

***Generation Interconnection
Feasibility Study Report***

For

***PJM Generation Interconnection Request
Queue Position AD1-034***

***Sapony 115kV
44.9 MW Capacity / 74.9 MW Energy***

February 2018

Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

Preface

The intent of the Feasibility Study is to determine a plan, with high level estimated cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the IC. The IC may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the IC may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the Impact Study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by ITO, the costs may be included in the study.

General

The IC has proposed a solar generating facility located in Sussex County, Virginia. The installed facilities will have a total capability of 74.9 MW with 44.9 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is December 31, 2020. **This study does not imply an ITO commitment to this in-service date.**

Point of Interconnection

AD1-034 will interconnect with the ITO transmission system via one of the following Points of Interconnection:

Option 1: AD1-034 will interconnect into the existing Sapyony 115kV Substation

Option 2: AD1-034 will interconnect via a new three breaker ring bus switching station that connects the Sapyony – Clubhouse 230kV line.

Cost Summary

The AD1-034 project will be responsible for the following costs:

Description	Total Cost
Attachment Facilities	\$ 1,550,000
Direct Connection Network Upgrades	\$ 5,500,000
Non Direct Connection Network Upgrades	\$ 800,000
Total Costs	\$ 7,850,000

In addition, the AD1-034 project may be responsible for a contribution to the following costs:

Description	Total Cost
New System Upgrades	\$ 0
Previously Identified Upgrades	\$ 17,500,000
Total Costs	\$ 17,750,000

PJM Open Access Transmission Tariff (OATT) section 217.3A outlines cost allocation rules. The rules are further clarified in PJM Manual 14A Attachment B. For New System Upgrades, the cost allocation rule differ depending on whether the minimum amount of upgrades to resolve a single reliability criteria violation will cost less than \$5,000,000. For upgrades estimated to cost less than \$5,000,000 the allocation of costs will not occur outside of the Queue in which the need for the Network Upgrade was identified. Cost allocation within the Queue will be contingent each Queue projects Distribution Factor on the overloaded facility. For upgrades estimated to cost \$5,000,000 or greater the allocation of costs will start with the first Queue project to cause the need for the upgrade. Later queue projects will receive cost allocation contingent on their contribution to the violation and are allocated to the queues that have not closed less than 5 years following the execution of the first Interconnection Service Agreement which identifies the need for this upgrade.

The Feasibility Study is used to make a preliminary determination of the type and scope of Attachment Facilities, Local Upgrades, and Network Upgrades that will be necessary to accommodate the Interconnection Request and to provide the Interconnection Customer a preliminary estimate of the time that will be required to construct any necessary facilities and upgrades and the Interconnection Customer's cost responsibility. The System Impact Study provides refined and comprehensive estimates of cost responsibility and construction lead times for new facilities and system upgrades. Facilities Studies will include, commensurate with the degree of engineering specificity as provided in the Facilities Study Agreement, good faith estimates of the cost, determined in accordance with Section 217 of the Tariff,

- (a) to be charged to each affected New Service Customer for the Facilities and System Upgrades that are necessary to accommodate this queue project;

- (b) the time required to complete detailed design and construction of the facilities and upgrades; and
- (c) a description of any site-specific environmental issues or requirements that could reasonably be anticipated to affect the cost or time required to complete construction of such facilities and upgrades.

System Reinforcements

Violation #	Upgrade Description	Upgrade Cost
	*NEW SYSTEM REINFORCEMENTS	
	NONE	
	CONTRIBUTIONS TO PREVIOUS SYSTEM REINFORCEMENTS	
3	Replace the 500-230 kV transformer #1 increase its line rating to 1134 MVA (normal), 1203 MVA (emergency), and 1365 MVA (load dump). It is estimated to cost \$17,500,000 and 24-30 months to engineer and construct.	\$17,500,000
4,5	Line #259 Chesterfield – Basin 230 kV: reconductor 0.14 miles of 1109 ACAR with a conductor which will increase the line rating to approximately 706 MVA (normal), 706 MVA (emergency), and 812 MVA (load dump). It is estimated to cost \$250,000 and 15-18 months to engineer, permit and construct.	\$250,000
	Total Network Upgrades	\$17,750,000

***Note:**

For New System Reinforcements, only violations in which the AD1-034 overloads the facility are included in the table above. Costs for New System Reinforcement for which AD1-034 is not the first project to overload the facility are included for reference in the later part of this report. Cost allocation will be provided in the Impact Study.

Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost is \$550,000.

Transmission: Construct approximately one span of 115 kV Attachment line between the generation substation and the existing Sapony Substation. The estimated cost for this work is \$1,000,000.

The estimated total cost of the Attachment Facilities is \$1,550,000. It is estimated to take 18-24 months to complete this work upon execution of an Interconnection Construction Service Agreement (ICSA). These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase.

Direct Connection Cost Estimate

Substation: Add a three-breaker ring bus in the Sapony 115 kV Substation (interconnection substation). The estimated cost of this work scope is \$5,500,000. It is estimated to take 24-36 months to complete this work upon execution of an Interconnection Construction Service Agreement.

Non-Direct Network Upgrades:

Transmission: Install transmission structure in-line with transmission line to allow the proposed interconnection switching station to be interconnected with the transmission system. Estimated cost is \$800,000 and is estimated to take 24-30 months to complete.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

Interconnection Customer Requirements

ITO's Facility Connection Requirements as posted on PJM's website

<http://www.pjm.com/~media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx>

Voltage Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for voltages and times as specified for the Eastern Interconnection in Attachment 1 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low voltage conditions, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Frequency Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for frequencies and times as specified in Attachment 2 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low frequency condition, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Reactive Power - The Generation Interconnection Customer shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading to 0.95 lagging measured at the generator's terminals.

Revenue Metering and SCADA Requirements

PJM Requirements

The IC will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

Meteorological Data Reporting Requirement

The solar generation facility shall provide the Transmission Provider with site-specific meteorological data including:

- Temperature (degrees Fahrenheit)
- Atmospheric pressure (hectopascals)
- Irradiance
- Forced outage data

OPTION 1:

Network Impacts

PJM assessed the impact of the proposed Queue Project as an injection into the ITO's transmission system, for compliance with NERC Reliability Criteria. The system was assessed using the summer 2021 RTEP case. When performing analysis, ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under single contingency (normal and stressed system conditions). A full listing of the ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C Contingency Conditions (Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating. The results of these studies are discussed in more detail below.

The Queue Project AD1-034 was evaluated as a 74.0 MW (Capacity 44.9 MW) injection tapping Reams to Purdy 115kV line in the ITO area. Project AD1-034 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AD1-034 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
DVP_P1-2: LN 217	CONTINGENCY 'DVP_P1-2: LN 217'
	OPEN BRANCH FROM BUS 314225 TO BUS 314227 CKT 1 6CHARCTY 230.00 - 6LAKESD 230.00 /*
	OPEN BRANCH FROM BUS 314225 TO BUS 314228 CKT 1 6CHARCTY 230.00 - 6MESSER 230.00 /*
	OPEN BRANCH FROM BUS 314228 TO BUS 314287 CKT 1 6MESSER 230.00 - 6CHSTF B 230.00 /*
	OPEN BUS 314225 /* ISLAND

Contingency Name	Description
	OPEN BUS 314228 /* ISLAND END
DVP_P1-2: LN 557	CONTINGENCY 'DVP_P1-2: LN 557' OPEN BRANCH FROM BUS 314214 TO BUS 314903 CKT 1 /* 6CHCKAHM 230.00 - 8CHCKAHM 500.00 OPEN BRANCH FROM BUS 314903 TO BUS 314908 CKT 1 /* 8CHCKAHM 500.00 - 8ELMONT 500.00 END
DVP_P1-2: LN 563	CONTINGENCY 'DVP_P1-2: LN 563' OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /* 8CARSON 500.00 - 8MDLTHAN 500.00 END
DVP_P4-2: H2T557	CONTINGENCY 'DVP_P4-2: H2T557' /* ELMONT OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /*ELMONT TO CHICKAHOMINY (LINE 557) OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1 /*CHICKAHOMINY 500-230 (TX#1) OPEN BRANCH FROM BUS 314908 TO BUS 314218 CKT 2 /*ELMONT 500-230 (TX#2) END
DVP_P7-1: LN 212-240_D	CONTINGENCY 'DVP_P7-1: LN 212-240_D' OPEN BRANCH FROM BUS 925330 TO BUS 314538 CKT 2 /* AB2-190 TAP 230.00 - 6SURRY 230.00 OPEN BRANCH FROM BUS 924810 TO BUS 314538 CKT 1 /* AB2-134 TAP 230.00 - 6SURRY 230.00 END

Summer Peak Analysis – 2021

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None.

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

#	Contingency		Affected Area	Facility Description	Bus		Power Flow	Loading %		Rating		MW		
	Type	Name			From	To		Initial	Final	Type	MVA	Contribution	Ref	
1	DCTL	DVP_P7-1: LN 212- 240_D	DVP - DVP	6BERMUDA-6CHESTF A 230 kV line	314278	314286	1	DC	91.02	91.59	LD	549	6.89	1
2	DCTL	DVP_P7-1: LN 212- 240_D	DVP - DVP	6HOPEWLL-6BERMUDA 230 kV line	314303	314278	1	DC	91.02	91.59	LD	549	6.89	2

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

#	Contingency		Affected Area	Facility Description	Bus		Power Ckt	Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To			Initial	Final	Type	MVA		
3	LFFB	DVP_P4-2: H2T557	DVP - DVP	8ELMONT 500/230 kV transformer	314218	314908	1	DC	121.83	122.49	LD	1051	17.47	3
4	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	124.66	125.76	ER	449	4.93	4
5	N-1	DVP_P1-2: LN 217	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	118.43	119.73	ER	449	6.8	

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

#	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
1,2	6BERMUDA-6CHESTF A 230 kV line; 6HOPEWLL-6BERMUDA 230 kV line	Line #228 Hopewell – Bermuda – Chesterfield 230 kV: wreck and rebuild the line of 11 miles increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated to cost \$27,425,000 and 44-48 months to engineer, permit, and construct. A Va CPCN is required.	Pending	\$27,425,000
Total New Network Upgrades				\$27,425,000

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a %

#	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
3	8ELMONT 500/230 kV transformer	Elmont 500 – 230 kV Tx#1: replace the 500-230 kV transformer #1 increase its line rating to 1134 MVA (normal), 1203 MVA (emergency), and 1365 MVA (load dump). It is estimated to cost \$17,500,000 and 24-30 months to engineer and construct	Pending	\$17,500,000
4,5	6CHESTF B-6BASIN 230 kV line	Line #259 Chesterfield – Basin 230 kV: reconductor 0.14 miles of 1109 ACAR with a conductor which will increase the line rating to approximately 706 MVA (normal), 706 MVA (emergency), and 812 MVA (load dump). It is estimated to cost \$250,000 and 15-18 months to engineer, permit and construct.	Pending	\$250,000
Total New Network Upgrades				\$17,750,000

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA	
6	N-1	DVP_P1-2: LN 557	DVP - DVP	6CHARCTY-6LAKESIDE 230 kV line	314225	314227	1	DC	98.58	99.51	ER	984	11.01
7	N-1	DVP_P1-2: LN 217	DVP - DVP	6BERMUDA-6CHESTF A 230 kV line	314278	314286	1	DC	105.8	106.41	ER	449	6.5

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA	
8	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	148.68	150.51	ER	449	8.12
9	N-1	DVP_P1-2: LN 217	DVP - DVP	6HOPEWLL-6BERMUDA 230 kV line	314303	314278	1	DC	105.8	106.41	ER	449	6.5

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

OPTION 2

Network Impacts

PJM assessed the impact of the proposed Queue Project as an injection into the ITO's transmission system, for compliance with NERC Reliability Criteria. The system was assessed using the summer 2021 RTEP case. When performing analysis, ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under single contingency (normal and stressed system conditions). A full listing of the ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

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The Queue Project AD1-034 was evaluated as a 74.0 MW (Capacity 44.9 MW) injection tapping Sapony to Clubhouse 230kV line in the ITO area. Project AD1-034 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AD1-034 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
DVP_P1-2: LN 2056	CONTINGENCY 'DVP_P1-2: LN 2056' OPEN BRANCH FROM BUS 313845 TO BUS 314579 CKT 1 /* 6HATHAWAY 230.00 - 6HORNRTN 230.00 END

Contingency Name	Description
DVP_P1-2: LN 2058	CONTINGENCY 'DVP_P1-2: LN 2058' OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /* 6ROCKYMT230T230.00 - 6MORNSTR 230.00 END
DVP_P1-2: LN 2131A	CONTINGENCY 'DVP_P1-2: LN 2131A' OPEN BRANCH FROM BUS 314662 TO BUS 916040 CKT 1 /* 6S HERTFORD 230.00 - Z1-036 TAP 230.00 OPEN BRANCH FROM BUS 314651 TO BUS 314662 CKT 1 /* 6WINFALL 230.00 - 6S HERTFORD 230.00 OPEN BUS 314662 /* ISLAND END
DVP_P1-2: LN 2141	CONTINGENCY 'DVP_P1-2: LN 2141' OPEN BRANCH FROM BUS 314561 TO BUS 314583 CKT 1 /* 6CAROLNA 230.00 - 6LAKEVIEW 230.00 END
DVP_P1-2: LN 217	CONTINGENCY 'DVP_P1-2: LN 217' OPEN BRANCH FROM BUS 314225 TO BUS 314227 CKT 1 /* 6CHARCTY 230.00 - 6LAKESD 230.00 OPEN BRANCH FROM BUS 314225 TO BUS 314228 CKT 1 /* 6CHARCTY 230.00 - 6MESSER 230.00 OPEN BRANCH FROM BUS 314228 TO BUS 314287 CKT 1 /* 6MESSER 230.00 - 6CHSTF B 230.00 OPEN BUS 314225 /* ISLAND OPEN BUS 314228 /* ISLAND END
DVP_P1-2: LN 2181	CONTINGENCY 'DVP_P1-2: LN 2181' OPEN BUS 304226 /* ISLAND: 6PA- RMOUNT#4115.00 OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-RMOUNT#4230.00 - 6NASH 230.00 OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY 230.00 - 6NASH 230.00

Contingency Name	Description
	OPEN BUS 314591 /* ISLAND: 6NASH 230.00 END
DVP_P1-2: LN 238-A	CONTINGENCY 'DVP_P1-2: LN 238-A' OPEN BRANCH FROM BUS 314282 TO BUS 314435 CKT 1 /* 6CARSON 230.00 - 6SAPONY 230.00 OPEN BRANCH FROM BUS 314435 TO BUS 934070 CKT 1 /* 6SAPONY 230.00 - AD1-034 TAP 230.00 OPEN BUS 314435 /* ISLAND END
DVP_P1-2: LN 246	CONTINGENCY 'DVP_P1-2: LN 246' OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* 6SUFFOLK 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 6EARLEYS 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 6NUCO TP 230.00 - 6NUCOR 230.00 OPEN BUS 314575 /* ISLAND OPEN BUS 314590 /* ISLAND END
DVP_P1-2: LN 563	CONTINGENCY 'DVP_P1-2: LN 563' OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /* 8CARSON 500.00 - 8MDLTHAN 500.00 END
DVP_P4-2: 239T2141	CONTINGENCY 'DVP_P4-2: 239T2141' /* LAKEVIEW OPEN BRANCH FROM BUS 314583 TO BUS 314579 CKT 1 /* 239 OPEN BRANCH FROM BUS 314579 TO BUS 314605 CKT 1 /* 2057 OPEN BRANCH FROM BUS 314583 TO BUS 314561 CKT 1 /* 2141 END

Contingency Name	Description
DVP_P4-2: 246T2034	CONTINGENCY 'DVP_P4-2: 246T2034' /* EARLEYS OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314537 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR OPEN BRANCH FROM BUS 314569 TO BUS 933450 CKT 1 /* 2034 END
DVP_P4-2: 562T563	CONTINGENCY 'DVP_P4-2: 562T563' /*CARSON OPEN BRANCH FROM BUS 314902 TO BUS 314923 CKT 1 /* /*CARSON TO MIDLOTHIAN OPEN BRANCH FROM BUS 314914 TO BUS 314902 CKT 1 /* /*CARSON 500.00 - 8SEPTA 500.00 END
DVP_P4-2: H2T557	CONTINGENCY 'DVP_P4-2: H2T557' /* ELMONT OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /* /*ELMONT TO CHICKAHOMINY (LINE 557) OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1 /* /*CHICKAHOMINY 500-230 (TX#1) OPEN BRANCH FROM BUS 314908 TO BUS 314218 CKT 2 /* /*ELMONT 500-230 (TX#2) END
DVP_P7-1: LN 81-2056	CONTINGENCY 'DVP_P7-1: LN 81-2056' OPEN BRANCH FROM BUS 314559 TO BUS 314578 CKT 1 /* 3CAROLNA 115.00 - 3HORNRTN 115.00 OPEN BRANCH FROM BUS 314578 TO BUS 314598 CKT 1 /* 3HORNRTN 115.00 - 3ROAN DP 115.00 OPEN BRANCH FROM BUS 314598 TO BUS 314628 CKT 1 /* 3ROAN DP 115.00 - 3DARLINGT DP115.00 OPEN BUS 314578 /* ISLAND: 3HORNRTN 115.00 OPEN BUS 314598 /* ISLAND: 3ROAN DP 115.00

Contingency Name	Description
	OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-RMOUNT#4230.00 - 6NASH 230.00
	OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6MORNSTR 230.00 - 6NASH 230.00
	OPEN BRANCH FROM BUS 304226 TO BUS 304222 CKT 1 /* 6PA-RMOUNT#4230.00 - 6ROCKYMT230T
	OPEN BUS 304226 /* ISLAND
	OPEN BUS 314591 /* ISLAND: 6NASH 230.00
	END

Summer Peak Analysis – 2021

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

#	Contingency		Affected Area	Facility Description	Bus		Power Flow	Loading %		Rating		MW		
	Type	Name			From	To		Initial	Final	Type	MVA	Contribution	Ref	
1	N-1	DVP_P1-2: LN 563	DVP - DVP	6CARSON-6CHRL249 230 kV line	314282	314285	1	DC	95.52	96.99	ER	559	8.75	
2	N-1	DVP_P1-2: LN 2141	DVP - DVP	6HORNRTN-6MORNSTR 230 kV line	314579	313845	1	DC	98.37	99.89	ER	442	6.72	1

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None.

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

#	Contingency		Affected Area	Facility Description	Bus		Ckt	Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To			Initial	Final	Type	MVA		
3	DCTL	DVP_P7-1: LN 81-2056	DVP - CPL	6MORNSTR- 6ROCKYMT230T 230 kV line	313845	304222	1	DC	136.36	137.04	ER	374	5.65	2
4	LFFB	DVP_P4-2: H2T557	DVP - DVP	8ELMONT 500/230 kV transformer	314218	314908	1	DC	121.83	122.31	LD	1051	12.9	3
5	LFFB	DVP_P4-2: 562T563	DVP - DVP	6CARSON-6CHRL249 230 kV line	314282	314285	1	DC	107.6	109.72	LD	684	15.19	4
6	LFFB	DVP_P4-2: 562T563	DVP - DVP	6CHRL249-6LOCKS 230 kV line	314285	314316	1	DC	104.8	106.91	LD	684	15.19	5
7	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	124.7	125.84	ER	449	5.06	6
8	N-1	DVP_P1-2: LN 217	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	118.28	119.39	ER	449	6.09	
9	LFFB	DVP_P4-2: 239T2141	DVP - DVP	6CLUBHSE 230/115 kV transformer	314563	314562	1	DC	109.32	113.91	LD	209	9.59	7
10	N-1	DVP_P1-2: LN 2056	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	126.89	128.96	ER	375	7.78	8
11	N-1	DVP_P1-2: LN 238-A	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	116.77	121.9	ER	375	19.25	
12	LFFB	DVP_P4-2: 246T2034	DVP - DVP	AD1-034 TAP-6SAPONY 230 kV line	934070	314435	1	DC	122.32	130.38	LD	637	54.37	9

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA	
13	N-1	DVP_P1-2: LN 2181	DVP - CPLE	6MORNSTR- 6ROCKYMT230T 230 kV line	313845	304222	1	DC	136.35	137.04	ER	374	5.71
14	N-1	DVP_P1-2: LN 2058	DVP - DVP	6MORNSTR-6NASH 230 kV line	313845	314591	1	DC	120.89	121.47	ER	449	5.83
15	N-1	DVP_P1-2: LN 217	DVP - DVP	6BERMUDA-6CHESTF A 230 kV line	314278	314286	1	DC	106.41	107.01	ER	449	5.98
16	N-1	DVP_P1-2: LN 563	DVP - DVP	6CARSON-6CHRL249 230 kV line	314282	314285	1	DC	97.48	99.63	ER	559	14.42
17	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHRL249-6LOCKS 230 kV line	314285	314316	1	DC	94.07	96.21	ER	559	14.42
18	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHESTF B-6BASIN 230 kV line	314287	314276	1	DC	148.71	150.59	ER	449	8.34

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA	
19	N-1	DVP_P1-2: LN 217	DVP - DVP	6HOPEWLL-6BERMUDA 230 kV line	314303	314278	1	DC	106.41	107.01	ER	449	5.98
20	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6SAPONY-6CARSON 230 kV line	314435	314282	1	DC	111.65	119.54	ER	679	53.45
21	Non	Non	DVP - DVP	6SAPONY-6CARSON 230 kV line	314435	314282	1	DC	87.78	95.59	NR	679	53.23
22	N-1	DVP_P1-2: LN 238-A	DVP - DVP	6CAROLNA-6ROA VAL 230 kV line	314561	314599	1	DC	93.88	98.1	ER	548	23.11
23	N-1	DVP_P1-2: LN 238-A	DVP - DVP	6HORNRTN-6MORNSTR 230 kV line	314579	313845	1	DC	113.22	118.67	ER	442	24.04
24	N-1	DVP_P1-2: LN 2056	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	145.05	148.46	ER	375	12.82
25	Non	Non	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	104.82	107.15	NR	352	8.22
26	N-1	DVP_P1-2: LN 2058	DVP - CPL	6NASH-6PA-RMOUNT#4 230 kV line	314591	304226	1	DC	110.57	111.13	ER	470	5.83
27	N-1	DVP_P1-2: LN 238-A	DVP - DVP	6ROA VAL- 6NORTHAMPTON 230 kV line	314599	314266	1	DC	93.83	98.05	ER	548	23.11
28	N-1	DVP_P1-2: LN 238-A	DVP - DVP	6S HERTFORD- 6WINFALL 230 kV line	314662	314651	1	DC	91.36	92.44	ER	733	7.91
29	N-1	DVP_P1-2: LN 246	DVP - DVP	AD1-034 TAP-6SAPONY 230 kV line	934070	314435	1	DC	120.43	129.46	ER	599	53.86
30	Non	Non	DVP - DVP	AD1-034 TAP-6SAPONY 230 kV line	934070	314435	1	DC	102.5	110.38	NR	599	53.23

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. All New Service Queue Requests, through the end of the Queue under study, that are contributors to a flowgate will be listed in the Appendices. Please note that there may be contributors that are subsequently queued after the queue under study that are not listed in the Appendices. Although this information is not used "as is" for cost allocation purposes, it can be used to gage the impact of other projects/generators.

It should be noted the project/generator MW contributions presented in the body of the report and appendices sections are full contributions, whereas the loading percentages reported in the body of the report, those contributions take into consideration the commercial probability of each project as well as the ramping impact of "Adder" contributions.

OPTION 1

Appendix 1

(DVP - DVP) The 6BERMUDA-6CHESTF A 230 kV line (from bus 314278 to bus 314286 ckt 1) loads from 91.02% to 91.59% (**DC power flow**) of its load dump rating (549 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 212-240_D'. This project contributes approximately 6.89 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 212-240_D'

OPEN BRANCH FROM BUS 925330 TO BUS 314538 CKT 2 /* AB2-190 TAP
230.00 - 6SURRY 230.00

OPEN BRANCH FROM BUS 924810 TO BUS 314538 CKT 1 /* AB2-134 TAP
230.00 - 6SURRY 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315065	1CHESTF6	20.42
315074	1HOPCGN1	20.52
315075	1HOPCGN2	20.26
315077	1HOPHCF1	6.49
315078	1HOPHCF2	6.49
315079	1HOPHCF3	6.49
315080	1HOPHCF4	9.85
315076	1HOPPOLC	4.62
315073	1STONECA	17.02
314315	3LOCKS E	0.65
932581	AC2-078 C	2.99
932582	AC2-078 E	4.88
934011	AD1-025 C OI	41.76
934012	AD1-025 E OI	24.74
934071	AD1-034 C OI	4.18
934072	AD1-034 E OI	2.71

934571	AD1-082 C OI	3.55
934572	AD1-082 E OI	2.02
935161	AD1-151 C OI	39.9
935162	AD1-151 E OI	26.6
935211	AD1-156 C	1.39
935212	AD1-156 E	0.93
LTF	CARR	0.06
LTF	CBM-S1	0.9
LTF	CBM-S2	2.08
LTF	CBM-W1	1.53
LTF	CBM-W2	4.7
LTF	CIN	0.35
LTF	CPLE	0.68
LTF	G-007	0.26
LTF	IPL	0.22
LTF	LGEE	0.08
LTF	MEC	0.88
LTF	MECS	0.25
LTF	O-066	0.88
LTF	RENSSELAER	0.05
LTF	ROSETON	0.35
292791	U1-032 E	8.87
LTF	WEC	0.1
914231	Y2-077	2.61
924811	AB2-134 C OI	31.83
924812	AB2-134 E OI	31.3

<i>925051</i>	<i>AB2-160 C OI</i>	<i>2.83</i>
<i>925052</i>	<i>AB2-160 E OI</i>	<i>4.62</i>
<i>925061</i>	<i>AB2-161 C OI</i>	<i>1.56</i>
<i>925062</i>	<i>AB2-161 E OI</i>	<i>2.54</i>
<i>925331</i>	<i>AB2-190 C</i>	<i>49.65</i>
<i>925332</i>	<i>AB2-190 E</i>	<i>21.28</i>
<i>927221</i>	<i>AC1-216 C OI</i>	<i>24.29</i>
<i>927222</i>	<i>AC1-216 E OI</i>	<i>19.11</i>

Appendix 2

(DVP - DVP) The 6HOPEWLL-6BERMUDA 230 kV line (from bus 314303 to bus 314278 ckt 1) loads from 91.02% to 91.59% (**DC power flow**) of its load dump rating (549 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 212-240_D'. This project contributes approximately 6.89 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 212-240_D'

OPEN BRANCH FROM BUS 925330 TO BUS 314538 CKT 2 /* AB2-190 TAP
230.00 - 6SURRY 230.00

OPEN BRANCH FROM BUS 924810 TO BUS 314538 CKT 1 /* AB2-134 TAP
230.00 - 6SURRY 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315065	1CHESTF6	20.42
315074	1HOPCGN1	20.52
315075	1HOPCGN2	20.26
315077	1HOPHCF1	6.49
315078	1HOPHCF2	6.49
315079	1HOPHCF3	6.49
315080	1HOPHCF4	9.85
315076	1HOPPOLC	4.62
315073	1STONECA	17.02
314315	3LOCKS E	0.65
932581	AC2-078 C	2.99
932582	AC2-078 E	4.88
934011	AD1-025 C O1	41.76
934012	AD1-025 E O1	24.74
934071	AD1-034 C O1	4.18
934072	AD1-034 E O1	2.71
934571	AD1-082 C O1	3.55

934572	AD1-082 E OI	2.02
935161	AD1-151 C OI	39.9
935162	AD1-151 E OI	26.6
935211	AD1-156 C	1.39
935212	AD1-156 E	0.93
LTF	CARR	0.06
LTF	CBM-S1	0.9
LTF	CBM-S2	2.08
LTF	CBM-W1	1.53
LTF	CBM-W2	4.7
LTF	CIN	0.35
LTF	CPL	0.68
LTF	G-007	0.26
LTF	IPL	0.22
LTF	LGEE	0.08
LTF	MEC	0.88
LTF	MECS	0.25
LTF	O-066	0.88
LTF	RENSSELAER	0.05
LTF	ROSETON	0.35
292791	U1-032 E	8.87
LTF	WEC	0.1
914231	Y2-077	2.61
924811	AB2-134 C OI	31.83
924812	AB2-134 E OI	31.3
925051	AB2-160 C OI	2.83

<i>925052</i>	<i>AB2-160 E OI</i>	<i>4.62</i>
<i>925061</i>	<i>AB2-161 C OI</i>	<i>1.56</i>
<i>925062</i>	<i>AB2-161 E OI</i>	<i>2.54</i>
<i>925331</i>	<i>AB2-190 C</i>	<i>49.65</i>
<i>925332</i>	<i>AB2-190 E</i>	<i>21.28</i>
<i>927221</i>	<i>AC1-216 C OI</i>	<i>24.29</i>
<i>927222</i>	<i>AC1-216 E OI</i>	<i>19.11</i>

Appendix 3

(DVP - DVP) The 8ELMONT 500/230 kV transformer (from bus 314218 to bus 314908 ckt 1) loads from 121.83% to 122.49% (**DC power flow**) of its load dump rating (1051 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: H2T557'. This project contributes approximately 17.47 MW to the thermal violation.

```
CONTINGENCY 'DVP_P4-2: H2T557'                               /* ELMONT
  OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1           /*ELMONT TO
CHICKAHOMINY (LINE 557)
  OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1
/*CHICKAHOMINY 500-230 (TX#1)
  OPEN BRANCH FROM BUS 314908 TO BUS 314218 CKT 2           /*ELMONT 500-
230 (TX#2)
END
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315067	1DARBY 1	4.99
315068	1DARBY 2	4.99
315069	1DARBY 3	5.01
315070	1DARBY 4	5.01
315043	1FOUR RIVERA	6.63
315044	1FOUR RIVERB	5.13
315045	1FOUR RIVERC	6.63
315046	1FOUR RIVERD	5.13
315047	1FOUR RIVERE	5.13
315048	1FOUR RIVERF	6.63
315074	1HOPCGN1	11.28
315075	1HOPCGN2	11.14
315083	1SPRUNCA	14.95
315084	1SPRUNCB	14.95
315085	1SPRUNCC	11.08

315086	1SPRUNCD	11.08
315073	1STONECA	9.36
314566	3CRESWEL	2.11
314572	3EMPORIA	0.36
314315	3LOCKS E	1.65
314617	3TUNIS	0.71
314539	3UNCAMP	2.19
314541	3WATKINS	0.61
314620	6CASHIE	0.72
314229	6MT RD221	1.41
314236	6NRTHEST	0.37
314189	6PAPERMILL	8.82
314594	6PLYMOTH	0.73
314250	6ROCKVILLE	0.4
314256	6ROCKVILLE E	1.15
314648	6SUNBURY	0.81
314651	6WINFALL	1.59
932041	AC2-012 C	9.62
932042	AC2-012 E	15.7
932501	AC2-070 C	2.9
932502	AC2-070 E	1.2
932531	AC2-073 C	3.1
932532	AC2-073 E	1.56
932581	AC2-078 C	4.75
932582	AC2-078 E	7.75
932591	AC2-079 C	6.82

932592	AC2-079 E	11.13
932831	AC2-110 C	1.74
932832	AC2-110 E	2.84
933061	AC2-130	3.48
933071	AC2-131 1	2.36
933081	AC2-131 2	1.07
933111	AC2-132 1	1.24
933121	AC2-132 2	0.63
933261	AC2-137 C	3.16
933262	AC2-137 E	2.05
933271	AC2-138 C	0.87
933272	AC2-138 E	1.09
933291	AC2-141 C	27.16
933292	AC2-141 E	11.59
933451	AC2-158 C	4.63
933452	AC2-158 E	4.63
933471	AC2-161 C	2.47
933472	AC2-161 E	1.27
933481	AC2-162 C	4.17
933482	AC2-162 E	2.15
933711	AC2-194 C	0.98
933712	AC2-194 E	1.59
933731	AC2-196 C	1.66
933732	AC2-196 E	1.1
933991	AD1-023 C	11.29
933992	AD1-023 E	6.14

934011	AD1-025 C OI	20.82
934012	AD1-025 E OI	12.33
934061	AD1-033 C OI	6.96
934062	AD1-033 E OI	4.64
934071	AD1-034 C OI	10.6
934072	AD1-034 E OI	6.87
934141	AD1-041 C OI	6.74
934142	AD1-041 E OI	4.49
934191	AD1-046 C	4.71
934192	AD1-046 E	3.14
934201	AD1-047 C	6.75
934202	AD1-047 E	4.5
934211	AD1-048 C	3.82
934212	AD1-048 E	1.93
934391	AD1-063 C	2.1
934392	AD1-063 E	1.4
934521	AD1-076 C OI	46.88
934522	AD1-076 E OI	23.87
934571	AD1-082 C OI	8.27
934572	AD1-082 E OI	4.72
934781	AD1-105 C	8.08
934782	AD1-105 E	5.62
LTF	AD1-120	5.93
LTF	AD1-121	5.89
935111	AD1-144 C	1.68
935112	AD1-144 E	0.92

<i>935161</i>	<i>AD1-151 C OI</i>	<i>19.89</i>
<i>935162</i>	<i>AD1-151 E OI</i>	<i>13.26</i>
<i>935211</i>	<i>AD1-156 C</i>	<i>2.56</i>
<i>935212</i>	<i>AD1-156 E</i>	<i>1.71</i>
<i>LTF</i>	<i>CARR</i>	<i>0.67</i>
<i>LTF</i>	<i>CBM-S1</i>	<i>3.86</i>
<i>LTF</i>	<i>CBM-S2</i>	<i>13.84</i>
<i>LTF</i>	<i>CBM-W1</i>	<i>0.21</i>
<i>LTF</i>	<i>CBM-W2</i>	<i>17.91</i>
<i>LTF</i>	<i>CIN</i>	<i>0.13</i>
<i>LTF</i>	<i>CLIFTY</i>	<i>1.62</i>
<i>LTF</i>	<i>CPL</i>	<i>4.75</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.47</i>
<i>LTF</i>	<i>G-007</i>	<i>2.31</i>
<i>LTF</i>	<i>IPL</i>	<i>0.06</i>
<i>LTF</i>	<i>LGEE</i>	<i>0.05</i>
<i>LTF</i>	<i>MEC</i>	<i>1.99</i>
<i>LTF</i>	<i>O-066</i>	<i>7.73</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.53</i>
<i>LTF</i>	<i>ROSETON</i>	<i>3.84</i>
<i>292791</i>	<i>U1-032 E</i>	<i>4.87</i>
<i>297087</i>	<i>V2-040</i>	<i>0.28</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.26</i>
<i>901082</i>	<i>W1-029E</i>	<i>41.82</i>
<i>LTF</i>	<i>WEC</i>	<i>0.06</i>
<i>907092</i>	<i>X1-038 E</i>	<i>5.47</i>

913392	Y1-086 E	1.99
916042	Z1-036 E	40.84
916192	Z1-068 E	1.76
917122	Z2-027 E	0.96
917592	Z2-099 E	0.38
918492	AA1-063AE OP	3.35
918512	AA1-065 E OP	3.74
918691	AA1-083	1.16
919152	AA1-139 E	5.92
919211	AA1-145	19.79
919732	AA2-059 E	0.5
LTF	AA2-074	3.23
920022	AA2-086 E	0.21
920042	AA2-088 E	9.15
920691	AA2-178 C	8.43
920692	AA2-178 E	3.61
930051	AB1-013 C	2.54
930052	AB1-013 E	17.02
930121	AB1-027 C	0.87
930122	AB1-027 E	1.89
930861	AB1-132 C	11.78
930862	AB1-132 E	5.05
931231	AB1-173 C	1.9
931232	AB1-173 E	0.89
931241	AB1-173AC	1.9
931242	AB1-173AE	0.89

923801	AB2-015 C OI	7.73
923802	AB2-015 E OI	6.34
923831	AB2-022 C	2.1
923832	AB2-022 E	1.13
923842	AB2-024 E	1.49
923852	AB2-025 E	1.09
923862	AB2-026 E	0.88
923911	AB2-031 C OI	1.88
923912	AB2-031 E OI	0.93
923991	AB2-040 C OI	6.19
923992	AB2-040 E OI	5.06
924061	AB2-050	1.16
924071	AB2-051	128.86
924241	AB2-068 OI	177.95
924381	AB2-087 C	0.48
924382	AB2-087 E	0.22
924501	AB2-099 C	0.49
924502	AB2-099 E	0.21
924511	AB2-100 C	10.48
924512	AB2-100 E	5.16
924811	AB2-134 C OI	15.87
924812	AB2-134 E OI	15.6
925051	AB2-160 C OI	7.18
925052	AB2-160 E OI	11.71
925061	AB2-161 C OI	3.63
925062	AB2-161 E OI	5.92

925171	AB2-174 C O1	5.96
925172	AB2-174 E O1	5.39
925281	AB2-186 C	0.55
925282	AB2-186 E	0.24
925291	AB2-188 C O1	2.08
925292	AB2-188 E O1	0.93
925331	AB2-190 C	24.76
925332	AB2-190 E	10.61
925522	AC1-027 E	1.07
925692	AC1-045 E	0.92
925861	AC1-065 C	4.36
925862	AC1-065 E	7.11
926071	AC1-086 C	17.34
926072	AC1-086 E	7.89
926291	AC1-107	268.61
926411	AC1-112 C	0.68
926412	AC1-112 E	1.93
926441	AC1-115 C	1.01
926442	AC1-115 E	1.64
926472	AC1-118 E	1.07
926551	AC1-134	14.83
926662	AC1-147 E	1.25
926741	AC1-159	62.13
926751	AC1-161 C	27.16
926752	AC1-161 E	11.59
926771	AC1-163 C	1.63

<i>926772</i>	<i>ACI-163 E</i>	<i>0.76</i>
<i>926781</i>	<i>ACI-164 C</i>	<i>58.41</i>
<i>926782</i>	<i>ACI-164 E</i>	<i>26.24</i>
<i>927041</i>	<i>ACI-191 C</i>	<i>17.46</i>
<i>927042</i>	<i>ACI-191 E</i>	<i>8.7</i>
<i>927111</i>	<i>ACI-206 C</i>	<i>9.15</i>
<i>927112</i>	<i>ACI-206 E</i>	<i>4.32</i>
<i>927221</i>	<i>ACI-216 C O1</i>	<i>12.11</i>
<i>927222</i>	<i>ACI-216 E O1</i>	<i>9.53</i>

Appendix 4

(DVP - DVP) The 6CHESTF B-6BASIN 230 kV line (from bus 314287 to bus 314276 ckt 1) loads from 124.66% to 125.76% (**DC power flow**) of its emergency rating (449 MVA) for the single line contingency outage of 'DVP_P1-2: LN 563'. This project contributes approximately 4.93 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 563'

OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1

/* 8CARSON

500.00 - 8MDLTHAN 500.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315065	1CHESTF6	33.33
315131	1EDGECEMA	3.18
315132	1EDGECEMB	3.18
315139	1GASTONA	1.58
315141	1GASTONB	1.58
315119	1GRAVEL3	1.24
315120	1GRAVEL4	1.26
315121	1GRAVEL5	1.24
315122	1GRAVEL6	1.26
315117	1GRAVELC	0.43
315074	1HOPCGN1	5.63
315075	1HOPCGN2	5.56
315077	1HOPHCF1	1.78
315078	1HOPHCF2	1.78
315079	1HOPHCF3	1.78
315080	1HOPHCF4	2.7
315076	1HOPPOLC	1.27
315116	1SURRY 1	12.47

<i>314314</i>	<i>3LOCKS</i>	<i>0.06</i>
<i>314315</i>	<i>3LOCKS E</i>	<i>0.77</i>
<i>932041</i>	<i>AC2-012 C</i>	<i>3.21</i>
<i>932581</i>	<i>AC2-078 C</i>	<i>2.86</i>
<i>932591</i>	<i>AC2-079 C</i>	<i>3.07</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>3.22</i>
<i>932701</i>	<i>AC2-093 C</i>	<i>23.37</i>
<i>933451</i>	<i>AC2-158 C</i>	<i>1.94</i>
<i>933461</i>	<i>AC2-159 C</i>	<i>2.55</i>
<i>933471</i>	<i>AC2-161 C</i>	<i>0.89</i>
<i>933711</i>	<i>AC2-194 C</i>	<i>0.35</i>
<i>933731</i>	<i>AC2-196 C</i>	<i>0.55</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>4.54</i>
<i>934011</i>	<i>AD1-025 C OI</i>	<i>9.21</i>
<i>934041</i>	<i>AD1-029 C</i>	<i>3.98</i>
<i>934061</i>	<i>AD1-033 C OI</i>	<i>2.31</i>
<i>934071</i>	<i>AD1-034 C OI</i>	<i>4.93</i>
<i>934201</i>	<i>AD1-047 C</i>	<i>3.58</i>
<i>934331</i>	<i>AD1-057 C OI</i>	<i>3.86</i>
<i>934521</i>	<i>AD1-076 C OI</i>	<i>18.6</i>
<i>934571</i>	<i>AD1-082 C OI</i>	<i>4.27</i>
<i>935111</i>	<i>AD1-144 C</i>	<i>0.56</i>
<i>935161</i>	<i>AD1-151 C OI</i>	<i>8.8</i>
<i>935211</i>	<i>AD1-156 C</i>	<i>1.97</i>
<i>LTF</i>	<i>CARR</i>	<i>0.2</i>
<i>LTF</i>	<i>CBM-SI</i>	<i>3.34</i>

<i>LTF</i>	<i>CBM-S2</i>	<i>7.3</i>
<i>LTF</i>	<i>CBM-W1</i>	<i>6.1</i>
<i>LTF</i>	<i>CBM-W2</i>	<i>17.57</i>
<i>LTF</i>	<i>CIN</i>	<i>1.4</i>
<i>LTF</i>	<i>CPLE</i>	<i>2.35</i>
<i>LTF</i>	<i>IPL</i>	<i>0.89</i>
<i>LTF</i>	<i>LGEE</i>	<i>0.31</i>
<i>LTF</i>	<i>MEC</i>	<i>3.38</i>
<i>LTF</i>	<i>MECS</i>	<i>1.11</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.16</i>
<i>LTF</i>	<i>ROSETON</i>	<i>1.15</i>
<i>LTF</i>	<i>WEC</i>	<i>0.39</i>
<i>914231</i>	<i>Y2-077</i>	<i>0.72</i>
<i>LTF</i>	<i>AA2-074</i>	<i>1.6</i>
<i>920631</i>	<i>AA2-169 C</i>	<i>0.75</i>
<i>920691</i>	<i>AA2-178 C</i>	<i>3.22</i>
<i>930051</i>	<i>AB1-013 C</i>	<i>0.97</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>3.05</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>6.17</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>1.01</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>1.01</i>
<i>923801</i>	<i>AB2-015 C OI</i>	<i>3.22</i>
<i>923831</i>	<i>AB2-022 C</i>	<i>0.73</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.31</i>
<i>923911</i>	<i>AB2-031 C OI</i>	<i>1.</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.11</i>

923991	AB2-040 C OI	3.28
924071	AB2-051	42.84
924151	AB2-059 C OI	3.6
924381	AB2-087 C	0.21
924391	AB2-088 C	0.15
924491	AB2-098 C	0.19
924501	AB2-099 C	0.22
924511	AB2-100 C	6.19
924811	AB2-134 C OI	7.02
925051	AB2-160 C OI	3.33
925061	AB2-161 C OI	1.87
925121	AB2-169 C	2.2
925171	AB2-174 C OI	3.2
925281	AB2-186 C	0.2
925291	AB2-188 C OI	0.79
925331	AB2-190 C	10.95
925591	AC1-034 C	2.34
925821	AC1-061	< 0.01
926071	AC1-086 C	9.08
926201	AC1-098 C	2.26
926211	AC1-099 C	0.76
926741	AC1-159	20.65
926771	AC1-163 C	0.71
927021	AC1-189 C	2.92
927111	AC1-206 C	5.47
927141	AC1-208 C	3.41

<i>927221</i>	<i>ACI-216 C OI</i>	<i>5.36</i>
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OPTION 2

Appendix 1

(DVP - DVP) The 6HORNRTN-6MORNSTR 230 kV line (from bus 314579 to bus 313845 ckt 1) loads from 98.37% to 99.89% (**DC power flow**) of its emergency rating (442 MVA) for the single line contingency outage of 'DVP_P1-2: LN 2141'. This project contributes approximately 6.72 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 2141'

OPEN BRANCH FROM BUS 314561 TO BUS 314583 CKT 1

/* 6CAROLNA

230.00 - 6LAKEVEW 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315139	1GASTONA	9.67
315141	1GASTONB	9.67
315136	1ROSEMG1	7.63
315138	1ROSEMG2	3.58
315137	1ROSEMS1	4.73
314704	3LAWRENC	0.27
934043	AD1-029 BAT	8.06
934071	AD1-034 C O2	6.72
934201	AD1-047 C	4.21
935211	AD1-156 C	0.61
LTF	AMIL	0.32
LTF	BAYOU	1.71
LTF	BIG_CAJUN1	2.69
LTF	BIG_CAJUN2	5.42
LTF	BLUEG	1.68
LTF	CALDERWOOD	1.
LTF	CANNELTON	0.32
LTF	CATAWBA	0.98
LTF	CBM-N	< 0.01
LTF	CELEVELAND	2.79
LTF	CHEOAH	0.94
LTF	CHILHOWEE	0.33
LTF	CHOCTAW	1.83
LTF	CLIFTY	6.12
LTF	COTTONWOOD	6.68
LTF	DEARBORN	0.6
LTF	EDWARDS	0.52
LTF	ELMERSMITH	0.94
LTF	FARMERCITY	0.41
LTF	G-007A	0.68

<i>LTF</i>	<i>GIBSON</i>	<i>0.59</i>
<i>LTF</i>	<i>HAMLET</i>	<i>4.01</i>
<i>LTF</i>	<i>MORGAN</i>	<i>2.96</i>
<i>LTF</i>	<i>NEWTON</i>	<i>1.43</i>
<i>LTF</i>	<i>NYISO</i>	<i>0.04</i>
<i>LTF</i>	<i>O-066A</i>	<i>0.31</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>3.08</i>
<i>LTF</i>	<i>ROWAN</i>	<i>2.02</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.28</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.27</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.69</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.61</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.32</i>
<i>LTF</i>	<i>TVA</i>	<i>1.24</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>1.79</i>
<i>LTF</i>	<i>VFT</i>	<i>1.81</i>
<i>LTF</i>	<i>X1-078</i>	<i>0.53</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>37.6</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>1.18</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>1.18</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.38</i>
<i>923911</i>	<i>AB2-031 C O1</i>	<i>1.17</i>
<i>923991</i>	<i>AB2-040 C O1</i>	<i>3.85</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>17.83</i>
<i>925171</i>	<i>AB2-174 C O1</i>	<i>4.45</i>
<i>926071</i>	<i>AC1-086 C</i>	<i>55.37</i>
<i>927111</i>	<i>AC1-206 C</i>	<i>14.05</i>

Appendix 2

(DVP - CPLE) The 6MORNSTR-6ROCKYMT230T 230 kV line (from bus 313845 to bus 304222 ckt 1) loads from 136.36% to 137.04% (**DC power flow**) of its emergency rating (374 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 81-2056'. This project contributes approximately 5.65 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 81-2056'

OPEN BRANCH FROM BUS 314559 TO BUS 314578 CKT 1 /* 3CAROLNA
 115.00 - 3HORNRTN 115.00
 OPEN BRANCH FROM BUS 314578 TO BUS 314598 CKT 1 /* 3HORNRTN
 115.00 - 3ROAN DP 115.00
 OPEN BRANCH FROM BUS 314598 TO BUS 314628 CKT 1 /* 3ROAN DP
 115.00 - 3DARLINGT DP115.00
 OPEN BUS 314578 /* ISLAND: 3HORNRTN 115.00
 OPEN BUS 314598 /* ISLAND: 3ROAN DP 115.00
 OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-
 RMOUNT#4230.00 - 6NASH 230.00
 OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6MORNSTR
 230.00 - 6NASH 230.00
 OPEN BRANCH FROM BUS 304226 TO BUS 304222 CKT 1 /* 6PA-
 RMOUNT#4230.00 - 6ROCKYMT230T
 OPEN BUS 304226 /* ISLAND
 OPEN BUS 314591 /* ISLAND: 6NASH 230.00
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	24.8
315132	1EDGECEMB	24.8
315139	1GASTONA	4.01
315141	1GASTONB	4.01
315126	1ROARAP2	1.22
315128	1ROARAP4	1.18
315136	1ROSEMG1	3.36
315138	1ROSEMG2	1.57
315137	1ROSEMS1	2.09
314557	3BETHEL C	1.61
314554	3BTLEBRO	1.08
314566	3CRESWEL	1.09
314572	3EMPORIA	0.27
314582	3KELFORD	0.7
314603	3SCOT NK	3.23
314617	3TUNIS	0.55
314541	3WATKINS	0.33
314620	6CASHIE	0.49
314574	6EVERETS	1.81

314594	6PLYMOTH	0.44
932631	AC2-084 C	9.38
932632	AC2-084 E	4.62
933451	AC2-158 C	3.44
933452	AC2-158 E	3.44
933461	AC2-159 C	4.87
933462	AC2-159 E	4.87
933991	AD1-023 C	7.25
933992	AD1-023 E	3.95
934041	AD1-029 C	11.6
934042	AD1-029 E	7.65
934071	AD1-034 C O2	3.43
934072	AD1-034 E O2	2.22
934201	AD1-047 C	5.53
934202	AD1-047 E	3.69
934331	AD1-057 C O2	11.83
934332	AD1-057 E O2	6.31
934521	AD1-076 C O2	31.66
934522	AD1-076 E O2	16.12
LTF	AMIL	0.38
LTF	BAYOU	1.98
LTF	BIG_CAJUN1	3.12
LTF	BIG_CAJUN2	6.28
LTF	BLUEG	1.99
LTF	CALDERWOOD	1.17
LTF	CANNELTON	0.38
LTF	CARR	< 0.01
LTF	CATAWBA	1.14
LTF	CELEVELAND	3.25
LTF	CHEOAH	1.09
LTF	CHILHOWEE	0.38
LTF	CHOCTAW	2.13
LTF	CLIFTY	7.32
LTF	COTTONWOOD	7.76
LTF	DEARBORN	0.72
LTF	EDWARDS	0.61
LTF	ELMERSMITH	1.11
LTF	FARMERCITY	0.48
LTF	G-007A	0.76
LTF	GIBSON	0.69
LTF	HAMLET	4.52
LTF	MORGAN	3.43
LTF	NEWTON	1.68
LTF	O-066A	0.35
LTF	PRAIRIE	3.62

<i>LTF</i>	<i>ROWAN</i>	<i>2.4</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.32</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.32</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.82</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.73</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.38</i>
<i>LTF</i>	<i>TVA</i>	<i>1.45</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>2.08</i>
<i>900671</i>	<i>V4-068 C</i>	<i>0.07</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.18</i>
<i>LTF</i>	<i>VFT</i>	<i>2.03</i>
<i>LTF</i>	<i>X1-078</i>	<i>0.59</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.38</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.84</i>
<i>917341</i>	<i>Z2-044 C</i>	<i>0.34</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.75</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>1.68</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>6.74</i>
<i>917592</i>	<i>Z2-099 E</i>	<i>0.25</i>
<i>918411</i>	<i>AA1-050</i>	<i>1.41</i>
<i>918491</i>	<i>AA1-063AC OP</i>	<i>1.14</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>2.74</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>1.16</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>2.92</i>
<i>918531</i>	<i>AA1-067 C</i>	<i>0.25</i>
<i>918532</i>	<i>AA1-067 E</i>	<i>0.54</i>
<i>918561</i>	<i>AA1-072 C</i>	<i>0.06</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.14</i>
<i>919691</i>	<i>AA2-053 C</i>	<i>1.27</i>
<i>919692</i>	<i>AA2-053 E</i>	<i>2.78</i>
<i>919701</i>	<i>AA2-057 C</i>	<i>1.72</i>
<i>919702</i>	<i>AA2-057 E</i>	<i>4.39</i>
<i>919821</i>	<i>AA2-068 C</i>	<i>0.51</i>
<i>919822</i>	<i>AA2-068 E</i>	<i>1.19</i>
<i>920022</i>	<i>AA2-086 E</i>	<i>0.14</i>
<i>920042</i>	<i>AA2-088 E</i>	<i>5.93</i>
<i>920591</i>	<i>AA2-165 C</i>	<i>0.23</i>
<i>920592</i>	<i>AA2-165 E</i>	<i>0.58</i>
<i>920671</i>	<i>AA2-174 C</i>	<i>0.06</i>
<i>920672</i>	<i>AA2-174 E</i>	<i>0.32</i>
<i>920691</i>	<i>AA2-178 C</i>	<i>4.34</i>
<i>920692</i>	<i>AA2-178 E</i>	<i>1.86</i>
<i>930051</i>	<i>AB1-013 C</i>	<i>1.31</i>
<i>930052</i>	<i>AB1-013 E</i>	<i>8.77</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>14.55</i>

930402	ABI-081 E	6.23
930861	ABI-132 C	15.61
930862	ABI-132 E	6.69
931231	ABI-173 C	1.56
931232	ABI-173 E	0.73
931241	ABI-173AC	1.56
931242	ABI-173AE	0.73
923801	AB2-015 C O1	3.93
923802	AB2-015 E O1	3.23
923911	AB2-031 C O1	1.54
923912	AB2-031 E O1	0.76
923941	AB2-035 C	0.68
923942	AB2-035 E	0.29
923991	AB2-040 C O1	5.07
923992	AB2-040 E O1	4.15
924151	AB2-059 C O1	17.14
924152	AB2-059 E O1	8.83
924381	AB2-087 C	0.4
924382	AB2-087 E	0.19
924391	AB2-088 C	0.87
924392	AB2-088 E	0.42
924491	AB2-098 C	0.42
924492	AB2-098 E	0.18
924501	AB2-099 C	0.4
924502	AB2-099 E	0.17
924511	AB2-100 C	8.29
924512	AB2-100 E	4.08
925121	AB2-169 C	4.03
925122	AB2-169 E	3.62
925171	AB2-174 C O1	4.74
925172	AB2-174 E O1	4.29
925291	AB2-188 C O1	1.07
925292	AB2-188 E O1	0.48
925591	AC1-034 C	13.75
925592	AC1-034 E	10.37
926071	AC1-086 C	22.99
926072	AC1-086 E	10.47
926201	AC1-098 C	6.58
926202	AC1-098 E	3.92
926211	AC1-099 C	2.2
926212	AC1-099 E	1.29
926771	AC1-163 C	1.32
926772	AC1-163 E	0.62
927021	AC1-189 C	12.21
927022	AC1-189 E	6.08

<i>927111</i>	<i>ACI-206 C</i>	<i>6.69</i>
<i>927112</i>	<i>ACI-206 E</i>	<i>3.16</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>10.44</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>4.63</i>

Appendix 3

(DVP - DVP) The 8ELMONT 500/230 kV transformer (from bus 314218 to bus 314908 ckt 1) loads from 121.83% to 122.31% (**DC power flow**) of its load dump rating (1051 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: H2T557'. This project contributes approximately 12.9 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: H2T557' /* ELMONT
 OPEN BRANCH FROM BUS 314908 TO BUS 314903 CKT 1 /*ELMONT TO
 CHICKAHOMINY (LINE 557)
 OPEN BRANCH FROM BUS 314903 TO BUS 314214 CKT 1
 /*CHICKAHOMINY 500-230 (TX#1)
 OPEN BRANCH FROM BUS 314908 TO BUS 314218 CKT 2 /*ELMONT 500-
 230 (TX#2)
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315067	1DARBY 1	4.99
315068	1DARBY 2	4.99
315069	1DARBY 3	5.01
315070	1DARBY 4	5.01
315043	1FOUR RIVERA	6.63
315044	1FOUR RIVERB	5.13
315045	1FOUR RIVERC	6.63
315046	1FOUR RIVERD	5.13
315047	1FOUR RIVERE	5.13
315048	1FOUR RIVERF	6.63
315074	1HOPCGN1	11.28
315075	1HOPCGN2	11.14
315083	1SPRUNCA	14.95
315084	1SPRUNCB	14.95
315085	1SPRUNCC	11.08
315086	1SPRUNCD	11.08
315073	1STONECA	9.36
314566	3CRESWEL	2.11
314572	3EMPORIA	0.36
314315	3LOCKS E	1.65
314617	3TUNIS	0.71
314539	3UNCAMP	2.19
314541	3WATKINS	0.61
314620	6CASHIE	0.72
314229	6MT RD221	1.41
314236	6NRTHEST	0.37
314189	6PAPERMILL	8.82
314594	6PLYMOTH	0.73
314250	6ROCKVILLE	0.4

314256	6ROCKVILLE E	1.15
314648	6SUNBURY	0.81
314651	6WINFALL	1.59
932041	AC2-012 C	9.62
932042	AC2-012 E	15.7
932501	AC2-070 C	2.9
932502	AC2-070 E	1.2
932531	AC2-073 C	3.1
932532	AC2-073 E	1.56
932581	AC2-078 C	4.75
932582	AC2-078 E	7.75
932591	AC2-079 C	6.82
932592	AC2-079 E	11.13
932831	AC2-110 C	1.74
932832	AC2-110 E	2.84
933061	AC2-130	3.48
933071	AC2-131 1	2.36
933081	AC2-131 2	1.07
933111	AC2-132 1	1.24
933121	AC2-132 2	0.63
933261	AC2-137 C	3.16
933262	AC2-137 E	2.05
933271	AC2-138 C	0.87
933272	AC2-138 E	1.09
933291	AC2-141 C	27.16
933292	AC2-141 E	11.59
933451	AC2-158 C	4.63
933452	AC2-158 E	4.63
933471	AC2-161 C	2.47
933472	AC2-161 E	1.27
933481	AC2-162 C	4.17
933482	AC2-162 E	2.15
933711	AC2-194 C	0.98
933712	AC2-194 E	1.59
933731	AC2-196 C	1.66
933732	AC2-196 E	1.1
933991	AD1-023 C	11.29
933992	AD1-023 E	6.14
934011	AD1-025 C O2	20.82
934012	AD1-025 E O2	12.33
934061	AD1-033 C O2	6.97
934062	AD1-033 E O2	4.65
934071	AD1-034 C O2	7.83
934072	AD1-034 E O2	5.07
934141	AD1-041 C O2	7.07

934142	AD1-041 E O2	4.71
934191	AD1-046 C	4.71
934192	AD1-046 E	3.14
934201	AD1-047 C	6.75
934202	AD1-047 E	4.5
934211	AD1-048 C	3.82
934212	AD1-048 E	1.93
934391	AD1-063 C	2.1
934392	AD1-063 E	1.4
934521	AD1-076 C O2	44.5
934522	AD1-076 E O2	22.66
934571	AD1-082 C O2	8.78
934572	AD1-082 E O2	5.01
934781	AD1-105 C	8.08
934782	AD1-105 E	5.62
LTF	AD1-120	5.93
LTF	AD1-121	5.89
935111	AD1-144 C	1.68
935112	AD1-144 E	0.92
935161	AD1-151 C O2	15.11
935162	AD1-151 E O2	10.07
935211	AD1-156 C	2.56
935212	AD1-156 E	1.71
LTF	CARR	0.67
LTF	CBM-S1	3.86
LTF	CBM-S2	13.84
LTF	CBM-W1	0.21
LTF	CBM-W2	17.92
LTF	CIN	0.13
LTF	CLIFTY	1.61
LTF	CPL	4.75
LTF	DEARBORN	0.47
LTF	G-007	2.31
LTF	IPL	0.06
LTF	LGEE	0.05
LTF	MEC	1.99
LTF	O-066	7.73
LTF	RENSSELAER	0.53
LTF	ROSETON	3.84
292791	U1-032 E	4.87
297087	V2-040	0.28
900672	V4-068 E	0.26
901082	W1-029E	41.82
LTF	WEC	0.06
907092	X1-038 E	5.47

913392	Y1-086 E	1.99
916042	Z1-036 E	40.84
916192	Z1-068 E	1.76
917122	Z2-027 E	0.96
917592	Z2-099 E	0.38
918492	AA1-063AE OP	3.35
918512	AA1-065 E OP	3.74
918691	AA1-083	1.16
919152	AA1-139 E	5.92
919211	AA1-145	19.79
919732	AA2-059 E	0.5
LTF	AA2-074	3.23
920022	AA2-086 E	0.21
920042	AA2-088 E	9.15
920691	AA2-178 C	8.43
920692	AA2-178 E	3.61
930051	AB1-013 C	2.54
930052	AB1-013 E	17.02
930121	AB1-027 C	0.87
930122	AB1-027 E	1.89
930861	AB1-132 C	11.78
930862	AB1-132 E	5.05
931231	AB1-173 C	1.9
931232	AB1-173 E	0.89
931241	AB1-173AC	1.9
931242	AB1-173AE	0.89
923801	AB2-015 C O1	7.73
923802	AB2-015 E O1	6.34
923831	AB2-022 C	2.1
923832	AB2-022 E	1.13
923842	AB2-024 E	1.49
923852	AB2-025 E	1.09
923862	AB2-026 E	0.88
923911	AB2-031 C O1	1.88
923912	AB2-031 E O1	0.93
923991	AB2-040 C O1	6.19
923992	AB2-040 E O1	5.06
924061	AB2-050	1.16
924071	AB2-051	128.86
924241	AB2-068 O1	177.95
924381	AB2-087 C	0.48
924382	AB2-087 E	0.22
924501	AB2-099 C	0.49
924502	AB2-099 E	0.21
924511	AB2-100 C	10.48

924512	AB2-100 E	5.16
924811	AB2-134 C O1	15.87
924812	AB2-134 E O1	15.6
925051	AB2-160 C O1	7.18
925052	AB2-160 E O1	11.71
925061	AB2-161 C O1	3.63
925062	AB2-161 E O1	5.92
925171	AB2-174 C O1	5.96
925172	AB2-174 E O1	5.39
925281	AB2-186 C	0.55
925282	AB2-186 E	0.24
925291	AB2-188 C O1	2.08
925292	AB2-188 E O1	0.93
925331	AB2-190 C	24.76
925332	AB2-190 E	10.61
925522	AC1-027 E	1.07
925692	AC1-045 E	0.92
925861	AC1-065 C	4.36
925862	AC1-065 E	7.11
926071	AC1-086 C	17.34
926072	AC1-086 E	7.89
926291	AC1-107	268.61
926411	AC1-112 C	0.68
926412	AC1-112 E	1.93
926441	AC1-115 C	1.01
926442	AC1-115 E	1.64
926472	AC1-118 E	1.07
926551	AC1-134	14.83
926662	AC1-147 E	1.25
926741	AC1-159	62.13
926751	AC1-161 C	27.16
926752	AC1-161 E	11.59
926771	AC1-163 C	1.63
926772	AC1-163 E	0.76
926781	AC1-164 C	58.41
926782	AC1-164 E	26.24
927041	AC1-191 C	17.46
927042	AC1-191 E	8.7
927111	AC1-206 C	9.15
927112	AC1-206 E	4.32
927221	AC1-216 C O1	12.11
927222	AC1-216 E O1	9.53

Appendix 4

(DVP - DVP) The 6CARSON-6CHRL249 230 kV line (from bus 314282 to bus 314285 ckt 1) loads from 107.6% to 109.72% (**DC power flow**) of its load dump rating (684 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 562T563'. This project contributes approximately 15.19 MW to the thermal violation.

```
CONTINGENCY 'DVP_P4-2: 562T563'                /*CARSON
  OPEN BRANCH FROM BUS 314902 TO BUS 314923 CKT 1  /*CARSON TO
MIDLOTHIAN
  OPEN BRANCH FROM BUS 314914 TO BUS 314902 CKT 1  /*CARSON 500.00
- 8SEPTA 500.00
END
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315105	1BRUNSWICKSI	11.25
315131	1EDGECMA	4.76
315132	1EDGECMB	4.76
315139	1GASTONA	2.46
315141	1GASTONB	2.46
315136	1ROSEMG1	1.7
315138	1ROSEMG2	0.8
315137	1ROSEMS1	1.06
315073	1STONECA	-2.58
314557	3BETHELC	0.39
314554	3BTLEBRO	0.41
314572	3EMPORIA	0.33
314578	3HORNRTN	1.92
314582	3KELFORD	0.39
314704	3LAWRENC	0.28
314603	3SCOT NK	1.62
314617	3TUNIS	0.36
314541	3WATKINS	0.24
314620	6CASHIE	0.31
314574	6EVERETS	1.06
932631	AC2-084 C	4.46
932632	AC2-084 E	2.2
932701	AC2-093 C	40.58
932702	AC2-093 E	23.21
932761	AC2-100 C	2.16
932762	AC2-100 E	1.05
933451	AC2-158 C	2.15
933452	AC2-158 E	2.15
933461	AC2-159 C	3.44
933462	AC2-159 E	3.44
933991	AD1-023 C	4.58

933992	AD1-023 E	2.49
934041	AD1-029 C	5.52
934042	AD1-029 E	3.64
934071	AD1-034 C O2	9.22
934072	AD1-034 E O2	5.97
934201	AD1-047 C	5.74
934202	AD1-047 E	3.83
934231	AD1-050 C	2.37
934232	AD1-050 E	1.3
934311	AD1-055 C	1.03
934312	AD1-055 E	0.27
934331	AD1-057 C O2	5.2
934332	AD1-057 E O2	2.77
934341	AD1-058 C	2.35
934342	AD1-058 E	0.6
934521	AD1-076 C O2	19.48
934522	AD1-076 E O2	9.92
934611	AD1-087 C O2	3.75
934612	AD1-087 E O2	1.75
934621	AD1-088 C O2	6.62
934622	AD1-088 E O2	3.11
LTF	AD1-120	5.26
LTF	AD1-121	5.24
934911	AD1-123 C	0.45
934912	AD1-123 E	0.23
934991	AD1-131 C	0.77
934992	AD1-131 E	0.51
935171	AD1-152 C O2	3.36
935172	AD1-152 E O2	2.24
935211	AD1-156 C	1.
935212	AD1-156 E	0.67
LTF	CARR	0.18
LTF	CBM-S1	6.32
LTF	CBM-S2	12.36
LTF	CBM-W1	13.64
LTF	CBM-W2	33.99
LTF	CIN	3.08
LTF	CPLE	3.87
LTF	G-007	1.04
LTF	IPL	1.96
LTF	LGEE	0.67
LTF	MEC	6.97
LTF	MECS	3.01
LTF	O-066	3.47
LTF	RENSSELAER	0.14

<i>LTF</i>	<i>ROSETON</i>	<i>1.04</i>
<i>292791</i>	<i>U1-032 E</i>	<i>-1.34</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.13</i>
<i>LTF</i>	<i>WEC</i>	<i>0.84</i>
<i>916301</i>	<i>Z1-086 C</i>	<i>33.</i>
<i>916302</i>	<i>Z1-086 E</i>	<i>5.26</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.46</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.3</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>1.84</i>
<i>917592</i>	<i>Z2-099 E</i>	<i>0.18</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>2.09</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>1.82</i>
<i>918532</i>	<i>AA1-067 E</i>	<i>0.32</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.08</i>
<i>919692</i>	<i>AA2-053 E</i>	<i>2.08</i>
<i>919702</i>	<i>AA2-057 E</i>	<i>1.84</i>
<i>919822</i>	<i>AA2-068 E</i>	<i>0.54</i>
<i>LTF</i>	<i>AA2-074</i>	<i>2.63</i>
<i>920022</i>	<i>AA2-086 E</i>	<i>0.1</i>
<i>920042</i>	<i>AA2-088 E</i>	<i>4.33</i>
<i>920592</i>	<i>AA2-165 E</i>	<i>0.24</i>
<i>920631</i>	<i>AA2-169 C</i>	<i>1.18</i>
<i>920632</i>	<i>AA2-169 E</i>	<i>0.54</i>
<i>920672</i>	<i>AA2-174 E</i>	<i>0.24</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>4.55</i>
<i>930402</i>	<i>AB1-081 E</i>	<i>1.95</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>9.57</i>
<i>930862</i>	<i>AB1-132 E</i>	<i>4.1</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>1.61</i>
<i>931232</i>	<i>AB1-173 E</i>	<i>0.75</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>1.61</i>
<i>931242</i>	<i>AB1-173AE</i>	<i>0.75</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.57</i>
<i>923852</i>	<i>AB2-025 E</i>	<i>1.3</i>
<i>923911</i>	<i>AB2-031 C OI</i>	<i>1.6</i>
<i>923912</i>	<i>AB2-031 E OI</i>	<i>0.79</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.16</i>
<i>923942</i>	<i>AB2-035 E</i>	<i>0.07</i>
<i>923991</i>	<i>AB2-040 C OI</i>	<i>5.26</i>
<i>923992</i>	<i>AB2-040 E OI</i>	<i>4.3</i>
<i>924021</i>	<i>AB2-043 C OI</i>	<i>1.43</i>
<i>924022</i>	<i>AB2-043 E OI</i>	<i>2.34</i>
<i>924151</i>	<i>AB2-059 C OI</i>	<i>5.37</i>
<i>924152</i>	<i>AB2-059 E OI</i>	<i>2.76</i>
<i>924161</i>	<i>AB2-060 C OI</i>	<i>4.07</i>

924162	AB2-060 E O1	1.92
924301	AB2-077 C O1	0.91
924302	AB2-077 E O1	0.6
924311	AB2-078 C O1	0.91
924312	AB2-078 E O1	0.6
924321	AB2-079 C O1	0.91
924322	AB2-079 E O1	0.6
924381	AB2-087 C	0.25
924382	AB2-087 E	0.12
924391	AB2-088 C	0.21
924392	AB2-088 E	0.1
924401	AB2-089 C	1.08
924402	AB2-089 E	0.55
924411	AB2-090 C	1.8
924412	AB2-090 E	0.92
924491	AB2-098 C	0.25
924492	AB2-098 E	0.11
924501	AB2-099 C	0.26
924502	AB2-099 E	0.11
924511	AB2-100 C	10.65
924512	AB2-100 E	5.25
925121	AB2-169 C	2.45
925122	AB2-169 E	2.2
925171	AB2-174 C O1	5.22
925172	AB2-174 E O1	4.72
925221	AB2-176 C	0.74
925222	AB2-176 E	0.32
925591	AC1-034 C	3.33
925592	AC1-034 E	2.52
925611	AC1-036 C	0.37
925612	AC1-036 E	0.61
925781	AC1-054 C	3.71
925782	AC1-054 E	1.71
926071	AC1-086 C	14.1
926072	AC1-086 E	6.42
926201	AC1-098 C	3.13
926202	AC1-098 E	1.86
926211	AC1-099 C	1.05
926212	AC1-099 E	0.62
926271	AC1-105 C	2.38
926272	AC1-105 E	1.19
926771	AC1-163 C	0.84
926772	AC1-163 E	0.39
927021	AC1-189 C	3.98
927022	AC1-189 E	1.98

<i>927111</i>	<i>ACI-206 C</i>	<i>9.5</i>
<i>927112</i>	<i>ACI-206 E</i>	<i>4.49</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>4.92</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>2.19</i>
<i>927251</i>	<i>ACI-221 C</i>	<i>0.94</i>
<i>927252</i>	<i>ACI-221 E</i>	<i>0.94</i>
<i>927261</i>	<i>ACI-222 C</i>	<i>1.48</i>
<i>927262</i>	<i>ACI-222 E</i>	<i>1.41</i>

Appendix 5

(DVP - DVP) The 6CHRL249-6LOCKS 230 kV line (from bus 314285 to bus 314316 ckt 1) loads from 104.8% to 106.91% (**DC power flow**) of its load dump rating (684 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 562T563'. This project contributes approximately 15.19 MW to the thermal violation.

```
CONTINGENCY 'DVP_P4-2: 562T563'                /*CARSON
  OPEN BRANCH FROM BUS 314902 TO BUS 314923 CKT 1  /*CARSON TO
MIDLOTHIAN
  OPEN BRANCH FROM BUS 314914 TO BUS 314902 CKT 1  /*CARSON 500.00
- 8SEPTA 500.00
END
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315105	1BRUNSWICKS1	11.25
315131	1EDGECMA	4.76
315132	1EDGECMB	4.76
315139	1GASTONA	2.46
315141	1GASTONB	2.46
315136	1ROSEMG1	1.7
315138	1ROSEMG2	0.8
315137	1ROSEMS1	1.06
315073	1STONECA	-2.58
314557	3BETHELC	0.39
314554	3BTLEBRO	0.41
314572	3EMPORIA	0.33
314578	3HORNRTN	1.92
314582	3KELFORD	0.39
314704	3LAWRENC	0.28
314603	3SCOT NK	1.62
314617	3TUNIS	0.36
314541	3WATKINS	0.24
314620	6CASHIE	0.31
314574	6EVERETS	1.06
932631	AC2-084 C	4.46
932632	AC2-084 E	2.2
932701	AC2-093 C	40.58
932702	AC2-093 E	23.21
932761	AC2-100 C	2.16
932762	AC2-100 E	1.05
933451	AC2-158 C	2.15
933452	AC2-158 E	2.15
933461	AC2-159 C	3.44
933462	AC2-159 E	3.44
933991	AD1-023 C	4.58

933992	AD1-023 E	2.49
934041	AD1-029 C	5.52
934042	AD1-029 E	3.64
934071	AD1-034 C O2	9.22
934072	AD1-034 E O2	5.97
934201	AD1-047 C	5.74
934202	AD1-047 E	3.83
934231	AD1-050 C	2.37
934232	AD1-050 E	1.3
934311	AD1-055 C	1.03
934312	AD1-055 E	0.27
934331	AD1-057 C O2	5.2
934332	AD1-057 E O2	2.77
934341	AD1-058 C	2.35
934342	AD1-058 E	0.6
934521	AD1-076 C O2	19.48
934522	AD1-076 E O2	9.92
934611	AD1-087 C O2	3.75
934612	AD1-087 E O2	1.75
934621	AD1-088 C O2	6.62
934622	AD1-088 E O2	3.11
LTF	AD1-120	5.26
LTF	AD1-121	5.24
934911	AD1-123 C	0.45
934912	AD1-123 E	0.23
934991	AD1-131 C	0.77
934992	AD1-131 E	0.51
935171	AD1-152 C O2	3.36
935172	AD1-152 E O2	2.24
935211	AD1-156 C	1.
935212	AD1-156 E	0.67
LTF	CARR	0.18
LTF	CBM-S1	6.32
LTF	CBM-S2	12.36
LTF	CBM-W1	13.64
LTF	CBM-W2	33.99
LTF	CIN	3.08
LTF	CPLE	3.87
LTF	G-007	1.04
LTF	IPL	1.96
LTF	LGEE	0.67
LTF	MEC	6.97
LTF	MECS	3.01
LTF	O-066	3.47
LTF	RENSSELAER	0.14

<i>LTF</i>	<i>ROSETON</i>	<i>1.04</i>
<i>292791</i>	<i>U1-032 E</i>	<i>-1.34</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.13</i>
<i>LTF</i>	<i>WEC</i>	<i>0.84</i>
<i>916301</i>	<i>Z1-086 C</i>	<i>33.</i>
<i>916302</i>	<i>Z1-086 E</i>	<i>5.26</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.46</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.3</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>1.84</i>
<i>917592</i>	<i>Z2-099 E</i>	<i>0.18</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>2.09</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>1.82</i>
<i>918532</i>	<i>AA1-067 E</i>	<i>0.32</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.08</i>
<i>919692</i>	<i>AA2-053 E</i>	<i>2.08</i>
<i>919702</i>	<i>AA2-057 E</i>	<i>1.84</i>
<i>919822</i>	<i>AA2-068 E</i>	<i>0.54</i>
<i>LTF</i>	<i>AA2-074</i>	<i>2.63</i>
<i>920022</i>	<i>AA2-086 E</i>	<i>0.1</i>
<i>920042</i>	<i>AA2-088 E</i>	<i>4.33</i>
<i>920592</i>	<i>AA2-165 E</i>	<i>0.24</i>
<i>920631</i>	<i>AA2-169 C</i>	<i>1.18</i>
<i>920632</i>	<i>AA2-169 E</i>	<i>0.54</i>
<i>920672</i>	<i>AA2-174 E</i>	<i>0.24</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>4.55</i>
<i>930402</i>	<i>AB1-081 E</i>	<i>1.95</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>9.57</i>
<i>930862</i>	<i>AB1-132 E</i>	<i>4.1</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>1.61</i>
<i>931232</i>	<i>AB1-173 E</i>	<i>0.75</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>1.61</i>
<i>931242</i>	<i>AB1-173AE</i>	<i>0.75</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.57</i>
<i>923852</i>	<i>AB2-025 E</i>	<i>1.3</i>
<i>923911</i>	<i>AB2-031 C OI</i>	<i>1.6</i>
<i>923912</i>	<i>AB2-031 E OI</i>	<i>0.79</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.16</i>
<i>923942</i>	<i>AB2-035 E</i>	<i>0.07</i>
<i>923991</i>	<i>AB2-040 C OI</i>	<i>5.26</i>
<i>923992</i>	<i>AB2-040 E OI</i>	<i>4.3</i>
<i>924021</i>	<i>AB2-043 C OI</i>	<i>1.43</i>
<i>924022</i>	<i>AB2-043 E OI</i>	<i>2.34</i>
<i>924151</i>	<i>AB2-059 C OI</i>	<i>5.37</i>
<i>924152</i>	<i>AB2-059 E OI</i>	<i>2.76</i>
<i>924161</i>	<i>AB2-060 C OI</i>	<i>4.07</i>

924162	AB2-060 E O1	1.92
924301	AB2-077 C O1	0.91
924302	AB2-077 E O1	0.6
924311	AB2-078 C O1	0.91
924312	AB2-078 E O1	0.6
924321	AB2-079 C O1	0.91
924322	AB2-079 E O1	0.6
924381	AB2-087 C	0.25
924382	AB2-087 E	0.12
924391	AB2-088 C	0.21
924392	AB2-088 E	0.1
924401	AB2-089 C	1.08
924402	AB2-089 E	0.55
924411	AB2-090 C	1.8
924412	AB2-090 E	0.92
924491	AB2-098 C	0.25
924492	AB2-098 E	0.11
924501	AB2-099 C	0.26
924502	AB2-099 E	0.11
924511	AB2-100 C	10.65
924512	AB2-100 E	5.25
925121	AB2-169 C	2.45
925122	AB2-169 E	2.2
925171	AB2-174 C O1	5.22
925172	AB2-174 E O1	4.72
925221	AB2-176 C	0.74
925222	AB2-176 E	0.32
925591	AC1-034 C	3.33
925592	AC1-034 E	2.52
925611	AC1-036 C	0.37
925612	AC1-036 E	0.61
925781	AC1-054 C	3.71
925782	AC1-054 E	1.71
926071	AC1-086 C	14.1
926072	AC1-086 E	6.42
926201	AC1-098 C	3.13
926202	AC1-098 E	1.86
926211	AC1-099 C	1.05
926212	AC1-099 E	0.62
926271	AC1-105 C	2.38
926272	AC1-105 E	1.19
926771	AC1-163 C	0.84
926772	AC1-163 E	0.39
927021	AC1-189 C	3.98
927022	AC1-189 E	1.98

<i>927111</i>	<i>ACI-206 C</i>	<i>9.5</i>
<i>927112</i>	<i>ACI-206 E</i>	<i>4.49</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>4.92</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>2.19</i>
<i>927251</i>	<i>ACI-221 C</i>	<i>0.94</i>
<i>927252</i>	<i>ACI-221 E</i>	<i>0.94</i>
<i>927261</i>	<i>ACI-222 C</i>	<i>1.48</i>
<i>927262</i>	<i>ACI-222 E</i>	<i>1.41</i>

Appendix 6

(DVP - DVP) The 6CHESTF B-6BASIN 230 kV line (from bus 314287 to bus 314276 ckt 1) loads from 124.7% to 125.84% (**DC power flow**) of its emergency rating (449 MVA) for the single line contingency outage of 'DVP_P1-2: LN 563'. This project contributes approximately 5.06 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 563'

OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1
500.00 - 8MDLTHAN 500.00

/* 8CARSON

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315065	1CHESTF6	33.34
315131	1EDGECEMA	3.18
315132	1EDGECEMB	3.18
315139	1GASTONA	1.58
315141	1GASTONB	1.58
315119	1GRAVEL3	1.24
315120	1GRAVEL4	1.26
315121	1GRAVEL5	1.24
315122	1GRAVEL6	1.26
315117	1GRAVELC	0.43
315074	1HOPCGN1	5.63
315075	1HOPCGN2	5.56
315077	1HOPHCF1	1.78
315078	1HOPHCF2	1.78
315079	1HOPHCF3	1.78
315080	1HOPHCF4	2.7
315076	1HOPPOLC	1.27
315116	1SURRY 1	12.47
314314	3LOCKS	0.06
314315	3LOCKS E	0.77
932041	AC2-012 C	3.21
932581	AC2-078 C	2.86
932591	AC2-079 C	3.07
932631	AC2-084 C	3.22
932701	AC2-093 C	23.37
933451	AC2-158 C	1.94
933461	AC2-159 C	2.55
933471	AC2-161 C	0.89
933711	AC2-194 C	0.35
933731	AC2-196 C	0.55
933991	AD1-023 C	4.54
934011	AD1-025 C O2	9.21
934041	AD1-029 C	3.98

934061	AD1-033 C O2	2.31
934071	AD1-034 C O2	5.06
934201	AD1-047 C	3.58
934331	AD1-057 C O2	3.61
934521	AD1-076 C O2	18.25
934571	AD1-082 C O2	5.05
935111	AD1-144 C	0.56
935211	AD1-156 C	1.97
LTF	CARR	0.2
LTF	CBM-S1	3.35
LTF	CBM-S2	7.31
LTF	CBM-W1	6.11
LTF	CBM-W2	17.58
LTF	CIN	1.4
LTF	CPLE	2.35
LTF	IPL	0.89
LTF	LGEE	0.31
LTF	MEC	3.38
LTF	MECS	1.12
LTF	RENSSELAER	0.16
LTF	ROSETON	1.14
LTF	WEC	0.39
914231	Y2-077	0.72
LTF	AA2-074	1.6
920631	AA2-169 C	0.75
920691	AA2-178 C	3.22
930051	AB1-013 C	0.97
930401	AB1-081 C	3.05
930861	AB1-132 C	6.17
931231	AB1-173 C	1.01
931241	AB1-173AC	1.01
923801	AB2-015 C O1	3.22
923831	AB2-022 C	0.73
923851	AB2-025 C	0.31
923911	AB2-031 C O1	1.
923941	AB2-035 C	0.11
923991	AB2-040 C O1	3.28
924071	AB2-051	42.84
924151	AB2-059 C O1	3.6
924381	AB2-087 C	0.21
924391	AB2-088 C	0.15
924491	AB2-098 C	0.19
924501	AB2-099 C	0.22
924511	AB2-100 C	6.19
924811	AB2-134 C O1	7.02

925051	AB2-160 C O1	3.33
925061	AB2-161 C O1	1.87
925121	AB2-169 C	2.2
925171	AB2-174 C O1	3.2
925281	AB2-186 C	0.2
925291	AB2-188 C O1	0.79
925331	AB2-190 C	10.95
925591	AC1-034 C	2.34
925821	AC1-061	< 0.01
926071	AC1-086 C	9.08
926201	AC1-098 C	2.26
926211	AC1-099 C	0.76
926741	AC1-159	20.65
926771	AC1-163 C	0.71
927021	AC1-189 C	2.92
927111	AC1-206 C	5.47
927141	AC1-208 C	3.41
927221	AC1-216 C O1	5.36

Appendix 7

(DVP - DVP) The 6CLUBHSE 230/115 kV transformer (from bus 314563 to bus 314562 ckt 1) loads from 109.32% to 113.91% (**DC power flow**) of its load dump rating (209 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 239T2141'. This project contributes approximately 9.59 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 239T2141' /* LAKEVIEW
 OPEN BRANCH FROM BUS 314583 TO BUS 314579 CKT 1 /* 239
 OPEN BRANCH FROM BUS 314579 TO BUS 314605 CKT 1 /* 2057
 OPEN BRANCH FROM BUS 314583 TO BUS 314561 CKT 1 /* 2141
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315139	1GASTONA	4.6
315141	1GASTONB	4.6
314541	3WATKINS	-0.27
934043	AD1-029 BAT	9.45
934071	AD1-034 C O2	5.82
934072	AD1-034 E O2	3.77
934233	AD1-050 BAT	5.52
LTF	AMIL	0.13
LTF	BAYOU	0.69
LTF	BIG_CAJUN1	1.09
LTF	BIG_CAJUN2	2.18
LTF	BLUEG	0.69
LTF	CALDERWOOD	0.41
LTF	CANNELTON	0.13
LTF	CATAWBA	0.39
LTF	CBM-N	0.02
LTF	CELEVELAND	1.12
LTF	CHEOAH	0.38
LTF	CHILHOWEE	0.13
LTF	CHOCTAW	0.74
LTF	CLIFTY	2.53
LTF	COTTONWOOD	2.7
LTF	DEARBORN	0.23
LTF	EDWARDS	0.21
LTF	ELMERSMITH	0.39
LTF	FARMERCITY	0.17
LTF	G-007A	0.55
LTF	GIBSON	0.24
LTF	HAMLET	1.52
LTF	MORGAN	1.2
LTF	NEWTON	0.58
LTF	NYISO	0.28

<i>LTF</i>	<i>O-066A</i>	<i>0.26</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>1.25</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.83</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.11</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.11</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.28</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.25</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.13</i>
<i>LTF</i>	<i>TVA</i>	<i>0.51</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.72</i>
<i>LTF</i>	<i>VFT</i>	<i>1.48</i>
<i>LTF</i>	<i>X1-078</i>	<i>0.42</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>17.9</i>
<i>930862</i>	<i>AB1-132 E</i>	<i>7.67</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.33</i>
<i>923852</i>	<i>AB2-025 E</i>	<i>0.75</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>14.28</i>
<i>924512</i>	<i>AB2-100 E</i>	<i>7.03</i>
<i>926071</i>	<i>AC1-086 C</i>	<i>26.37</i>
<i>926072</i>	<i>AC1-086 E</i>	<i>12.</i>
<i>927111</i>	<i>AC1-206 C</i>	<i>12.3</i>
<i>927112</i>	<i>AC1-206 E</i>	<i>5.82</i>

Appendix 8

(DVP - DVP) The 6LAKEVEW-6CAROLNA 230 kV line (from bus 314583 to bus 314561 ckt 1) loads from 126.89% to 128.96% (**DC power flow**) of its emergency rating (375 MVA) for the single line contingency outage of 'DVP_P1-2: LN 2056'. This project contributes approximately 7.78 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 2056'

OPEN BRANCH FROM BUS 313845 TO BUS 314579 CKT 1
230.00 - 6HORNRTN 230.00

/* 6HATHAWAY

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315139	1GASTONA	12.26
315141	1GASTONB	12.26
315136	1ROSEMG1	8.8
315138	1ROSEMG2	4.12
315137	1ROSEMS1	5.46
314704	3LAWRENC	0.21
934043	AD1-029 BAT	14.31
934071	AD1-034 C O2	7.78
934233	AD1-050 BAT	3.5
935211	AD1-156 C	0.6
LTF	AMIL	0.18
LTF	BAYOU	0.93
LTF	BIG_CAJUN1	1.47
LTF	BIG_CAJUN2	2.95
LTF	BLUEG	0.92
LTF	CALDERWOOD	0.55
LTF	CANNELTON	0.18
LTF	CATAWBA	0.53
LTF	CBM-N	< 0.01
LTF	CELEVELAND	1.5
LTF	CHEOAH	0.51
LTF	CHILHOWEE	0.18
LTF	CHOCTAW	1.
LTF	CLIFTY	3.38
LTF	COTTONWOOD	3.64
LTF	DEARBORN	0.33
LTF	EDWARDS	0.28
LTF	ELMERSMITH	0.52
LTF	FARMERCITY	0.22
LTF	G-007A	0.39
LTF	GIBSON	0.32
LTF	HAMLET	2.16
LTF	MORGAN	1.61

<i>LTF</i>	<i>NEWTON</i>	<i>0.78</i>
<i>LTF</i>	<i>NYISO</i>	<i>0.03</i>
<i>LTF</i>	<i>O-066A</i>	<i>0.18</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>1.69</i>
<i>LTF</i>	<i>ROWAN</i>	<i>1.08</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.15</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.15</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.38</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.34</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.18</i>
<i>LTF</i>	<i>TVA</i>	<i>0.68</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.97</i>
<i>LTF</i>	<i>VFT</i>	<i>1.03</i>
<i>LTF</i>	<i>X1-078</i>	<i>0.3</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>47.69</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.44</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>21.43</i>
<i>926071</i>	<i>AC1-086 C</i>	<i>70.23</i>
<i>927111</i>	<i>AC1-206 C</i>	<i>16.67</i>

Appendix 9

(DVP - DVP) The AD1-034 TAP-6SAPONY 230 kV line (from bus 934070 to bus 314435 ckt 1) loads from 122.32% to 130.38% (**DC power flow**) of its load dump rating (637 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 246T2034'. This project contributes approximately 54.37 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 246T2034' /* EARLEYS
 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246
 OPEN BRANCH FROM BUS 314575 TO BUS 314537 CKT 1 /* 246
 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR
 OPEN BRANCH FROM BUS 314569 TO BUS 933450 CKT 1 /* 2034
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	11.46
315132	1EDGECEMB	11.46
315139	1GASTONA	7.99
315141	1GASTONB	7.99
315126	1ROARAP2	2.89
315128	1ROARAP4	2.78
315136	1ROSEMG1	5.4
315138	1ROSEMG2	2.53
315137	1ROSEMS1	3.35
314557	3BETHEL C	0.96
314554	3BTLEBRO	0.97
314572	3EMPORIA	1.07
314578	3HORNRTN	5.76
314582	3KELFORD	1.24
314704	3LAWRENC	0.85
314603	3SCOT NK	4.89
314617	3TUNIS	1.14
314541	3WATKINS	0.52
314574	6EVERETS	2.71
932631	AC2-084 C	12.97
932632	AC2-084 E	6.39
933461	AC2-159 C	10.98
933462	AC2-159 E	10.98
934041	AD1-029 C	16.05
934042	AD1-029 E	10.58
934071	AD1-034 C O2	32.99
934072	AD1-034 E O2	21.38
934201	AD1-047 C	18.26
934202	AD1-047 E	12.17
934231	AD1-050 C	5.37
934232	AD1-050 E	2.93

934331	AD1-057 C O2	14.21
934332	AD1-057 E O2	7.58
934621	AD1-088 C O2	12.9
934622	AD1-088 E O2	6.05
LTF	AD1-120	4.72
LTF	AD1-121	4.7
LTF	CARR	0.12
LTF	CBM-S1	5.81
LTF	CBM-S2	11.59
LTF	CBM-W1	12.9
LTF	CBM-W2	31.36
LTF	CIN	2.91
LTF	CPL	3.91
LTF	G-007	0.8
LTF	IPL	1.85
LTF	LGEE	0.63
LTF	MEC	6.5
LTF	MECS	2.94
LTF	O-066	2.67
LTF	RENSSELAER	0.1
LTF	ROSETON	0.7
900671	V4-068 C	0.13
900672	V4-068 E	0.37
LTF	WEC	0.8
917331	Z2-043 C	0.68
917332	Z2-043 E	1.49
917341	Z2-044 C	0.34
917342	Z2-044 E	0.75
917511	Z2-088 C OP1	1.13
917512	Z2-088 E OP1	4.55
917591	Z2-099 C	0.22
917592	Z2-099 E	0.48
918411	AA1-050	0.95
918491	AA1-063AC OP	2.52
918492	AA1-063AE OP	6.06
918511	AA1-065 C OP	2.7
918512	AA1-065 E OP	6.77
918531	AA1-067 C	0.37
918532	AA1-067 E	0.81
918561	AA1-072 C	0.1
918562	AA1-072 E	0.25
919691	AA2-053 C	2.94
919692	AA2-053 E	6.44
919701	AA2-057 C	1.91
919702	AA2-057 E	4.86

919821	AA2-068 C	0.64
919822	AA2-068 E	1.51
LTF	AA2-074	2.66
920021	AA2-086 C	0.11
920022	AA2-086 E	0.26
920041	AA2-088 C	1.35
920042	AA2-088 E	11.25
920591	AA2-165 C	0.26
920592	AA2-165 E	0.64
920631	AA2-169 C	2.97
920632	AA2-169 E	1.36
920671	AA2-174 C	0.13
920672	AA2-174 E	0.74
930401	AB1-081 C	10.91
930402	AB1-081 E	4.68
930861	AB1-132 C	31.1
930862	AB1-132 E	13.33
931231	AB1-173 C	5.14
931232	AB1-173 E	2.4
931241	AB1-173AC	5.14
931242	AB1-173AE	2.4
923911	AB2-031 C OI	5.1
923912	AB2-031 E OI	2.51
923941	AB2-035 C	0.4
923942	AB2-035 E	0.17
923991	AB2-040 C OI	16.74
923992	AB2-040 E OI	13.69
924021	AB2-043 C OI	2.79
924022	AB2-043 E OI	4.58
924151	AB2-059 C OI	12.86
924152	AB2-059 E OI	6.63
924161	AB2-060 C OI	7.93
924162	AB2-060 E OI	3.73
924301	AB2-077 C OI	1.75
924302	AB2-077 E OI	1.17
924311	AB2-078 C OI	1.75
924312	AB2-078 E OI	1.17
924321	AB2-079 C OI	1.75
924322	AB2-079 E OI	1.17
924381	AB2-087 C	0.86
924382	AB2-087 E	0.4
924391	AB2-088 C	0.52
924392	AB2-088 E	0.25
924401	AB2-089 C	2.43
924402	AB2-089 E	1.25

924411	AB2-090 C	3.52
924412	AB2-090 E	1.8
924491	AB2-098 C	0.63
924492	AB2-098 E	0.27
924501	AB2-099 C	0.85
924502	AB2-099 E	0.36
924511	AB2-100 C	36.7
924512	AB2-100 E	18.08
925171	AB2-174 C OI	16.74
925172	AB2-174 E OI	15.15
925221	AB2-176 C	1.45
925222	AB2-176 E	0.62
925591	AC1-034 C	8.2
925592	AC1-034 E	6.18
925781	AC1-054 C	8.75
925782	AC1-054 E	4.03
926071	AC1-086 C	45.8
926072	AC1-086 E	20.85
926201	AC1-098 C	9.1
926202	AC1-098 E	5.42
926211	AC1-099 C	3.05
926212	AC1-099 E	1.79
926771	AC1-163 C	2.79
926772	AC1-163 E	1.3
927021	AC1-189 C	9.96
927022	AC1-189 E	4.96
927111	AC1-206 C	32.89
927112	AC1-206 E	15.55
927141	AC1-208 C	14.12
927142	AC1-208 E	6.27