

Generation Interconnection Feasibility Study Report Queue Position AD2-029

The Interconnection Customer (IC) has proposed a 19.5 MW (7.9 MWC) solar generating facility to be located in Dorchester County, Maryland. PJM studied AD2-029 as a 19.5 MW injection into the Delmarva Power and Light Company (DPL) system at the Airey 69 kV Substation and evaluated it for compliance with reliability criteria for summer peak conditions in 2021. AD2-029 was studied with a commercial probability of 53%. The planned in-service date, as requested by the IC during the project kick-off call, is December 31, 2019. This date may not be attainable due to additional required PJM studies and Transmission Owner construction schedule.

Point of Interconnection

The Interconnection Customer requested a distribution level interconnection. Distribution facilities in the area of the AD2-029 project are owned by the Choptank Electric Cooperative (CEC). It is anticipated that the AD2-029 project will connect with the CEC system at a new substation to be constructed adjacent to the DPL West Cambridge to Vienna 69 kV circuit. The DPL transmission system will supply the new CEC substation.

Transmission Owner Scope of Attachment Facility Work

There is no DPL Attachment Facility work required for the AD2-029 project. The IC must contact CEC for their work scope and schedule.

Metering

Revenue metering specifications will be established by CEC.

Interconnection Customer Scope of Work

The Interconnection Customer assumes full responsibility for design and construction of all facilities associated with the AD2-029 generating station and the direct connection line on the IC side of the Point of Interconnection.

The IC will be required to install metering and telemetry equipment to provide revenue metering and real-time telemetry data to PJM. The requirements for this equipment are listed in Appendix 2, Section 8 of Attachment O to the PJM Tariff, as well as PJM Manuals 01 and 14D.

It is the IC's responsibility to send the data that PJM and DPL requires directly to PJM. The IC will grant permission for PJM to send DPL the following telemetry that the IC sends to PJM: real time MW, MVAR, volts, amperes, generator status, and interval MWH and MVARH.

Summer Peak Analysis - 2021

Transmission Network Impacts

Potential transmission network impacts are as follows:

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

- 1. (DP&L - DP&L) The CHURCH-TOWNSEND 138 kV line (from bus 232100 to bus 232107 ckt 1) loads from 123.55% to 124.83% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'/* #1 & #2 KEENEY-STEELE 230
 OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
 OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2
 END

Please refer to Appendix 1 for a table containing the generators having contribution to this flowgate.

- 2. (DP&L - DP&L) The CHURCH-TOWNSEND 138 kV line (from bus 232100 to bus 232107 ckt 1) loads from 108.64% to 109.93% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_B'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_B'/* #1 & #2 KEENEY-STEELE 230
 OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
 OPEN LINE FROM BUS 923960 TO BUS 232000 CKT 2
 END

- 3. (DP&L - DP&L) The MIDLTNTP-MT PLSNT 138 kV line (from bus 232106 to bus 232104 ckt 1) loads from 119.6% to 120.89% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'/* #1 & #2 KEENEY-STEELE 230
 OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
 OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2

END

Please refer to Appendix 2 for a table containing the generators having contribution to this flowgate.

4. (DP&L - DP&L) The MIDLTNTP-MT PLSNT 138 kV line (from bus 232106 to bus 232104 ckt 1) loads from 104.7% to 105.99% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_B'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_B'/* #1 & #2 KEENEY-STEELE 230
OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
OPEN LINE FROM BUS 923960 TO BUS 232000 CKT 2
END

5. (DP&L - DP&L) The TOWNSEND-MIDLTNTP 138 kV line (from bus 232107 to bus 232106 ckt 1) loads from 130.04% to 131.32% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'/* #1 & #2 KEENEY-STEELE 230
OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2
END

Please refer to Appendix 3 for a table containing the generators having contribution to this flowgate.

6. (DP&L - DP&L) The TOWNSEND-MIDLTNTP 138 kV line (from bus 232107 to bus 232106 ckt 1) loads from 115.13% to 116.42% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_B'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_B'/* #1 & #2 KEENEY-STEELE 230
OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1
OPEN LINE FROM BUS 923960 TO BUS 232000 CKT 2
END

7. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 162.43% to 167.92% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP11'. This project contributes approximately 5.11 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP11'/*STEELE BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
230 230

DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1/*STEELE AD2-004
TAP 230 230
END

Please refer to Appendix 4 for a table containing the generators having contribution to this flowgate.

8. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 109.6% to 114.69% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP12'. This project contributes approximately 4.73 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP12'/*STEELE BUS BREAKER TO VIENNA
DISCONNECT BRANCH FROM BUS 232000 TO BUS 232103 CKT 2 /*STEELE STEELE
230 138 AT21
DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1/*STEELE AD2-004
TAP 230 230
END

9. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 103.44% to 105.52% (**DC power flow**) of its emergency rating (93 MVA) for the single line contingency outage of "'232000'. This project contributes approximately 1.93 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

10. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 168.23% to 173.73% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP11'. This project contributes approximately 5.11 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP11'/*STEELE BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
230 230
DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1/*STEELE AD2-004
TAP 230 230
END

Please refer to Appendix 5 for a table containing the generators having contribution to this flowgate.

11. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 115.41% to 120.49% (**DC power flow**) of its emergency rating (93 MVA) for the line fault

with failed breaker contingency outage of 'DPL_P4-2_DP12'. This project contributes approximately 4.73 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP12'/*STEELE BUS BREAKER TO VIENNA
DISCONNECT BRANCH FROM BUS 232000 TO BUS 232103 CKT 2/*STEELE STEELE
230 138 AT21
DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1/*STEELE AD2-004
TAP 230 230
END

12. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 109.24% to 111.32% (**DC power flow**) of its emergency rating (93 MVA) for the single line contingency outage of "'232000'. This project contributes approximately 1.93 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

13. (DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 126.74% to 133.69% (**DC power flow**) of its emergency rating (42 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP36'. This project contributes approximately 2.92 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP36'/*COOL SPRINGS BUS BREAKER TO IR 2
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232006 CKT 1 /*COOL
SPRINGS INDRIV 4 230 230
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232004 CKT 1 /*COOL
SPRINGS MILFORD 230 230
END

Please refer to Appendix 6 for a table containing the generators having contribution to this flowgate.

14. (DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 126.74% to 133.69% (**DC power flow**) of its emergency rating (42 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP34'. This project contributes approximately 2.92 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP34'/*COOL SPRINGS BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232004 CKT 1/*COOL SPRINGS
INDRIV 4 230 230
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232269 CKT 1/*COOL SPRINGS 230
138
END

15. (DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 126.74% to 133.69% (**DC power flow**) of its emergency rating (42 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP35'. This project contributes approximately 2.92 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP35'/*COOL SPRINGS BUS BREAKER TO IR
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232006 CKT 1/*COOL SPRINGS
INDRIV 4 230 230
DISCONNECT BRANCH FROM BUS 232001 TO BUS 232269 CKT 1/*COOL SPRINGS 230
138
END

16. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 114.74% to 116.89% (**DC power flow**) of its emergency rating (58 MVA) for the single line contingency outage of 'DPL_P1_2_CKT 6728'. This project contributes approximately 1.24 MW to the thermal violation.

CONTINGENCY 'DPL_P1_2_CKT 6728'
OPEN LINE FROM BUS 232272 TO BUS 232274 CIRCUIT 1/MOUNT HERMON - PINEY
GROVE 69
DISCONNECT BUS 230912/ PINEY GROVE 69 CAP
END

Please refer to Appendix 7 for a table containing the generators having contribution to this flowgate.

17. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 114.44% to 116.65% (**DC power flow**) of its emergency rating (58 MVA) for the single line contingency outage of 'DPL_P1_3_LORETO AT1&2'. This project contributes approximately 1.28 MW to the thermal violation.

CONTINGENCY 'DPL_P1_3_LORETO AT1&2'
OPEN LINE FROM BUS 232127 TO BUS 232275 CIRCUIT 1/LORETTO AT1 138/69
OPEN LINE FROM BUS 232127 TO BUS 232275 CIRCUIT 2 /LORETTO AT2 138/69
END

18. (DP&L - DP&L) The AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) loads from 141.96% to 142.58% (**DC power flow**) of its emergency rating (551 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP59'. This project contributes approximately 7.63 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP59'/*PINEY GROVE BUS BREAKER
DISCONNECT BRANCH FROM BUS 232131 TO BUS 924680 CKT 1/*PINEY GROVE AB2-
120 TAP 138 138
DISCONNECT BRANCH FROM BUS 232007 TO BUS 232128 CKT 1/*PINEY GROVE
PINEY GROVE 230 138

END

Please refer to Appendix 8 for a table containing the generators having contribution to this flowgate.

19. (DP&L - DP&L) The AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) loads from 141.88% to 142.5% (**DC power flow**) of its emergency rating (551 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP60A'. This project contributes approximately 7.63 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP60A' /*PINEY GROVE BUS BREAKER
DISCONNECT BRANCH FROM BUS 232007 TO BUS 232006 CKT 1/*PINEY GROVE
INDIAN RIVER 230 230
DISCONNECT BRANCH FROM BUS 232007 TO BUS 232128 CKT 1/*PINEY GROVE
PINEY GROVE 230 138
END

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

1. (DP&L - DP&L) The VIENNA 8-NELSON 138 kV line (from bus 232117 to bus 232119 ckt 1) loads from 164.17% to 165.02% (**DC power flow**) of its emergency rating (226 MVA) for the single line contingency outage of "'232000'. This project contributes approximately 4.25 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

2. (DP&L - DP&L) The NELSON-INDRV2&3 138 kV line (from bus 232119 to bus 232121 ckt 1) loads from 151.52% to 152.58% (**DC power flow**) of its emergency rating (193 MVA) for the single line contingency outage of "'232000'. This project contributes approximately 4.55 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

3. (DP&L - DP&L) The LORETTO-PINEY138 138 kV line (from bus 232127 to bus 232128 ckt 1) loads from 127.83% to 128.7% (**DC power flow**) of its emergency rating (159 MVA) for the single line contingency outage of "'232000'". This project contributes approximately 3.06 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

4. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 108.71% to 113.81% (**DC power flow**) of its emergency rating (93 MVA) for the single line contingency outage of "'232000'". This project contributes approximately 4.74 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

5. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 114.52% to 119.62% (**DC power flow**) of its emergency rating (93 MVA) for the single line contingency outage of "'232000'". This project contributes approximately 4.74 MW to the thermal violation.

CONTINGENCY '232000'STEELE 230 936020 AD2-004 TAP 230 1
OPEN BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
END

6. (DP&L - DP&L) The SHARPTWN-LAUREL 69 kV line (from bus 232239 to bus 232249 ckt 1) loads from 111.32% to 120.0% (**DC power flow**) of its emergency rating (43 MVA) for the single line contingency outage of 'DPL_P1_2_CKT 67BB'. This project contributes approximately 3.73 MW to the thermal violation.

CONTINGENCY 'DPL_P1_2_CKT 67BB'
DISCONNECT BUS 232233/ TODD - PRESTON - TANYARD 69
DISCONNECT BUS 232606/ PRESTON 12
DISCONNECT BUS 232821/ TANYARD - TALBOT 69
DISCONNECT BUS 232820/ TALBOT - LAKESIDE 69
END

7. (DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 125.12% to 132.13% (**DC power flow**) of its emergency rating (42 MVA) for the single line contingency outage of 'DPL_P1_3_COOLSPG AT20'. This project contributes approximately 2.95 MW to the thermal violation.

CONTINGENCY 'DPL_P1_3_COOLSPG AT20'
OPEN LINE FROM BUS 232001 TO BUS 232269 CIRCUIT 1/COOL SPRINGS AT20 230/69

END

8. (DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 103.63% to 110.79% (**DC power flow**) of its normal rating (42 MVA) for **non-contingency** condition. This project contributes approximately 3.01 MW to the thermal violation.
9. (DP&L - DP&L) The HEBRON-ROCKAWLKN 69 kV line (from bus 232270 to bus 232291 ckt 1) loads from 118.43% to 124.84% (**DC power flow**) of its emergency rating (64 MVA) for the single line contingency outage of 'DPL_P1_2_CKT 6705'. This project contributes approximately 4.1 MW to the thermal violation.

CONTINGENCY 'DPL_P1_2_CKT 6705'
DISCONNECT BUS 232239/ LAUREL - SHARPTOWN - VIENNA 69 & SHARPTOWN
XFMR
DISCONNECT BUS 232607/ SHARPTOWN 12
END

10. (DP&L - DP&L) The HEBRON-ROCKAWLKN 69 kV line (from bus 232270 to bus 232291 ckt 1) loads from 98.52% to 103.6% (**DC power flow**) of its normal rating (64 MVA) for **non-contingency** condition. This project contributes approximately 3.25 MW to the thermal violation.
11. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 172.88% to 178.3% (**DC power flow**) of its emergency rating (58 MVA) for the single line contingency outage of 'DPL_P1_3_LORETO AT1&2'. This project contributes approximately 3.14 MW to the thermal violation.

CONTINGENCY 'DPL_P1_3_LORETO AT1&2'
OPEN LINE FROM BUS 232127 TO BUS 232275 CIRCUIT 1/LORETTO AT1 138/69
OPEN LINE FROM BUS 232127 TO BUS 232275 CIRCUIT 2/LORETTO AT2 138/69
END

12. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 151.64% to 157.25% (**DC power flow**) of its normal rating (58 MVA) for **non-contingency** condition. This project contributes approximately 3.25 MW to the thermal violation.
13. (DP&L - DP&L) The AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) loads from 137.9% to 138.5% (**DC power flow**) of its emergency rating (551 MVA) for the single line contingency outage of 'DPL_P1_2_CKT 13707'. This project contributes approximately 7.28 MW to the thermal violation.

CONTINGENCY 'DPL_P1_2_CKT 13707'
OPEN LINE FROM BUS 232119 TO BUS 232117 CIRCUIT 1/NELSON - VIENNA 138
END

14. (DP&L - DP&L) The AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) loads from 132.32% to 132.86% (**DC power flow**) of its normal rating (551 MVA) for **non-contingency** condition. This project contributes approximately 6.59 MW to the thermal violation.

Summer Peak Load Flow Analysis Reinforcements

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

None

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

- 1&2. To mitigate the (DP&L) CHURCH-TOWNSEND 138 kV line (from bus 232100 to bus 232107 ckt 1) overload will require substation reinforcements at Church Substation. The estimate to perform this work is **\$500,000** and will take approximately **24-36 months** to complete.
- 3&4. To mitigate the (DP&L) MIDLTNTP-MT PLSNT 138 kV line (from bus 232106 to bus 232104 ckt 1) overload will require increasing the emergency rating of the Townsend to Middletown Tap 138 kV line by rebuilding the circuit. The rebuild will include the installation of new poles, foundations, insulators, and conductor. It will also require substation reinforcements at Middletown Tap Substation. The estimate to perform this work is **\$480,000** and will take approximately **32-48 months** to complete.
- 5&6. To mitigate the (DP&L) TOWNSEND-MIDLTNTP 138 kV line (from bus 232107 to bus 232106 ckt 1) overload will require increasing the emergency rating of the Townsend to Middletown Tap 138 kV line by rebuilding the circuit. The rebuild will include the installation of new poles, foundations, insulators, and conductor. It will also require substation reinforcements at Townsend & Middletown Tap Substation. The estimate to perform this work is **\$700,000** and will take approximately **36-48 months** to complete.
- 7,8,9. This overload is identified in a previous queue and cost was allocated to that queue, AD2-029 will not get any cost allocation for the below project. However if all prior projects withdraw, AD2-029 will need to be re-tooled and could get cost allocation for the below upgrade in the future. AD2-029 isn't deliverable until the below upgrade is built.

Reinforcements include the replacement of a disconnect switch at Preston Substation. The estimate to perform this work is **\$36,000** and will take approximately **1 year** to complete.

- 10, 11,12. To mitigate the (DP&L) TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) overload will require substation reinforcements at Todd Substation. The estimate to perform this work is **\$600,000** and will take approximately **24 months** to complete.

In addition, there are limiting equipment at Todd & Preston that has been previously identified in a previous queue and cost was allocated to that queue, AD2-029 will not get any cost allocation for the below project. However if all prior projects withdraw, AD2-029 will need to be re-tooled and could get cost allocation for the below upgrade in the future. AD2-029 isn't deliverable until the below upgrade is built.

Reinforcements include substation reinforcements at Preston Substation and Todd Substation. The estimate to perform this work is **\$67,000** and will take approximately **1 year** to complete.

- 13,14,15. To mitigate the (DP&L - DP&L) VIENN-SHARPTWN 69 kV line overload will require rebuilding the 69 kV transmission line. The estimated cost to perform this work is **\$5,839,000** and will take approximately **3 years** to complete.

- 16&17. (DPL) To mitigate the overload will require increasing the emergency rating of the Rockawalkin to N Salisbury 69 kV line by rebuilding that section of the circuit. The rebuild will include the installation of new poles, foundations, insulators, and conductor. The estimated cost to perform this work is **\$5,157,000** and will take **44-48 months** to complete.

Note: There is a supplemental project (s0835) in place to upgrade this entire circuit 6708 from Vienna to N Salisbury. The portion from Hebron to N Salisbury (which includes Rockawalkin – N Salisbury) is estimated to cost approximately \$8.6M and is scheduled to be completed by 12/31/2019. Total cost of the entire project (Vienna to N Salisbury) is approximately **\$21.1M**. Expected ISD is 12/31/2023.

- 18&19. To mitigate the (DP&L) AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) overload will require increasing the emergency rating of the Vienna to Steele 230 kV line by rebuilding the circuit. The rebuild will include the installation of new poles, foundations, insulators, and conductor. It will also require substation reinforcements at Steele Substation. The estimate to perform this work is **\$59,000,000** and will take approximately **36-60 months** to complete.

Steady-State Voltage Requirements

To be performed during later study phases if required.

Short Circuit

No issues identified.

Stability and Reactive Power Requirement

To be performed during later study phases if required.

Light Load Analysis - 2021

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

Facilities Study Estimate

(If a Facilities Study is required, provide the estimated duration and cost estimate to perform Facilities Study)

If required the deposit would be \$50,000.

Delmarva Power and Light Costs

Cost estimates will further be refined as a part of the Impact Study and Facilities Study for this project. The Interconnection Customer will be responsible for all costs incurred by DPL in connection with the AD2-029 project. Such costs may include, but are not limited to, any transmission system assets currently in DPL's rate base that are prematurely retired due to the AD2-029 project. PJM shall work with DPL to identify these retirement costs and any additional expenses. DPL reserves the right to reassess issues presented in this document and, upon appropriate justification, submit additional costs related to the AD2-029 project.

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact. It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DP&L - DP&L) The CHURCH-TOWNSEND 138 kV line (from bus 232100 to bus 232107 ckt 1) loads from 123.55% to 124.83% (**DC power flow**) of its emergency rating (348 MVA) for the tower

line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'

/* #1 & #2 KEENEY-STEELE

230

OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1

OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	5.57
932162	AC2-023 E	4.05
933641	AC2-186 C	0.73
933642	AC2-186 E	1.19
933651	AC2-187 C	1.46
933652	AC2-187 E	2.38
933661	AC2-188 C	1.46
933662	AC2-188 E	2.38
935121	AD1-145	1.83
935131	AD1-146 C	0.68
935132	AD1-146 E	1.11
936021	AD2-004 O1	153.22
936231	AD2-029 C	1.82
936232	AD2-029 E	2.65
936351	AD2-045 C O1	5.1
936352	AD2-045 E O1	3.26
936611	AD2-076 C O1	7.35
936612	AD2-076 E O1	11.99
936691	AD2-088 C O1	3.52
936692	AD2-088 E O1	2.35
LTF	AMIL	0.05
LTF	BAYOU	0.19
LTF	BIG_CAJUN1	0.3
LTF	BIG_CAJUN2	0.6
LTF	BLUEG	0.32
LTF	CALDERWOOD	0.1
LTF	CANNELTON	0.06
LTF	CARR	0.06
LTF	CATAWBA	0.06
LTF	CELEVELAND	0.19
LTF	CHEOAH	0.09
LTF	CHILHOWEE	0.03
LTF	CHOCTAW	0.2
LTF	CLIFTY	1.3
LTF	COTTONWOOD	0.76
LTF	DEARBORN	0.16

232902	<i>EASTMUNI</i>	4.18
<i>LTF</i>	<i>EDWARDS</i>	0.1
<i>LTF</i>	<i>ELMERSMITH</i>	0.16
<i>LTF</i>	<i>FARMERCITY</i>	0.06
<i>LTF</i>	<i>G-007</i>	0.02
<i>LTF</i>	<i>GIBSON</i>	0.11
<i>LTF</i>	<i>HAMLET</i>	0.21
<i>LTF</i>	<i>MORGAN</i>	0.32
<i>LTF</i>	<i>NEWTON</i>	0.24
232910	<i>NRG_G1</i>	2.05
232911	<i>NRG_G2</i>	2.05
<i>LTF</i>	<i>O-066</i>	0.19
<i>LTF</i>	<i>PRAIRIE</i>	0.47
<i>LTF</i>	<i>RENSSELAER</i>	0.05
<i>LTF</i>	<i>ROSETON</i>	0.33
<i>LTF</i>	<i>ROWAN</i>	0.13
<i>LTF</i>	<i>SANTEETLA</i>	0.03
<i>LTF</i>	<i>SMITHLAND</i>	0.04
<i>LTF</i>	<i>TATANKA</i>	0.11
<i>LTF</i>	<i>TILTON</i>	0.11
<i>LTF</i>	<i>TRIMBLE</i>	0.06
<i>LTF</i>	<i>TVA</i>	0.14
<i>LTF</i>	<i>UNIONPOWER</i>	0.14
904210	<i>V4-022C</i>	0.38
904212	<i>V4-022E</i>	0.61
232919	<i>VN10</i>	0.63
901004	<i>W1-003 E</i>	0.9
901014	<i>W1-004 E</i>	0.9
901024	<i>W1-005 E</i>	0.9
901034	<i>W1-006 E</i>	0.9
907052	<i>X1-032 E</i>	0.8
910571	<i>X3-008 C</i>	0.37
910572	<i>X3-008 E</i>	3.05
910821	<i>X3-066 C</i>	0.19
910822	<i>X3-066 E</i>	1.57
913361	<i>Y1-079 C</i>	0.28
913362	<i>Y1-079 E</i>	2.29
913411	<i>Y1-080 C</i>	0.06
913412	<i>Y1-080 E</i>	0.48
915542	<i>Y3-058 E</i>	1.92
917082	<i>Z2-012 E</i>	2.45
917432	<i>Z2-076 E</i>	0.37
917442	<i>Z2-077 E</i>	0.37
917581	<i>Z2-097 C</i>	0.33
917582	<i>Z2-097 E</i>	0.69

918432	AA1-059 E	0.34
918832	AA1-102 E	18.74
920312	AA2-129 E	3.96
930201	AB1-056 C	11.43
930202	AB1-056 E	32.54
930211	AB1-057 C	11.6
930212	AB1-057 E	33.07
930881	AB1-137 C	0.76
930882	AB1-137 E	0.32
930921	AB1-141 C	5.88
930922	AB1-141 E	2.74
930931	AB1-142 C	5.88
930932	AB1-142 E	2.74
931111	AB1-162 C	2.67
931112	AB1-162 E	4.37
931261	AB1-176 C	1.43
931262	AB1-176 E	2.36
923921	AB2-032 C	5.92
923922	AB2-032 E	2.79
923951	AB2-036 C	12.59
923952	AB2-036 E	20.59
923961	AB2-037 C	19.69
923962	AB2-037 E	32.17
924191	AB2-063 C	3.2
924192	AB2-063 E	5.23
924361	AB2-084 C	0.76
924362	AB2-084 E	1.24
924681	AB2-120 C	7.5
924682	AB2-120 E	12.23
924781	AB2-130 C OI	6.31
924782	AB2-130 E OI	10.3
924801	AB2-133 C OI	11.57
924802	AB2-133 E OI	14.67
924821	AB2-135 C	12.3
924822	AB2-135 E	14.03
924831	AB2-136 C	5.82
924832	AB2-136 E	6.17
924971	AB2-153 C	3.31
924972	AB2-153 E	5.4
925091	AB2-166 C	0.4
925092	AB2-166 E	0.7
925151	AB2-172 C	4.68
925152	AB2-172 E	7.63
925261	AB2-180 C	2.89
925262	AB2-180 E	1.24

925271	AB2-185 C	5.16
925272	AB2-185 E	2.21
925651	AC1-041 C	0.37
925652	AC1-041 E	0.61
925731	AC1-049 C	0.28
925732	AC1-049 E	0.45
925741	AC1-050 C	0.41
925742	AC1-050 E	0.65
926721	AC1-154 C	0.53
926722	AC1-154 E	0.87
926911	AC1-177	0.81
927031	AC1-190 C	8.54
927032	AC1-190 E	3.66
927191	AC1-213 C	0.64
927192	AC1-213 E	0.42
927241	AC1-220 C	6.57
927242	AC1-220 E	4.61
927321	AC1-229 C	0.68
927322	AC1-229 E	1.1

Appendix 2

(DP&L - DP&L) The MIDLTNTP-MT PLSNT 138 kV line (from bus 232106 to bus 232104 ckt 1) loads from 119.6% to 120.89% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'

/* #1 & #2 KEENEY-STEELE

230

OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1

OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	5.57
932162	AC2-023 E	4.05
933641	AC2-186 C	0.73
933642	AC2-186 E	1.19
933651	AC2-187 C	1.46
933652	AC2-187 E	2.38
933661	AC2-188 C	1.46
933662	AC2-188 E	2.38
935121	AD1-145	1.83
935131	AD1-146 C	0.68
935132	AD1-146 E	1.11
936021	AD2-004 O1	153.22
936231	AD2-029 C	1.82
936232	AD2-029 E	2.65
936351	AD2-045 C O1	5.1
936352	AD2-045 E O1	3.26
936611	AD2-076 C O1	7.35
936612	AD2-076 E O1	11.99
936691	AD2-088 C O1	3.52
936692	AD2-088 E O1	2.35
LTF	AMIL	0.05
LTF	BAYOU	0.19
LTF	BIG_CAJUN1	0.3
LTF	BIG_CAJUN2	0.6
LTF	BLUEG	0.32
LTF	CALDERWOOD	0.1
LTF	CANNELTON	0.06
LTF	CARR	0.06
LTF	CATAWBA	0.06
LTF	CELEVELAND	0.19
LTF	CHEOAH	0.09
LTF	CHILHOWEE	0.03

<i>LTF</i>	<i>CHOCTAW</i>	<i>0.2</i>
<i>LTF</i>	<i>CLIFTY</i>	<i>1.3</i>
<i>LTF</i>	<i>COTTONWOOD</i>	<i>0.76</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.16</i>
<i>232902</i>	<i>EASTMUNI</i>	<i>4.18</i>
<i>LTF</i>	<i>EDWARDS</i>	<i>0.1</i>
<i>LTF</i>	<i>ELMERSMITH</i>	<i>0.16</i>
<i>LTF</i>	<i>FARMERCITY</i>	<i>0.06</i>
<i>LTF</i>	<i>G-007</i>	<i>0.02</i>
<i>LTF</i>	<i>GIBSON</i>	<i>0.11</i>
<i>LTF</i>	<i>HAMLET</i>	<i>0.21</i>
<i>LTF</i>	<i>MORGAN</i>	<i>0.32</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.24</i>
<i>232910</i>	<i>NRG_G1</i>	<i>2.05</i>
<i>232911</i>	<i>NRG_G2</i>	<i>2.05</i>
<i>LTF</i>	<i>O-066</i>	<i>0.19</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.47</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.05</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.33</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.13</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.03</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.04</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.11</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.11</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.06</i>
<i>LTF</i>	<i>TVA</i>	<i>0.14</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.14</i>
<i>904210</i>	<i>V4-022C</i>	<i>0.38</i>
<i>904212</i>	<i>V4-022E</i>	<i>0.61</i>
<i>232919</i>	<i>VN10</i>	<i>0.63</i>
<i>901004</i>	<i>W1-003 E</i>	<i>0.9</i>
<i>901014</i>	<i>W1-004 E</i>	<i>0.9</i>
<i>901024</i>	<i>W1-005 E</i>	<i>0.9</i>
<i>901034</i>	<i>W1-006 E</i>	<i>0.9</i>
<i>907052</i>	<i>X1-032 E</i>	<i>0.8</i>
<i>910571</i>	<i>X3-008 C</i>	<i>0.37</i>
<i>910572</i>	<i>X3-008 E</i>	<i>3.05</i>
<i>910821</i>	<i>X3-066 C</i>	<i>0.19</i>
<i>910822</i>	<i>X3-066 E</i>	<i>1.57</i>
<i>913361</i>	<i>Y1-079 C</i>	<i>0.28</i>
<i>913362</i>	<i>Y1-079 E</i>	<i>2.29</i>
<i>913411</i>	<i>Y1-080 C</i>	<i>0.06</i>
<i>913412</i>	<i>Y1-080 E</i>	<i>0.48</i>
<i>915542</i>	<i>Y3-058 E</i>	<i>1.92</i>
<i>917082</i>	<i>Z2-012 E</i>	<i>2.45</i>

917432	Z2-076 E	0.37
917442	Z2-077 E	0.37
917581	Z2-097 C	0.33
917582	Z2-097 E	0.69
918432	AA1-059 E	0.34
918832	AA1-102 E	18.74
920312	AA2-129 E	3.96
930201	AB1-056 C	11.43
930202	AB1-056 E	32.54
930211	AB1-057 C	11.6
930212	AB1-057 E	33.07
930881	AB1-137 C	0.76
930882	AB1-137 E	0.32
930921	AB1-141 C	5.88
930922	AB1-141 E	2.74
930931	AB1-142 C	5.88
930932	AB1-142 E	2.74
931111	AB1-162 C	2.67
931112	AB1-162 E	4.37
931261	AB1-176 C	1.43
931262	AB1-176 E	2.36
923921	AB2-032 C	5.92
923922	AB2-032 E	2.79
923951	AB2-036 C	12.59
923952	AB2-036 E	20.59
923961	AB2-037 C	19.69
923962	AB2-037 E	32.17
924191	AB2-063 C	3.2
924192	AB2-063 E	5.23
924361	AB2-084 C	0.76
924362	AB2-084 E	1.24
924681	AB2-120 C	7.5
924682	AB2-120 E	12.23
924781	AB2-130 C OI	6.31
924782	AB2-130 E OI	10.3
924801	AB2-133 C OI	11.57
924802	AB2-133 E OI	14.67
924821	AB2-135 C	12.3
924822	AB2-135 E	14.03
924831	AB2-136 C	5.82
924832	AB2-136 E	6.17
924971	AB2-153 C	3.31
924972	AB2-153 E	5.4
925091	AB2-166 C	0.4
925092	AB2-166 E	0.7

925151	AB2-172 C	4.68
925152	AB2-172 E	7.63
925251	AB2-179 C	26.91
925252	AB2-179 E	8.87
925261	AB2-180 C	2.89
925262	AB2-180 E	1.24
925271	AB2-185 C	5.16
925272	AB2-185 E	2.21
925651	AC1-041 C	0.37
925652	AC1-041 E	0.61
925731	AC1-049 C	0.28
925732	AC1-049 E	0.45
925741	AC1-050 C	0.41
925742	AC1-050 E	0.65
926721	AC1-154 C	0.53
926722	AC1-154 E	0.87
926911	AC1-177	0.81
927031	AC1-190 C	8.54
927032	AC1-190 E	3.66
927191	AC1-213 C	0.64
927192	AC1-213 E	0.42
927241	AC1-220 C	6.57
927242	AC1-220 E	4.61
927321	AC1-229 C	0.68
927322	AC1-229 E	1.1

Appendix 3

(DP&L - DP&L) The TOWNSEND-MIDLTNTP 138 kV line (from bus 232107 to bus 232106 ckt 1) loads from 130.04% to 131.32% (**DC power flow**) of its emergency rating (348 MVA) for the tower line contingency outage of 'DPL_P7_1_DBL_1NCB_A'. This project contributes approximately 4.48 MW to the thermal violation.

CONTINGENCY 'DPL_P7_1_DBL_1NCB_A'

/* #1 & #2 KEENEY-STEELE

230

OPEN LINE FROM BUS 231003 TO BUS 232000 CKT 1

OPEN LINE FROM BUS 231003 TO BUS 923960 CKT 2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	5.57
932162	AC2-023 E	4.05
933641	AC2-186 C	0.73
933642	AC2-186 E	1.19
933651	AC2-187 C	1.46
933652	AC2-187 E	2.38
933661	AC2-188 C	1.46
933662	AC2-188 E	2.38
935121	AD1-145	1.83
935131	AD1-146 C	0.68
935132	AD1-146 E	1.11
936021	AD2-004 O1	153.22
936231	AD2-029 C	1.82
936232	AD2-029 E	2.65
936351	AD2-045 C O1	5.1
936352	AD2-045 E O1	3.26
936611	AD2-076 C O1	7.35
936612	AD2-076 E O1	11.99
936691	AD2-088 C O1	3.52
936692	AD2-088 E O1	2.35
LTF	AMIL	0.05
LTF	BAYOU	0.19
LTF	BIG_CAJUN1	0.3
LTF	BIG_CAJUN2	0.6
LTF	BLUEG	0.32
LTF	CALDERWOOD	0.1
LTF	CANNELTON	0.06
LTF	CARR	0.06
LTF	CATAWBA	0.06
LTF	CELEVELAND	0.19
LTF	CHEOAH	0.09
LTF	CHILHOWEE	0.03

<i>LTF</i>	<i>CHOCTAW</i>	<i>0.2</i>
<i>LTF</i>	<i>CLIFTY</i>	<i>1.3</i>
<i>LTF</i>	<i>COTTONWOOD</i>	<i>0.76</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.16</i>
<i>232902</i>	<i>EASTMUNI</i>	<i>4.18</i>
<i>LTF</i>	<i>EDWARDS</i>	<i>0.1</i>
<i>LTF</i>	<i>ELMERSMITH</i>	<i>0.16</i>
<i>LTF</i>	<i>FARMERCITY</i>	<i>0.06</i>
<i>LTF</i>	<i>G-007</i>	<i>0.02</i>
<i>LTF</i>	<i>GIBSON</i>	<i>0.11</i>
<i>LTF</i>	<i>HAMLET</i>	<i>0.21</i>
<i>LTF</i>	<i>MORGAN</i>	<i>0.32</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.24</i>
<i>232910</i>	<i>NRG_G1</i>	<i>2.05</i>
<i>232911</i>	<i>NRG_G2</i>	<i>2.05</i>
<i>LTF</i>	<i>O-066</i>	<i>0.19</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.47</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.05</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.33</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.13</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.03</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.04</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.11</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.11</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.06</i>
<i>LTF</i>	<i>TVA</i>	<i>0.14</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.14</i>
<i>904210</i>	<i>V4-022C</i>	<i>0.38</i>
<i>904212</i>	<i>V4-022E</i>	<i>0.61</i>
<i>232919</i>	<i>VN10</i>	<i>0.63</i>
<i>901004</i>	<i>W1-003 E</i>	<i>0.9</i>
<i>901014</i>	<i>W1-004 E</i>	<i>0.9</i>
<i>901024</i>	<i>W1-005 E</i>	<i>0.9</i>
<i>901034</i>	<i>W1-006 E</i>	<i>0.9</i>
<i>907052</i>	<i>X1-032 E</i>	<i>0.8</i>
<i>910571</i>	<i>X3-008 C</i>	<i>0.37</i>
<i>910572</i>	<i>X3-008 E</i>	<i>3.05</i>
<i>910821</i>	<i>X3-066 C</i>	<i>0.19</i>
<i>910822</i>	<i>X3-066 E</i>	<i>1.57</i>
<i>913361</i>	<i>Y1-079 C</i>	<i>0.28</i>
<i>913362</i>	<i>Y1-079 E</i>	<i>2.29</i>
<i>913411</i>	<i>Y1-080 C</i>	<i>0.06</i>
<i>913412</i>	<i>Y1-080 E</i>	<i>0.48</i>
<i>915542</i>	<i>Y3-058 E</i>	<i>1.92</i>
<i>917082</i>	<i>Z2-012 E</i>	<i>2.45</i>

917432	Z2-076 E	0.37
917442	Z2-077 E	0.37
917581	Z2-097 C	0.33
917582	Z2-097 E	0.69
918432	AA1-059 E	0.34
918832	AA1-102 E	18.74
920312	AA2-129 E	3.96
930201	AB1-056 C	11.43
930202	AB1-056 E	32.54
930211	AB1-057 C	11.6
930212	AB1-057 E	33.07
930881	AB1-137 C	0.76
930882	AB1-137 E	0.32
930921	AB1-141 C	5.88
930922	AB1-141 E	2.74
930931	AB1-142 C	5.88
930932	AB1-142 E	2.74
931111	AB1-162 C	2.67
931112	AB1-162 E	4.37
931261	AB1-176 C	1.43
931262	AB1-176 E	2.36
923921	AB2-032 C	5.92
923922	AB2-032 E	2.79
923951	AB2-036 C	12.59
923952	AB2-036 E	20.59
923961	AB2-037 C	19.69
923962	AB2-037 E	32.17
924191	AB2-063 C	3.2
924192	AB2-063 E	5.23
924361	AB2-084 C	0.76
924362	AB2-084 E	1.24
924681	AB2-120 C	7.5
924682	AB2-120 E	12.23
924781	AB2-130 C OI	6.31
924782	AB2-130 E OI	10.3
924801	AB2-133 C OI	11.57
924802	AB2-133 E OI	14.67
924821	AB2-135 C	12.3
924822	AB2-135 E	14.03
924831	AB2-136 C	5.82
924832	AB2-136 E	6.17
924971	AB2-153 C	3.31
924972	AB2-153 E	5.4
925091	AB2-166 C	0.4
925092	AB2-166 E	0.7

925151	AB2-172 C	4.68
925152	AB2-172 E	7.63
925251	AB2-179 C	26.91
925252	AB2-179 E	8.87
925261	AB2-180 C	2.89
925262	AB2-180 E	1.24
925271	AB2-185 C	5.16
925272	AB2-185 E	2.21
925651	AC1-041 C	0.37
925652	AC1-041 E	0.61
925731	AC1-049 C	0.28
925732	AC1-049 E	0.45
925741	AC1-050 C	0.41
925742	AC1-050 E	0.65
926721	AC1-154 C	0.53
926722	AC1-154 E	0.87
926911	AC1-177	0.81
927031	AC1-190 C	8.54
927032	AC1-190 E	3.66
927191	AC1-213 C	0.64
927192	AC1-213 E	0.42
927241	AC1-220 C	6.57
927242	AC1-220 E	4.61
927321	AC1-229 C	0.68
927322	AC1-229 E	1.1

Appendix 4

(DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 162.43% to 167.92% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP11'. This project contributes approximately 5.11 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP11'
MILFORD

/*STEELE BUS BREAKER TO

DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1
STEELE 230 230

/*MILFORD

DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
004 TAP 230 230

/*STEELE AD2-

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	4.32
932162	AC2-023 E	3.14
935121	AD1-145	0.98
935131	AD1-146 C	0.29
935132	AD1-146 E	0.47
936021	AD2-004 O1	86.5
936231	AD2-029 C	2.08
936232	AD2-029 E	3.03
936691	AD2-088 C O1	2.09
936692	AD2-088 E O1	1.4
LTF	AMIL	0.02
LTF	BAYOU	0.07
LTF	BIG_CAJUN1	0.11
LTF	BIG_CAJUN2	0.23
LTF	BLUEG	0.12
LTF	CALDERWOOD	0.04
LTF	CANNELTON	0.02
LTF	CARR	0.02
LTF	CATAWBA	0.02
LTF	CELEVELAND	0.07
LTF	CHEOAH	0.04
LTF	CHILHOWEE	0.01
LTF	CHOCTAW	0.08
LTF	CLIFTY	0.51
LTF	COTTONWOOD	0.3
LTF	DEARBORN	0.06
LTF	EDWARDS	0.04
LTF	ELMERSMITH	0.06
LTF	FARMERCITY	0.02
LTF	G-007	0.03

<i>LTF</i>	<i>GIBSON</i>	<i>0.04</i>
<i>LTF</i>	<i>HAMLET</i>	<i>0.08</i>
<i>LTF</i>	<i>MORGAN</i>	<i>0.12</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.09</i>
<i>LTF</i>	<i>O-066</i>	<i>0.12</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.18</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.02</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.13</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.05</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.01</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.01</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.04</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.04</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.02</i>
<i>LTF</i>	<i>TVA</i>	<i>0.06</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.06</i>
<i>904210</i>	<i>V4-022C</i>	<i>0.21</i>
<i>904212</i>	<i>V4-022E</i>	<i>0.34</i>
<i>232919</i>	<i>VN10</i>	<i>0.6</i>
<i>901004</i>	<i>W1-003 E</i>	<i>0.5</i>
<i>901014</i>	<i>W1-004 E</i>	<i>0.5</i>
<i>901024</i>	<i>W1-005 E</i>	<i>0.5</i>
<i>901034</i>	<i>W1-006 E</i>	<i>0.5</i>
<i>907052</i>	<i>X1-032 E</i>	<i>0.46</i>
<i>910571</i>	<i>X3-008 C</i>	<i>0.57</i>
<i>910572</i>	<i>X3-008 E</i>	<i>4.74</i>
<i>913411</i>	<i>Y1-080 C</i>	<i>0.07</i>
<i>913412</i>	<i>Y1-080 E</i>	<i>0.55</i>
<i>915541</i>	<i>Y3-058 C</i>	<i>0.17</i>
<i>915542</i>	<i>Y3-058 E</i>	<i>1.38</i>
<i>917082</i>	<i>Z2-012 E</i>	<i>1.37</i>
<i>917432</i>	<i>Z2-076 E</i>	<i>0.17</i>
<i>917442</i>	<i>Z2-077 E</i>	<i>0.17</i>
<i>918432</i>	<i>AA1-059 E</i>	<i>0.2</i>
<i>918832</i>	<i>AA1-102 E</i>	<i>10.78</i>
<i>920312</i>	<i>AA2-129 E</i>	<i>2.2</i>
<i>930201</i>	<i>AB1-056 C</i>	<i>4.65</i>
<i>930202</i>	<i>AB1-056 E</i>	<i>13.25</i>
<i>930211</i>	<i>AB1-057 C</i>	<i>4.73</i>
<i>930212</i>	<i>AB1-057 E</i>	<i>13.47</i>
<i>930881</i>	<i>AB1-137 C</i>	<i>0.33</i>
<i>930882</i>	<i>AB1-137 E</i>	<i>0.14</i>
<i>924361</i>	<i>AB2-084 C</i>	<i>0.43</i>
<i>924362</i>	<i>AB2-084 E</i>	<i>0.71</i>
<i>924681</i>	<i>AB2-120 C</i>	<i>4.15</i>

924682	<i>AB2-120 E</i>	6.77
924781	<i>AB2-130 C OI</i>	3.76
924782	<i>AB2-130 E OI</i>	6.13
924831	<i>AB2-136 C</i>	7.4
924832	<i>AB2-136 E</i>	7.85
925091	<i>AB2-166 C</i>	0.25
925092	<i>AB2-166 E</i>	0.44
925151	<i>AB2-172 C</i>	7.26
925152	<i>AB2-172 E</i>	11.85
925261	<i>AB2-180 C</i>	2.08
925262	<i>AB2-180 E</i>	0.89
925651	<i>AC1-041 C</i>	0.21
925652	<i>AC1-041 E</i>	0.34
925731	<i>AC1-049 C</i>	0.13
925732	<i>AC1-049 E</i>	0.21
925741	<i>AC1-050 C</i>	0.35
925742	<i>AC1-050 E</i>	0.55
926911	<i>AC1-177</i>	0.46
927031	<i>AC1-190 C</i>	12.84
927032	<i>AC1-190 E</i>	5.5
927191	<i>AC1-213 C</i>	0.41
927192	<i>AC1-213 E</i>	0.27
927321	<i>AC1-229 C</i>	0.29
927322	<i>AC1-229 E</i>	0.47

Appendix 5

(DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 168.23% to 173.73% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP11'. This project contributes approximately 5.11 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP11'
MILFORD

/*STEELE BUS BREAKER TO

DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1
STEELE 230 230

/*MILFORD

DISCONNECT BRANCH FROM BUS 232000 TO BUS 936020 CKT 1
004 TAP 230 230

/*STEELE AD2-

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	4.32
932162	AC2-023 E	3.14
935121	AD1-145	0.98
935131	AD1-146 C	0.29
935132	AD1-146 E	0.47
936021	AD2-004 O1	86.5
936231	AD2-029 C	2.08
936232	AD2-029 E	3.03
936691	AD2-088 C O1	2.09
936692	AD2-088 E O1	1.4
LTF	AMIL	0.02
LTF	BAYOU	0.07
LTF	BIG_CAJUN1	0.11
LTF	BIG_CAJUN2	0.23
LTF	BLUEG	0.12
LTF	CALDERWOOD	0.04
LTF	CANNELTON	0.02
LTF	CARR	0.02
LTF	CATAWBA	0.02
LTF	CELEVELAND	0.07
LTF	CHEOAH	0.04
LTF	CHILHOWEE	0.01
LTF	CHOCTAW	0.08
LTF	CLIFTY	0.51
LTF	COTTONWOOD	0.3
LTF	DEARBORN	0.06
LTF	EDWARDS	0.04
LTF	ELMERSMITH	0.06
LTF	FARMERCITY	0.02
LTF	G-007	0.03

<i>LTF</i>	<i>GIBSON</i>	<i>0.04</i>
<i>LTF</i>	<i>HAMLET</i>	<i>0.08</i>
<i>LTF</i>	<i>MORGAN</i>	<i>0.12</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.09</i>
<i>LTF</i>	<i>O-066</i>	<i>0.12</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.18</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.02</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.13</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.05</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.01</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.01</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.04</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.04</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.02</i>
<i>LTF</i>	<i>TVA</i>	<i>0.06</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.06</i>
<i>904210</i>	<i>V4-022C</i>	<i>0.21</i>
<i>904212</i>	<i>V4-022E</i>	<i>0.34</i>
<i>232919</i>	<i>VN10</i>	<i>0.6</i>
<i>901004</i>	<i>W1-003 E</i>	<i>0.5</i>
<i>901014</i>	<i>W1-004 E</i>	<i>0.5</i>
<i>901024</i>	<i>W1-005 E</i>	<i>0.5</i>
<i>901034</i>	<i>W1-006 E</i>	<i>0.5</i>
<i>907052</i>	<i>X1-032 E</i>	<i>0.46</i>
<i>910571</i>	<i>X3-008 C</i>	<i>0.57</i>
<i>910572</i>	<i>X3-008 E</i>	<i>4.74</i>
<i>913411</i>	<i>Y1-080 C</i>	<i>0.07</i>
<i>913412</i>	<i>Y1-080 E</i>	<i>0.55</i>
<i>915541</i>	<i>Y3-058 C</i>	<i>0.17</i>
<i>915542</i>	<i>Y3-058 E</i>	<i>1.38</i>
<i>917082</i>	<i>Z2-012 E</i>	<i>1.37</i>
<i>917432</i>	<i>Z2-076 E</i>	<i>0.17</i>
<i>917442</i>	<i>Z2-077 E</i>	<i>0.17</i>
<i>918432</i>	<i>AA1-059 E</i>	<i>0.2</i>
<i>918832</i>	<i>AA1-102 E</i>	<i>10.78</i>
<i>920312</i>	<i>AA2-129 E</i>	<i>2.2</i>
<i>930201</i>	<i>AB1-056 C</i>	<i>4.65</i>
<i>930202</i>	<i>AB1-056 E</i>	<i>13.25</i>
<i>930211</i>	<i>AB1-057 C</i>	<i>4.73</i>
<i>930212</i>	<i>AB1-057 E</i>	<i>13.47</i>
<i>930881</i>	<i>AB1-137 C</i>	<i>0.33</i>
<i>930882</i>	<i>AB1-137 E</i>	<i>0.14</i>
<i>924361</i>	<i>AB2-084 C</i>	<i>0.43</i>
<i>924362</i>	<i>AB2-084 E</i>	<i>0.71</i>
<i>924681</i>	<i>AB2-120 C</i>	<i>4.15</i>

924682	<i>AB2-120 E</i>	6.77
924781	<i>AB2-130 C OI</i>	3.76
924782	<i>AB2-130 E OI</i>	6.13
924831	<i>AB2-136 C</i>	7.4
924832	<i>AB2-136 E</i>	7.85
925091	<i>AB2-166 C</i>	0.25
925092	<i>AB2-166 E</i>	0.44
925151	<i>AB2-172 C</i>	7.26
925152	<i>AB2-172 E</i>	11.85
925261	<i>AB2-180 C</i>	2.08
925262	<i>AB2-180 E</i>	0.89
925651	<i>AC1-041 C</i>	0.21
925652	<i>AC1-041 E</i>	0.34
925731	<i>AC1-049 C</i>	0.13
925732	<i>AC1-049 E</i>	0.21
925741	<i>AC1-050 C</i>	0.35
925742	<i>AC1-050 E</i>	0.55
926911	<i>AC1-177</i>	0.46
927031	<i>AC1-190 C</i>	12.84
927032	<i>AC1-190 E</i>	5.5
927191	<i>AC1-213 C</i>	0.41
927192	<i>AC1-213 E</i>	0.27
927321	<i>AC1-229 C</i>	0.29
927322	<i>AC1-229 E</i>	0.47

Appendix 6

(DP&L - DP&L) The VIENN_69-SHARPTWN 69 kV line (from bus 232241 to bus 232239 ckt 1) loads from 126.74% to 133.69% (**DC power flow**) of its emergency rating (42 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP36'. This project contributes approximately 2.92 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP36'
TO IR 2

/*COOL SPRINGS BUS BREAKER

DISCONNECT BRANCH FROM BUS 232001 TO BUS 232006 CKT 1
INDRIV 4 230 230

/*COOL SPRINGS

DISCONNECT BRANCH FROM BUS 232001 TO BUS 232004 CKT 1
MILFORD 230 230

/*COOL SPRINGS

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	1.7
932162	AC2-023 E	1.24
936231	AD2-029 C	1.19
936232	AD2-029 E	1.73
LTF	CARR	< 0.01
LTF	G-007	< 0.01
LTF	O-066	0.02
LTF	RENSSELAER	< 0.01
LTF	ROSETON	< 0.01
232919	VN10	0.45
910571	X3-008 C	0.19
910572	X3-008 E	1.55
913411	Y1-080 C	0.04
913412	Y1-080 E	0.31
924831	AB2-136 C	3.53
924832	AB2-136 E	3.75
925151	AB2-172 C	2.38
925152	AB2-172 E	3.89
925741	AC1-050 C	0.19
925742	AC1-050 E	0.31
927031	AC1-190 C	4.49
927032	AC1-190 E	1.93

Appendix 7

(DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 114.74% to 116.89% (**DC power flow**) of its emergency rating (58 MVA) for the single line contingency outage of 'DPL_P1_2_CKT 6728'. This project contributes approximately 1.24 MW to the thermal violation.

CONTINGENCY 'DPL_P1_2_CKT 6728'

OPEN LINE FROM BUS 232272 TO BUS 232274 CIRCUIT 1 /MOUNT HERMON -
PINEY GROVE 69

DISCONNECT BUS 230912

/ PINEY GROVE 69 CAP

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	14.15
936021	AD2-004 O1	3.54
936231	AD2-029 C	1.24
LTF	CBM-N	< 0.01
LTF	CBM-S1	0.02
LTF	CBM-S2	0.02
LTF	CBM-W1	0.07
LTF	CBM-W2	0.11
LTF	CIN	0.01
LTF	CPLE	< 0.01
LTF	IPL	< 0.01
LTF	LGEE	< 0.01
LTF	MEC	0.03
LTF	MECS	0.02
LTF	NYISO	0.02
LTF	O-066A	< 0.01
LTF	VFT	< 0.01
232919	VN10	0.47
LTF	WEC	< 0.01
910571	X3-008 C	0.19
913411	Y1-080 C	0.04
915541	Y3-058 C	0.72
924831	AB2-136 C	3.68
925091	AB2-166 C	-0.32
925151	AB2-172 C	2.47
925261	AB2-180 C	8.94
925741	AC1-050 C	0.75
927031	AC1-190 C	4.67

Appendix 8

(DP&L - DP&L) The AD2-004 TAP-STEELE 230 kV line (from bus 936020 to bus 232000 ckt 1) loads from 141.96% to 142.58% (**DC power flow**) of its emergency rating (551 MVA) for the line fault with failed breaker contingency outage of 'DPL_P4-2_DP59'. This project contributes approximately 7.63 MW to the thermal violation.

CONTINGENCY 'DPL_P4-2_DP59' /*PINEY GROVE BUS BREAKER
 DISCONNECT BRANCH FROM BUS 232131 TO BUS 924680 CKT 1 /*PINEY GROVE
 AB2-120 TAP 138 138
 DISCONNECT BRANCH FROM BUS 232007 TO BUS 232128 CKT 1 /*PINEY GROVE
 PINEY GROVE 230 138
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
932161	AC2-023 C	10.65
932162	AC2-023 E	7.75
935121	AD1-145	2.16
935131	AD1-146 C	0.52
935132	AD1-146 E	0.84
936021	AD2-004 O1	559.76
936231	AD2-029 C	3.11
936232	AD2-029 E	4.52
936691	AD2-088 C O1	4.8
936692	AD2-088 E O1	3.2
LTF	AMIL	0.07
LTF	BAYOU	0.24
LTF	BIG_CAJUN1	0.37
LTF	BIG_CAJUN2	0.74
LTF	BLUEG	0.4
LTF	CALDERWOOD	0.12
LTF	CANNELTON	0.07
LTF	CARR	0.08
LTF	CATAWBA	0.08
LTF	CELEVELAND	0.23
LTF	CHEOAH	0.11
LTF	CHILHOWEE	0.04
LTF	CHOCTAW	0.24
LTF	CLIFTY	1.63
LTF	COTTONWOOD	0.95
232926	CRISFLD1	0.97
LTF	DEARBORN	0.2
LTF	EDWARDS	0.12
LTF	ELMERSMITH	0.2
LTF	FARMERCITY	0.08
LTF	G-007	0.19

<i>LTF</i>	<i>GIBSON</i>	<i>0.13</i>
<i>LTF</i>	<i>HAMLET</i>	<i>0.26</i>
<i>LTF</i>	<i>MORGAN</i>	<i>0.4</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.3</i>
<i>LTF</i>	<i>O-066</i>	<i>0.67</i>
<i>232912</i>	<i>OH NUG1</i>	<i>4.32</i>
<i>232913</i>	<i>OH NUG2</i>	<i>4.26</i>
<i>232914</i>	<i>OH NUG3</i>	<i>4.32</i>
<i>232915</i>	<i>OH NUG4</i>	<i>4.32</i>
<i>232916</i>	<i>OH NUG5</i>	<i>4.32</i>
<i>232917</i>	<i>OH NUG6</i>	<i>4.3</i>
<i>232918</i>	<i>OH NUG7</i>	<i>4.29</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.59</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.06</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.46</i>
<i>LTF</i>	<i>ROWAN</i>	<i>0.16</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.03</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.05</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.14</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.14</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.08</i>
<i>LTF</i>	<i>TVA</i>	<i>0.18</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>0.18</i>
<i>904210</i>	<i>V4-022C</i>	<i>0.92</i>
<i>904212</i>	<i>V4-022E</i>	<i>1.51</i>
<i>232907</i>	<i>VN8</i>	<i>17.06</i>
<i>901003</i>	<i>W1-003 C</i>	<i>1.49</i>
<i>901004</i>	<i>W1-003 E</i>	<i>2.21</i>
<i>901013</i>	<i>W1-004 C</i>	<i>1.49</i>
<i>901014</i>	<i>W1-004 E</i>	<i>2.21</i>
<i>901023</i>	<i>W1-005 C</i>	<i>1.49</i>
<i>901024</i>	<i>W1-005 E</i>	<i>2.21</i>
<i>901033</i>	<i>W1-006 C</i>	<i>1.49</i>
<i>901034</i>	<i>W1-006 E</i>	<i>2.21</i>
<i>907052</i>	<i>X1-032 E</i>	<i>1.97</i>
<i>910572</i>	<i>X3-008 E</i>	<i>3.93</i>
<i>913412</i>	<i>Y1-080 E</i>	<i>0.82</i>
<i>915542</i>	<i>Y3-058 E</i>	<i>3.69</i>
<i>917082</i>	<i>Z2-012 E</i>	<i>6.03</i>
<i>917432</i>	<i>Z2-076 E</i>	<i>0.37</i>
<i>917442</i>	<i>Z2-077 E</i>	<i>0.37</i>
<i>918431</i>	<i>AA1-059 C</i>	<i>0.42</i>
<i>918432</i>	<i>AA1-059 E</i>	<i>0.84</i>
<i>918831</i>	<i>AA1-102</i>	<i>3.65</i>
<i>918832</i>	<i>AA1-102 E</i>	<i>45.97</i>

920312	AA2-129 E	9.75
920321	AA2-130	0.19
930881	AB1-137 C	0.61
930882	AB1-137 E	0.26
924361	AB2-084 C	1.87
924362	AB2-084 E	3.05
924681	AB2-120 C	18.28
924682	AB2-120 E	29.83
924781	AB2-130 C OI	8.61
924782	AB2-130 E OI	14.05
924831	AB2-136 C	9.15
924832	AB2-136 E	9.7
925091	AB2-166 C	0.74
925092	AB2-166 E	1.3
925151	AB2-172 C	6.03
925152	AB2-172 E	9.83
925261	AB2-180 C	5.55
925262	AB2-180 E	2.38
925651	AC1-041 C	0.89
925652	AC1-041 E	1.45
925731	AC1-049 C	0.27
925732	AC1-049 E	0.44
925741	AC1-050 C	0.78
925742	AC1-050 E	1.24
926911	AC1-177	1.98
927031	AC1-190 C	11.43
927032	AC1-190 E	4.9
927191	AC1-213 C	1.24
927192	AC1-213 E	0.82
927321	AC1-229 C	0.54
927322	AC1-229 E	0.87