 months to complete this work. These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase. These costs do not include CIAC Tax Gross-up. The single line is shown below in Attachment 1.

Direct Connection Cost Estimate

Substation: Build a three breaker 230 kV Ring Bus near Briery Substation with associated equipment. Estimated Cost \$6,500,000. It is estimated to take 24-30 months to complete this work.

Non-Direct Connection Cost Estimate

Transmission: Re-arrange existing lines 230 kV lines to interconnect the new AC1-162 Switching Station. Estimated Cost \$1,000,000.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

Contribution to Previously Identified System Reinforcements

Reinforcement: Midlothian – North Anna 500 kV line #576: replace wave trap at both North Anna Substations. This will increase emergency rating by 31% to 2403 MVA. Estimated cost \$250,000 and it is estimated to 12-16 months to engineer and construct.

Interconnection Customer Requirements

ITO's Facility Connection Requirements as posted on PJM's website

<http://www.pjm.com/~media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx>

An Interconnection Customer entering the New Services Queue on or after October 1, 2012 with a proposed new Customer Facility that has a Maximum Facility Output equal to or greater than 100 MW shall install and maintain, at its expense, phasor measurement units (PMUs). See

Section 8.5.3 of Appendix 2 to the Interconnection Service Agreement as well as section 4.3 of PJM Manual 14D for additional information.

Voltage Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for voltages and times as specified for the Eastern Interconnection in Attachment 1 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low voltage conditions, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Frequency Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for frequencies and times as specified in Attachment 2 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low frequency condition, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Reactive Power - The Generation Interconnection Customer shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading to 0.95 lagging measured at the generator's terminals.

Revenue Metering and SCADA Requirements

PJM Requirements

The IC will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

Network Impacts

The Queue Project AC1-162 was evaluated as a 240.0 MW (Capacity 168.2 MW) injection at the Briery 230kV substation in the ITO area. Project AC1-162 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AC1-162 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
557T574	CONTINGENCY '557T574' /* ELMONT OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /*ELMONT TO CHICKAHOMINY (LINE 557) OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1 /*CHICKAHOMINY 500-230 (TX#1) OPEN BRANCH FROM BUS 314911 TO BUS 314908 CKT 1 /*ELMONT TO LADYSMITH (LINE 574) END
H2T557	CONTINGENCY 'H2T557' /* ELMONT OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /*ELMONT TO CHICKAHOMINY (LINE 557) OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1 /*CHICKAHOMINY 500-230 (TX#1) OPEN BRANCH FROM BUS 314908 TO BUS 314218 CKT 2 /*ELMONT 500-230 (TX#2) END
LN 511	CONTINGENCY 'LN 511' OPEN BRANCH FROM BUS 314902 TO BUS 314936 CKT 1 /* 8CARSON 500.00 - 8RAWLINGS 500.00 END
LN 557	CONTINGENCY 'LN 557' OPEN BRANCH FROM BUS 314214 TO BUS 314903 CKT 1 /* 6CHCKAHM 230.00 - 8CHCKAHM 500.00 OPEN BRANCH FROM BUS 314903 TO BUS 314908 CKT 1 /* 8CHCKAHM 500.00 - 8ELMONT 500.00 END
LN 574	CONTINGENCY 'LN 574' OPEN BRANCH FROM BUS 314908 TO BUS 314911 CKT 1 /* 8ELMONT 500.00 - 8LDYSMTH 500.00 END

Summer Peak Analysis - 2020

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
1	LFFB	557T574	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	314914	314918	1	DC	118.08	118.83	LD	3144	54.76	1

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
2	N-1	LN 557	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	314914	314918	1	DC	108.84	109.45	ER	2442	33.24	
3	N-1	LN 574	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	314914	314918	1	DC	109.09	109.77	ER	2442	37.05	
4	LFFB	H2T557	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	314914	314918	1	DC	101.27	101.95	LD	3144	49.71	
5	N-1	LN 511	DVP - DVP	8ROGERS RD-8CARSON 500 kV line	314940	314902	1	DC	106.23	107.32	ER	3219	35.3	2

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

None

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
# 1 - 4	8MDLTHAN-8NO ANNA 500 kV line	Replace wave trap at both North Anna Substations. This will increase emergency rating by 31% to 3424 MVA. Estimated time 12 – 16 months.	Pending	\$250,000
# 5	8ROGERS RD-8CARSON 500 kV line	Rebuild of the Carson - Rogers Rd 500 kV circuit	b2744	
Total New Network Upgrades				\$250,000

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Circuit		Initial	Final	Type	MVA	
6	N-1	LN 574	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	314914	314918	1	DC	132.55	133.52	ER	2442	52.86
7	N-1	LN 511	DVP - DVP	8ROGERS RD-8CARSON 500 kV line	314940	314902	1	DC	107.65	109.22	ER	3219	50.37

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

ITO Analysis

ITO assessed the impact of the proposed Queue Project #AC1-162 interconnection of a 240 MW Energy (168.2 MW Capacity) injection into the ITO's Transmission System at a new interconnection switching station located between the Briery – Farmville section of Line #235, for compliance with NERC Reliability Criteria on ITO's Transmission System. The system was assessed using the summer 2020 RTEP case provided to ITO by PJM. When performing a generation analysis, ITO's main analysis will be load flow study results under single contingency (both normal and stressed system conditions). ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under normal and stressed system conditions. A full listing of ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C Contingency Conditions (Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO's Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating.

As part of its generation impact analysis, the ITO routinely evaluates the impact that a proposed new generation resource will have under maximum generation conditions, stress system conditions and import/export system conditions (greater than 20 MW). The results of these studies are discussed in more detail below.

Category B Analysis (Single Contingency):

1. System Normal – No deficiencies identified
2. Critical System Condition (No Surry 230 kV Unit) – No deficiencies identified.

Category C Analysis: (Multiple Facility Analysis)

1. Bus Fault - No deficiencies identified
2. Line Stuck Breaker - No deficiencies identified
3. Tower Line – No deficiencies identified

The import and export conditions into and out of the ITO System are evaluated with any new interconnection greater than 20 MW, any new facility that is interconnected with the ITO System should not significantly decrement FCITC between utilities. These studies will be performed during the System Impact Study.

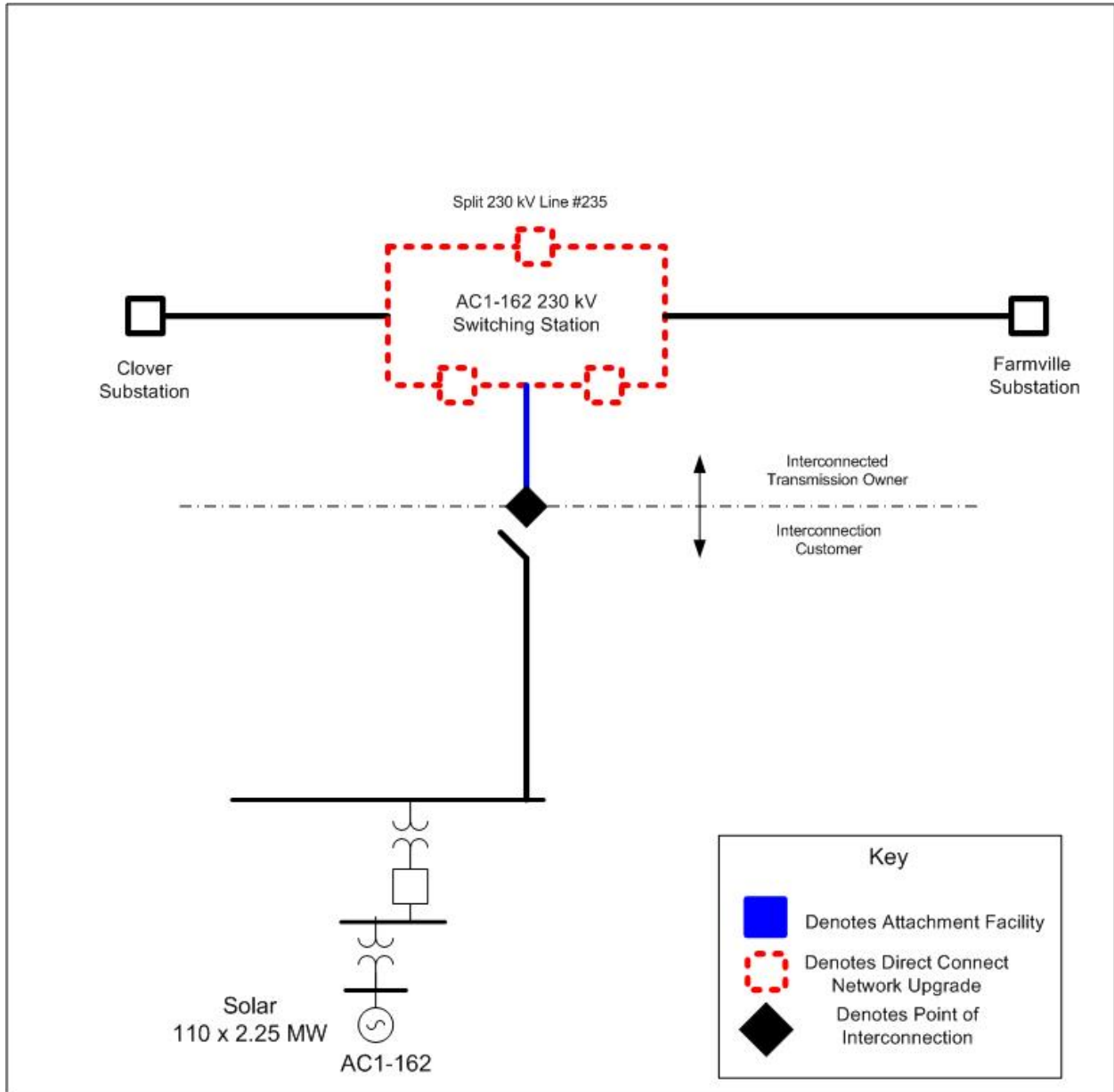
Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

Attachment 1.

System Configuration



Flowgate Appendices

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gauge other generators impact. When a flowgate is identified in multiple analysis the appendix is presented for only the analysis with the greatest overload.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DVP - DVP) The 8MDLTHAN-8NO ANNA 500 kV line (from bus 314914 to bus 314918 ckt 1) loads from 118.08% to 118.83% (**DC power flow**) of its load dump rating (3144 MVA) for the line fault with failed breaker contingency outage of '557T574'. This project contributes approximately 54.76 MW to the thermal violation.

CONTINGENCY '557T574' /* ELMONT
 OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /*ELMONT TO
 CHICKAHOMINY (LINE 557)
 OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1
 /*CHICKAHOMINY 500-230 (TX#1)
 OPEN BRANCH FROM BUS 314911 TO BUS 314908 CKT 1 /*ELMONT TO
 LADYSMITH (LINE 574)
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315102	1BRUNSWICKG1	16.69
315103	1BRUNSWICKG2	16.69
315104	1BRUNSWICKG3	16.69
315105	1BRUNSWICKS1	34.68
315108	1ELIZAR1	6.49
315109	1ELIZAR2	6.37
315110	1ELIZAR3	6.57
315073	1STONECA	10.33
315233	1SURRY 2	51.44
314784	1WEYRHSB	3.47
315091	1YORKTN2	48.12
314539	3UNCAMP	4.08
314541	3WATKINS	1.15
314189	6PAPERMILL	8.9
292791	U1-032 E	5.38
900672	V4-068 E	0.49
901082	W1-029E	79.39
907092	X1-038 E	10.2
913392	Y1-086 E	3.79
916042	Z1-036 E	77.93
916192	Z1-068 E	3.29
916301	Z1-086 C	101.56
916302	Z1-086 E	16.82

917122	Z2-027 E	1.83
917332	Z2-043 E	1.62
917342	Z2-044 E	0.89
LTF	Z2-067	29.61
917512	Z2-088 E OP1	12.51
917592	Z2-099 E	0.73
921092	AA1-049 C	4.23
921093	AA1-049 E	1.99
LTF	AA1-058	1.31
921162	AA1-063AC	13.84
921163	AA1-063AE	6.53
921172	AA1-064 C	15.11
921173	AA1-064 E	7.11
918512	AA1-065 E OP	7.32
921182	AA1-067 C	2.69
921183	AA1-067 E	1.15
918562	AA1-072 E	0.27
921532	AA1-132 C	13.05
921533	AA1-132 E	5.59
921542	AA1-133 C	17.45
921543	AA1-133 E	7.48
921552	AA1-134 C	17.03
921553	AA1-134 E	7.3
921562	AA1-135 C	14.94
921563	AA1-135 E	6.4
921572	AA1-138 C	16.71
921573	AA1-138 E	7.16
921582	AA1-139 C	26.18
921583	AA1-139 E	11.22
921752	AA2-053 C	14.05
921753	AA2-053 E	6.03
921762	AA2-057 C	11.13
921763	AA2-057 E	5.56
921772	AA2-059 C	4.05
921773	AA2-059 E	1.86
921862	AA2-068 C	3.53
921863	AA2-068 E	1.62
LTF	AA2-074	8.78
920022	AA2-086 E	0.39

921982	AA2-088 C	10.7
921983	AA2-088 E	17.46
922442	AA2-165 C	1.52
922443	AA2-165 E	0.73
922472	AA2-169 C	3.42
922473	AA2-169 E	1.57
922512	AA2-174 C	0.64
922513	AA2-174 E	0.7
922522	AA2-177 C	15.76
922523	AA2-177 E	6.75
922532	AA2-178 C	16.21
922533	AA2-178 E	6.95
922602	AB1-013 C	4.89
922603	AB1-013 E	32.74
922722	AB1-053 C	1.71
922723	AB1-053 E	0.96
922732	AB1-054 C	11.3
922733	AB1-054 E	5.56
922922	AB1-081 C OP	13.69
922923	AB1-081 E OP	5.87
923262	AB1-132 C OP	22.66
923263	AB1-132 E OP	9.71
923272	AB1-135 C OP	3.4
923273	AB1-135 E OP	1.46
923572	AB1-173 C OP	3.64
923573	AB1-173 E OP	1.7
923582	AB1-173AC OP	3.64
923583	AB1-173AE OP	1.7
923801	AB2-015 C OP	14.47
923802	AB2-015 E OP	11.87
923831	AB2-022 C	4.
923832	AB2-022 E	2.15
923841	AB2-024 C	3.32
923842	AB2-024 E	1.49
923851	AB2-025 C	4.08
923852	AB2-025 E	1.83
923861	AB2-026 C	3.73
923862	AB2-026 E	1.68
923911	AB2-031 C OP	3.61

923912	AB2-031 E OP	1.78
923941	AB2-035 C	0.52
923942	AB2-035 E	0.22
923981	AB2-039 C OP	13.92
923982	AB2-039 E OP	11.26
923991	AB2-040 C OP	11.87
923992	AB2-040 E OP	9.71
924021	AB2-043 C OP	4.48
924022	AB2-043 E OP	7.34
924071	AB2-051 C OP	240.18
924072	AB2-051 E OP	32.98
924151	AB2-059 C OP	16.13
924152	AB2-059 E OP	8.31
924161	AB2-060 C OP	12.55
924162	AB2-060 E OP	5.9
924241	AB2-068 OP	335.5
924301	AB2-077 C OP	2.84
924302	AB2-077 E OP	1.89
924311	AB2-078 C OP	2.84
924312	AB2-078 E OP	1.89
924321	AB2-079 C OP	2.84
924322	AB2-079 E OP	1.89
924381	AB2-087 C	0.93
924382	AB2-087 E	0.44
924391	AB2-088 C	0.67
924392	AB2-088 E	0.32
924401	AB2-089 C	3.21
924402	AB2-089 E	1.65
924411	AB2-090 C	5.64
924412	AB2-090 E	2.89
924491	AB2-098 C	0.9
924492	AB2-098 E	0.38
924501	AB2-099 C	0.97
924502	AB2-099 E	0.41
924511	AB2-100 C	18.51
924512	AB2-100 E	9.12
924761	AB2-128 C	15.86
924762	AB2-128 E	6.24
924811	AB2-134 C OP	20.21

924812	AB2-134 E OP	27.02
924931	AB2-147 C	4.13
924932	AB2-147 E	6.74
924941	AB2-149 C OP	5.71
924942	AB2-149 E OP	9.32
924951	AB2-150 C OP	4.13
924952	AB2-150 E OP	6.74
924961	AB2-152	4.04
925051	AB2-160 C OP	8.36
925052	AB2-160 E OP	13.63
925061	AB2-161 C OP	5.63
925062	AB2-161 E OP	9.18
925121	AB2-169 C OP	10.62
925122	AB2-169 E OP	9.53
925141	AB2-171 C OP	8.17
925142	AB2-171 E OP	13.33
925171	AB2-174 C OP	11.37
925172	AB2-174 E OP	10.29
925221	AB2-176 C	2.32
925222	AB2-176 E	0.99
925281	AB2-186 C	1.05
925282	AB2-186 E	0.45
925291	AB2-188 C OP	3.99
925292	AB2-188 E OP	1.79
925331	AB2-190 C	36.02
925332	AB2-190 E	9.01
925361	AC1-007 C OP	1.16
925362	AC1-007 E OP	1.89
925521	AC1-027 C	3.51
925522	AC1-027 E	2.01
925591	AC1-034 C OP	10.62
925592	AC1-034 E OP	8.01
925611	AC1-036 C	1.32
925612	AC1-036 E	2.15
925691	AC1-045 C	2.96
925692	AC1-045 E	1.62
925701	AC1-046 C	3.04
925702	AC1-046 E	1.66
925711	AC1-047 C	4.04

925712	ACI-047 E	2.22
925781	ACI-054 C OP	10.93
925782	ACI-054 E OP	5.04
925811	ACI-060	3.37
925821	ACI-061	0.06
925831	ACI-062	0.43
925841	ACI-063	0.52
925861	ACI-065 C	4.51
925862	ACI-065 E	7.36
926071	ACI-086 C	33.37
926072	ACI-086 E	15.19
926201	ACI-098 C	9.8
926202	ACI-098 E	5.84
926211	ACI-099 C	3.28
926212	ACI-099 E	1.93
926271	ACI-105 C OP	7.93
926272	ACI-105 E OP	3.95
926281	ACI-106	3.72
926291	ACI-107 OP	506.42
926661	ACI-147 C	3.95
926662	ACI-147 E	2.32
926741	ACI-159 C	238.32
926751	ACI-161 C OP	54.39
926752	ACI-161 E OP	23.22
926761	ACI-162 C	38.38
926762	ACI-162 E	16.38
926771	ACI-163 C	3.48
926772	ACI-163 E	1.63
926781	ACI-164 C OP	69.89
926782	ACI-164 E OP	31.4
927021	ACI-189 C	13.57
927022	ACI-189 E	6.76
927051	ACI-193 C	5.99
927052	ACI-193 E	9.77
927111	ACI-206 C OP	19.2
927112	ACI-206 E OP	9.08
927141	ACI-208 C	14.15
927142	ACI-208 E	6.28
927211	ACI-215 C	16.11

<i>927212</i>	<i>ACI-215 E</i>	<i>7.31</i>
<i>927221</i>	<i>ACI-216 C OP</i>	<i>15.42</i>
<i>927222</i>	<i>ACI-216 E OP</i>	<i>12.13</i>

Appendix 2

(DVP - DVP) The 8ROGERS RD-8CARSON 500 kV line (from bus 314940 to bus 314902 ckt 1) loads from 106.23% to 107.32% (**DC power flow**) of its emergency rating (3219 MVA) for the single line contingency outage of 'LN 511'. This project contributes approximately 35.3 MW to the thermal violation.

CONTINGENCY 'LN 511'

OPEN BRANCH FROM BUS 314902 TO BUS 314936 CKT 1 /* 8CARSON
500.00 - 8RAWLINGS 500.00
END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315102	1BRUNSWICKG1	29.8
315103	1BRUNSWICKG2	29.8
315104	1BRUNSWICKG3	29.8
315105	1BRUNSWICKS1	61.92
315150	1BUGGS 1	2.29
315151	1BUGGS 2	2.29
315153	1CLOVER1	34.1
315154	1CLOVER2	33.49
315159	1KERR 2	1.4
315164	1KERR 7	1.38
315266	1PLYWOOD A	2.17
314429	3JTRSVLE	0.4
916301	Z1-086 C	187.29
LTF	Z2-067	33.96
LTF	AA1-058	1.1
921172	AA1-064 C	23.98
LTF	AA2-074	9.55
924021	AB2-043 C OP	2.89
924161	AB2-060 C OP	8.29
LTF	AB2-075	4.49
LTF	AB2-076	5.21
924301	AB2-077 C OP	1.87
924311	AB2-078 C OP	1.87
924321	AB2-079 C OP	1.87
924411	AB2-090 C	3.64
925221	AB2-176 C	1.5
925611	AC1-036 C	0.87

<i>925831</i>	<i>ACI-062</i>	<i>0.29</i>
<i>925991</i>	<i>ACI-075 C</i>	<i>7.66</i>
<i>926021</i>	<i>ACI-080 C</i>	<i>2.56</i>
<i>926051</i>	<i>ACI-083 C OP</i>	<i>4.62</i>
<i>926271</i>	<i>ACI-105 C OP</i>	<i>8.21</i>
<i>926281</i>	<i>ACI-106</i>	<i>2.4</i>
<i>926461</i>	<i>ACI-117 C</i>	<i>0.92</i>
<i>926761</i>	<i>ACI-162 C</i>	<i>35.3</i>
<i>927211</i>	<i>ACI-215 C</i>	<i>10.5</i>
<i>927251</i>	<i>ACI-221 C</i>	<i>5.19</i>
<i>927261</i>	<i>ACI-222 C</i>	<i>7.51</i>