

***Generation Interconnection
Feasibility Study Report***

For

***PJM Generation Interconnection Request
Queue Position AD2-089***

***Anaconda-Tar River 115 kV
45 MW Capacity / 75 MW Energy***

July / 2018

Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

Preface

The intent of the Feasibility Study is to determine a plan, with high level estimated cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the IC. The IC may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the IC may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the Impact Study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by ITO, the costs may be included in the study.

General

The IC has proposed a solar generating facility located in Edgecombe County, North Carolina (Edgecombe County). The installed facilities will have a total capability of **75 MW** with **45 MW** of this output being recognized by PJM as capacity. The proposed in-service date for this project is **12/31/2020**. **This study does not imply an ITO commitment to this in-service date.**

Point of Interconnection (POI)

AD2-089 will interconnect with the ITO transmission system via a tap off of the Anaconda-Tar River 115 kV line. The tap will be 0.5 miles from Anaconda Substation and 1 mile from Tar River Substation on the east side of the N.O. switch near Anaconda. Refer to **Attachment 1**. No secondary POI was analyzed.

Cost Summary

The AD2-089 project will be responsible for the following costs:

Description	Total Cost
Attachment Facilities	\$1,550,000
Direct Connection Network Upgrades	\$6,300,000
Non Direct Connection Network Upgrades ¹	\$ 0
Total Costs	\$7,850,000

In addition, the AD2-089 project may be responsible for a contribution to the following costs:

Description	Total Cost
New System Upgrades	\$ 0
Previously Identified Upgrades	\$184,860,000
Total Costs	\$184,860,000

Cost allocations for these upgrades will be provided in the System Impact Study Report.

Note: PJM Open Access Transmission Tariff (OATT) section 217.3A outline cost allocation rules. The rules are further clarified in PJM Manual 14A Attachment B. The allocation of costs for a network upgrade will start with the first Queue project to cause the need for the upgrade. Later queue projects will receive cost allocation contingent on their contribution to the violation and are allocated to the queues that have not closed less than 5 years following the execution of the first Interconnection Service Agreement which identifies the need for this upgrade.

The Feasibility Study is used to make a preliminary determination of the type and scope of Attachment Facilities, Local Upgrades, and Network Upgrades that will be necessary to accommodate the Interconnection Request and to provide the Interconnection Customer a preliminary estimate of the time that will be required to construct any necessary facilities and upgrades and the Interconnection Customer's cost responsibility. The System Impact Study provides refined and comprehensive estimates of cost responsibility and construction lead times for new facilities and system upgrades. Facilities Studies will include, commensurate with the degree of engineering specificity as provided in the Facilities Study Agreement, good faith estimates of the cost, determined in accordance with Section 217 of the Tariff,

- (a) to be charged to each affected New Service Customer for the Facilities and System Upgrades that are necessary to accommodate this queue project;
- (b) the time required to complete detailed design and construction of the facilities and upgrades; and

¹ See the Non-Direct Connection Cost Estimate section. Remote terminal work will be determined in the Facilities Study phase.

(c) a description of any site-specific environmental issues or requirements that could reasonably be anticipated to affect the cost or time required to complete construction of such facilities and upgrades.

Transmission Owner Scope of Work

Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost \$550,000.

Transmission: Construct approximately one span of 115 kV Attachment line between the generation substation and a new AD2-089 Switching Station. The estimated cost for this work is \$1,000,000.

The estimated total cost of the Attachment Facilities is \$1,550,000. It is estimated to take 18-24 months to complete this work upon execution of an Interconnection Construction Service Agreement (ICSA). These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase. See Attachment One.

Direct Connection Cost Estimate

Substation: Establish the new 115 kV AD2-089 Switching Substation (interconnection substation). The arrangement in the substation will be as shown below on Dominion Attachment One: One-Line Diagram. The estimated cost of this work scope is \$5,500,000.

Transmission: Install transmission structure in-line with transmission line to allow the proposed interconnection switching station to be interconnected with the transmission system. Estimated cost is \$800,000 dollars and is estimated to take 24-30 months to complete. See Attachment One.

The total estimated cost to complete the Direct Connection Network Facilities is \$6,300,000. It is estimated to take 24-36 months to complete this work upon execution of an Interconnection Construction Service Agreement.

Non-Direct Connection Cost Estimate

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

Interconnection Customer Requirements

ITO's Facility Connection Requirements as posted on PJM's website

<http://www.pjm.com/~media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx>

Revenue Metering and SCADA Requirements

PJM Requirements

The IC will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

Meteorological Data Reporting Requirement

The solar generation facility shall provide the Transmission Provider with site-specific meteorological data including:

- Temperature (degrees Fahrenheit)
- Atmospheric pressure (hectopascals)
- Irradiance
- Forced outage data

Network Impacts

The Queue Project AD2-089 was evaluated as a 75.0 MW (Capacity 45.0 MW) injection at the tap of the Anaconda - Tarr River 115 kV line in the VAP area. Project AD2-089 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AD2-089 was studied with a commercial probability of 53%. Potential network impacts were as follows:

PJM assessed the impact of the proposed Queue Project as an injection into the ITO, for compliance with NERC Reliability Criteria. The system was assessed using the summer 2021 RTEP case. When performing analysis, ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under single contingency (normal and stressed system conditions). A full listing of the ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C Contingency Conditions (Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating. The results of these studies are discussed in more detail below.

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
"313845	No Data
"314288	No Data
AEP_P1-2_#1377	CONTINGENCY 'AEP_P1-2_#1377' OPEN BRANCH FROM BUS 242514 TO BUS 242520 CKT 1 / 242514 05J.FERR 765 242520 05J.FERR 500 1 OPEN BRANCH FROM BUS 242520 TO BUS 306719 CKT 1 / 242520 05J.FERR 500 306719 8ANTIOCH 500 1 END
AEP_P4_#7589_05J.FERR 765	CONTINGENCY 'AEP_P4_#7589_05J.FERR 765' OPEN BRANCH FROM BUS 242514 TO BUS 242520 CKT 1 / 242514 05J.FERR 765 242520 05J.FERR 500 1 OPEN BRANCH FROM BUS 242514 TO BUS 242684 CKT 2 / 242514 05J.FERR 765 242684 05J.FERR 138 2 OPEN BRANCH FROM BUS 242520 TO BUS 306719 CKT 1 / 242520 05J.FERR 500 306719 8ANTIOCH 500 1 END
DVP_P1-2: LN 130-A	CONTINGENCY 'DVP_P1-2: LN 130-A' OPEN BRANCH FROM BUS 314562 TO BUS 314570 CKT 1 /* 3CLUBHSE 115.00 - 3METCATP 115.00 OPEN BRANCH FROM BUS 314570 TO BUS 314572 CKT 1 /* 3METCATP 115.00 - 3EMPORIA 115.00 OPEN BRANCH FROM BUS 314570 TO BUS 314588 CKT 1 /* 3METCATP 115.00 - 3METCALF 115.00 OPEN BRANCH FROM BUS 314572 TO BUS 925170 CKT 1 /* 3EMPORIA 115.00 - AB2-174 TAP 115.00 OPEN BRANCH FROM BUS 314572 TO BUS 314863 CKT 1 /* 3EMPORIA 115.00 - 3EMPOR_1 115.00 OPEN BUS 314570 /* ISLAND OPEN BUS 314572 /* ISLAND

	END
DVP_P1-2: LN 2181	CONTINGENCY 'DVP_P1-2: LN 2181' OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00 OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-RMOUNT#4230.00 - 6NASH 230.00 OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY 230.00 - 6NASH 230.00 OPEN BUS 314591 /* ISLAND: 6NASH 230.00 END
DVP_P1-2: LN 238	CONTINGENCY 'DVP_P1-2: LN 238' OPEN BRANCH FROM BUS 314282 TO BUS 314435 CKT 1 /* 6CARSON 230.00 - 6SAPONY 230.00 OPEN BRANCH FROM BUS 314435 TO BUS 314563 CKT 1 /* 6SAPONY 230.00 - 6CLUBHSE 230.00 OPEN BRANCH FROM BUS 314562 TO BUS 314563 CKT 1 /* 3CLUBHSE 115.00 - 6CLUBHSE 230.00 OPEN BUS 314435 /* ISLAND END
DVP_P1-2: LN 246	CONTINGENCY 'DVP_P1-2: LN 246' OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* 6SUFFOLK 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 6EARLEYS 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 6NUCO TP 230.00 - 6NUCOR 230.00 OPEN BUS 314575 /* ISLAND OPEN BUS 314590 /* ISLAND END

DVP_P1-2: LN 254-A	CONTINGENCY 'DVP_P1-2: LN 254-A' OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1 /* 6CLUBHSE 230.00 - AB2-100 TAP 230.00 END
DVP_P4-2: 2020T2144	CONTINGENCY 'DVP_P4-2: 2020T2144' /* WINFALL 230 KV OPEN BRANCH FROM BUS 313851 TO BUS 314638 CKT 1 /* 6ECITYDP2 230.00 - 6ELIZ CT 230.00 OPEN BRANCH FROM BUS 313851 TO BUS 314639 CKT 1 /* 6ECITYDP2 230.00 - 6TANGLEW 230.00 OPEN BRANCH FROM BUS 314639 TO BUS 314651 CKT 1 /* 6TANGLEW 230.00 - 6WINFALL 230.00 OPEN BUS 313851 /* ISLAND: 6ECITYDP2 230.00 OPEN BUS 314639 /* ISLAND: 6TANGLEW 230.00 OPEN BUS 913391 /* ISLAND: Y1-086 C 230.00 OPEN BUS 913392 /* ISLAND: Y1-086 E 230.00 OPEN BUS 917121 /* ISLAND: Z2-027 C 230.00 OPEN BUS 917122 /* ISLAND: Z2-027 E 230.00 OPEN BRANCH FROM BUS 314651 TO BUS 901080 CKT 1 /* 6WINFALL 230.00 - W1-029 230.00 END
DVP_P4-2: 24662	CONTINGENCY 'DVP_P4-2: 24662' /* EARLEYS OPEN BRANCH FROM BUS 314568 TO BUS 314569 CKT 1 /* TX. #3 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314537 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR END

DVP_P4-2: 24682	CONTINGENCY 'DVP_P4-2: 24682' /* 24682 @ SUFFOLK OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* SUFFOLK - NUCOR TAP OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* NUCOR TAP - EARLEYS OPEN BRANCH FROM BUS 314536 TO BUS 314537 CKT 2 /* SUFFOLK 230-115 TX#5 OPEN BRANCH FROM BUS 314928 TO BUS 314537 CKT 2 /* SUFFOLK 500-230 TX#8 END
DVP_P4-2: 246T2034	CONTINGENCY 'DVP_P4-2: 246T2034' /* EARLEYS OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314537 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1 /* 2034 OPEN BRANCH FROM BUS 314620 TO BUS 933990 CKT 1 /* 2034 END
DVP_P4-2: 246T247	CONTINGENCY 'DVP_P4-2: 246T247' /* SUFFOLK 230 KV OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* 6SUFFOLK 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 6EARLEYS 230.00 - 6NUCO TP 230.00 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 6NUCO TP 230.00 - 6NUCOR 230.00 OPEN BUS 314575 /* ISLAND: 6NUCO TP 230.00 OPEN BUS 314590 /* ISLAND: 6NUCOR 230.00 OPEN BRANCH FROM BUS 314537 TO BUS 314648 CKT 1 /* 6SUFFOLK 230.00 - 6SUNBURY 230.00 OPEN BRANCH FROM BUS 314648 TO BUS 901080 CKT 1 /* 6SUNBURY 230.00 - W1-029 230.00


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OPEN BRANCH FROM BUS 304226 TO BUS 304222 CKT 1      /* 6PA-RMOUNT#4230.00 - 6ROCKYMT230T
OPEN BUS 304226                                     /* ISLAND
OPEN BUS 314591                                     /* ISLAND: 6NASH 230.00
END
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Summer Peak Analysis - 2021

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

Overload Number	Contingency Type	Contingency Name	Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Flowgate Appendix
					From	To	Circuit		Initial	Final	Type	MVA		
1	N-1	"313845	DVP - CPLE	6MORNSTR-6ROCKYMT230T 230 kV line	313845	304222	1	DC	105.3	109.15	ER	374	14.39	1
2	N-1	DVP_P1-2: LN 2181	DVP - CPLE	6MORNSTR-6ROCKYMT230T 230 kV line	313845	304222	1	DC	101.5	105.35	ER	374	14.39	
3	DCTL	DVP_P7-1: LN 2058-2181	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	419.24	433.61	ER	93	13.14	2
4	DCTL	DVP_P7-1: LN 81-2056	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV	314554	304223	1	DC	205.05	207.24	ER	93	4.52	

				line										
5	N-1	"313845	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	130.32	132.91	ER	93	2.41	
6	N-1	DVP_P1-2: LN 2181	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	129.46	132.05	ER	93	2.41	
7	LFFB	DVP_P4-2: 246T247	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	133.25	135.39		637	13.55	3
8	LFFB	DVP_P4-2: 246T2034	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	128.01	130.51		637	14.38	
9	LFFB	DVP_P4-2: 24662	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	126.53	128.61		637	13.15	
10	LFFB	DVP_P4-2: 24682	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	126.44	128.52		637	13.19	
11	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	314569	314575	1	DC	102.84	104.33	ER	572	8.51	4
12	N-1	DVP_P1-2: LN 2131_FSA	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	314569	314575	1	DC	102.58	104.07	ER	572	8.51	
13	DCTL	DVP_P7-1: LN 2058-2181	DVP - DVP	6EVERETS-AD2-068 TAP 230 kV line	314574	936530	1	DC	127.94	131.48		485	17.18	5
14	N-1	DVP_P1-2: LN 254-A	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	133.23	134.79	ER	375	5.87	6
15	N-1	DVP_P1-2: LN 238	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	131.55	133.04	ER	375	5.59	
16	LFFB	DVP_P4-2: 246T247	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	127.88	130.73		459	13.05	7
17	N-1	DVP_P1-2: LN 246	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	107.7	109.73	ER	375	7.61	
18	N-1	DVP_P1-2: LN 2141	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	107.7	109.63	ER	375	7.19	
19	LFFB	DVP_P4-2: 246T247	DVP - DVP	6ELIZ CT-6SHAWBRO 230 kV line	314638	314647	1	DC	134.93	136.22		699	9	8
20	LFFB	DVP_P4-2: 24682	DVP - DVP	6S HERTFORD-6WINFALL 230 kV line	314662	314651	1	DC	107.32	108.48		897	10.4	9
21	LFFB	DVP_P4-2: 24682	DVP - DVP	Z1-036 TAP-6S HERTFORD 230 kV line	916040	314662	1	DC	108.68	109.84		897	10.4	10
22	LFFB	DVP_P4-2: 246T247	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	141.69	144.54		459	13.05	11
23	N-1	DVP_P1-2: LN 246	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	119.03	121.07	ER	375	7.61	
24	N-1	DVP_P1-2: LN 2141	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	120.77	122.7	ER	375	7.19	
25	DCTL	DVP_P7-1: LN 2058-2181	DVP - CPLE	AD2-068 TAP-6GREENVILE T 230 kV line	936530	304451	1	DC	135.19	138.78	ER	478	17.18	12
26	LFFB	DVP_P4-2: 2020T2144	DVP - CPLE	AD2-068 TAP-6GREENVILE T 230 kV line	936530	304451	1	DC	115.32	117.06	ER	478	11.5	
27	LFFB	AEP_P4_#7589_05J.FERR 765	AEP - AEP	05EDAN 1-05DANVL2 138 kV line	242631	242620	1	DC	136.58	137.15	ER	415	5.29	13

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

None

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
1, 2	6MORNSTR-6ROCKYMT230T 230 kV line	DVP / CPLE: This line is a joint tie line between the Dominion Energy and Duke/Progress transmission systems. An affected systems study will need to be completed with Duke/Progress to determine impacts what needs to be done by both parties to increase the rating of this transmission line. This violation will be evaluated in the System Impact Study phase.	-	-
3, 4, 5, 6	3BTLEBRO-3ROCKYMT115T 115 kV	Same reinforcement as for Violations 1 and 2.	-	-
7, 8, 9, 10	6CLUBHSE-6SAPONY 230 kV line	DVP: Replace wave trap at Clubhouse Substation to increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated take 12-16 months to engineer and construct.	Pending	\$150,000
11, 12	6EARLEYS-6NUCO TP 230 kV line	DVP: Wreck and rebuild the line of 14 miles to increase its line rating to 1047 MVA (normal), 1047 MVA (emergency), and 1204 MVA (load dump). It is estimated to take 30-36 months to engineer, permit, and construct. A SCC and a Va CPCN is required.	Pending	\$37,800,000
13	6EVERETS-AD2-068 TAP 230 kV line	DVP: Wreck and rebuild the line of 18 miles to increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated to take 44-48 months to engineer, permit, and construct. A Va CPCN is required. A certificate from the NC PUC will most likely be required.	Pending	\$45,000,000
14, 15	6LAKEVEW-6CAROLNA 230 kV line	DVP: Wreck and rebuild the line of 1.5 miles to increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated to take 30-36 months to engineer, permit, and construct. A Va CPCN is required.	Pending	\$3,625,000

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
16, 17, 18	6LAKEVEW-AB2-100 TAP 230 kV line	DVP: Wreck and rebuild the line of 16 miles to increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated to take 44-48 months to engineer, permit, and construct. A Va CPCN is required. A certificate from the NC PUC will most likely be required.	Pending	\$40,000,000
19	6ELIZ CT-6SHAWBRO 230 kV line	DVP: Wreck and rebuild the line of 8 miles to increase its line rating to 1047 MVA (normal), 1047 MVA (emergency), and 1204 MVA (load dump). It is estimated to take 30-36 months to engineer, permit, and construct. A Va CPCN is required.	Pending	\$25,700,000
20	6S HERTFORD-6WINFALL 230 kV line	DVP: Wreck and rebuild the line of 8 miles to increase its line rating to 1047 MVA (normal), 1047 MVA (emergency), and 1204 MVA (load dump). It is estimated to take 30-36 months to engineer, permit, and construct. A Va CPCN is required.	Pending	\$19,875,000
21	Z1-036 TAP-6S HERTFORD 230 kV line	Same reinforcement as for Violation 20 above.	-	-
22, 23, 24	AB2-100 TAP-6CLUBHSE 230 kV line	DVP: Wreck and rebuild the AB2-100 TAP-Clubhouse 230kV line of 2 miles to increase its line rating to 722 MVA (normal), 722 MVA (emergency), and 830 MVA (load dump). It is estimated to take 24-28 months to engineer, permit and construct. A Va CPCN is required.	Pending	\$5,000,000
25, 26	AD2-068 TAP-6GREENVILE T 230 kV line	DVP / CPLE: This line is a joint tie line between the Dominion Energy and Duke/Progress transmission systems. An affected systems study will need to be completed with Duke/Progress to determine impacts what needs to be done by both parties to increase the rating of this transmission line. This violation will be evaluated in the System Impact Study phase.	-	-

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
27	05EDAN 1-05DANVL2 138 kV line	<p>AEP:</p> <ol style="list-style-type: none"> 1. Replace Switch (1200 A), estimated cost \$400,000. 2. Replace line risers (Limiting Element: Sub Cond 1590 AAC 61 Str.), estimated cost \$100,000. 3. Rebuild / Reconductor 3.16 miles of conductor (Limiting Element: 336/556 Six Wire ACSR), estimated cost \$4.72 million. 4. Conduct an engineering study to determine if Relay - CT Thermal limit settings can be adjusted to mitigate the overload (Estimated Cost \$25,000), if not, a new relay package will be required (Estimated Cost: \$600,000). (Limiting Element: Relay Thermal Limit 1795 Amps - East Danville) 5. Conduct an engineering study to determine if Relay - CT Thermal limit settings can be adjusted to mitigate the overload (Estimated Cost \$25,000), if not, a new relay package will be required (Estimated Cost: \$600,000). (Limiting Element: Relay Thermal Limit 1795 Amps - Danville) 6. Conduct an engineering study to determine if Relay - CT Compliance Trip limit settings can be adjusted to mitigate the overload (Estimated Cost \$25,000), if not, a new relay package will be required (Estimated Cost: \$600,000). (Limiting Element: Relay Compliance Trip Limit 1916 Amps - East Danville) 7. Conduct an engineering study to determine if Relay - CT Compliance Trip limit settings can be adjusted to mitigate the overload (Estimated Cost \$25,000), if not, a new relay package will be required (Estimated Cost: \$600,000). (Limiting Element: Relay Compliance Trip Limit 1916 Amps - Danville) 8. Rebuild / Reconductor 0.03 miles of conductor (Limiting Element: 1351.5 ACSR 45/7 DIPPER) Near East Danville, estimated cost \$0.045 million. 9. Rebuild / Reconductor 0.03 miles of conductor (Limiting Element: 1351.5 ACSR 45/7 DIPPER) Near Danville, estimated cost \$0.045 million. <p>An approximate construction time would be 24 to 36 months after signing an interconnection agreement</p>	Pending	\$7,710,000

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
Total Previous Network Upgrades (This project may have a contribution towards these reinforcements)				\$184,860,000

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

Overload Number	Type	Contingency Name	Affected Area	Facility Description	Bus		Circuit	Power Flow	Loading %		Rating Type	Rating MV A	MW Contribution	Flowgate Appendix
					From	To			Initial	Final				
28	N-1	"313845	DVP - CPLE	6MORNSTR-6ROCKYMT230T 230 kV line	313845	304222	1	DC	146.04	152.46	ER	374	23.98	
29	N-1	DVP_P1-2: LN 2058	DVP - DVP	6MORNSTR-6NASH 230 kV line	313845	314591	1	DC	125.85	131.3	ER	449	24.46	
30	N-1	DVP_P1-2: LN 246	DVP - DVP	6MACKEYS-6EDENTON 230 kV line	314203	314637	1	DC	107.51	108.94	ER	731	10.44	
31	N-1	"314288	DVP - DVP	6CHRL249-6LOCKS 230 kV line	314285	314316	1	DC	99.84	100.27	ER	559	5.33	
32	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6SAPONY-6CARSON 230 kV line	314435	314282	1	DC	125.91	127.67	ER	679	11.91	
33	N-1	"313845	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	182.22	184.17	ER	93	4.02	
34	N-1	DVP_P1-2: LN 246	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	134.49	136.71	ER	599	13.16	
35	Non	Non	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	114.4	116.34	NR	599	10.79	
36	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	314569	314575	1	DC	165.63	167.94	ER	572	14.18	

37	Non	Non	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	31456 9	31457 5	1	DC	98.15	100.0 9	NR	572	11.09	
38	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6EVERETS-AD2-068 TAP 230 kV line	31457 4	93653 0	1	DC	118.9 5	120.3 1	ER	449	11.49	
39	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6NUCO TP-6SUFFOLK 230 kV line	31457 5	31453 7	1	DC	159.6 1	161.9 3	ER	572	14.18	
40	N-1	DVP_P1-2: LN 254-A	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	31458 3	31456 1	1	DC	161.3 8	163.1 2	ER	375	9.78	
41	N-1	DVP_P1-2: LN 2131A	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	31458 3	92451 0	1	DC	156.1 1	159.2	ER	375	11.52	
42	Non	Non	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	31458 3	92451 0	1	DC	119.7 6	122.5 6	NR	375	10.48	
43	N-1	DVP_P1-2: LN 2058	DVP - CPLE	6NASH-6PA-RMOUNT#4 230 kV line	31459 1	30422 6	1	DC	115.2 9	120.5	ER	470	24.46	
44	N-1	DVP_P1-2: LN 246	DVP - DVP	6EDENTON-Z1-036 TAP 230 kV line	31463 7	91604 0	1	DC	103.0 9	104.5 1	ER	733	10.44	
45	N-1	DVP_P1-2: LN 246	DVP - DVP	6S HERTFORD-6WINFALL 230 kV line	31466 2	31465 1	1	DC	131.0 8	132.5	ER	733	10.43	
46	N-1	DVP_P1-2: LN 246	DVP - DVP	Z1-036 TAP-6S HERTFORD 230 kV line	91604 0	31466 2	1	DC	132.7 2	134.1 5	ER	733	10.43	
47	N-1	DVP_P1-2: LN 130-A	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	92451 0	31456 3	1	DC	167.7 1	170.6 9	ER	375	11.15	
48	Non	Non	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	92451 0	31456 3	1	DC	135.2 4	138.0 4	NR	375	10.48	
49	N-1	DVP_P1-2: LN 2131A	DVP - CPLE	AD2-068 TAP-6GREENVILE T 230 kV line	93653 0	30445 1	1	DC	115.7 1	117.3 1	ER	478	11.49	
50	Non	Non	DVP - DVP	AD2-089 TAP-3TARRTP 115 kV line	93670 0	31454 8	1	DC	2.22	116.8 6	NR	63	75	
51	N-1	AEP_P1-2_#1377	AEP - AEP	05EDAN 1-05DANVL2 138 kV line	24263 1	24262 0	1	DC	136.5 5	137.1 3	ER	415	5.29	
52	Non	Non	AEP - AEP	05EDAN 1-05DANVL2 138 kV line	24263 1	24262 0	1	DC	112.2 9	112.9 8	NR	275	4.2	

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

Attachment 1.
System Configuration

Attachment 2.

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gauge other generators impact. When a flowgate is identified in multiple analysis the appendix is presented for only the analysis with the greatest overload.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DVP - CPLE) The 6MORNSTR-6ROCKYMT230T 230 kV line (from bus 313845 to bus 304222 ckt 1) loads from 105.3% to 109.15% (**DC power flow**) of its emergency rating (374 MVA) for the single line contingency outage of '313845'. This project contributes approximately 14.39 MW to the thermal violation.

CONTINGENCY '313845'

6MORNSTR 230 314591 6NASH 230

1

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	1.32
315292	1DOMTR78	0.89
315293	1DOMTR9	0.73
315131	1EDGECEMA	24.67
315132	1EDGECEMB	24.67
315139	1GASTONA	3.83
315141	1GASTONB	3.83
315126	1ROARAP2	1.23
315128	1ROARAP4	1.18
315136	1ROSEMG1	3.2
315138	1ROSEMG2	1.5
315137	1ROSEMS1	1.98
315115	1S HAMPT1	0.84
314704	3LAWRENC	0.19
932631	AC2-084 C	8.41
933991	AD1-023 C	7.23
934201	AD1-047 C	5.76
934231	AD1-050 C	1.59
934331	AD1-057 C OI	19.74

<i>934521</i>	<i>AD1-076 C OI</i>	<i>28.43</i>
<i>936401</i>	<i>AD2-051 C OI</i>	<i>6.11</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>14.39</i>
<i>936711</i>	<i>AD2-090 C OI</i>	<i>3.7</i>
<i>937441</i>	<i>AD2-195 C</i>	<i>5.5</i>
<i>LTF</i>	<i>AMIL</i>	<i>0.38</i>
<i>LTF</i>	<i>BAYOU</i>	<i>1.99</i>
<i>LTF</i>	<i>BIG_CAJUN1</i>	<i>3.13</i>
<i>LTF</i>	<i>BIG_CAJUN2</i>	<i>6.3</i>
<i>LTF</i>	<i>BLUEG</i>	<i>1.99</i>
<i>LTF</i>	<i>CALDERWOOD</i>	<i>1.17</i>
<i>LTF</i>	<i>CANNELTON</i>	<i>0.38</i>
<i>LTF</i>	<i>CATAWBA</i>	<i>1.15</i>
<i>LTF</i>	<i>CELEVELAND</i>	<i>3.27</i>
<i>LTF</i>	<i>CHEOAH</i>	<i>1.1</i>
<i>LTF</i>	<i>CHILHOWEE</i>	<i>0.38</i>
<i>LTF</i>	<i>CHOCTAW</i>	<i>2.13</i>
<i>LTF</i>	<i>CLIFTY</i>	<i>7.31</i>
<i>LTF</i>	<i>COTTONWOOD</i>	<i>7.78</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.72</i>
<i>LTF</i>	<i>EDWARDS</i>	<i>0.61</i>
<i>LTF</i>	<i>ELMERSMITH</i>	<i>1.11</i>
<i>LTF</i>	<i>FARMERCITY</i>	<i>0.48</i>
<i>LTF</i>	<i>G-007A</i>	<i>0.79</i>
<i>LTF</i>	<i>GIBSON</i>	<i>0.69</i>
<i>LTF</i>	<i>HAMLET</i>	<i>4.55</i>

<i>LTF</i>	<i>MORGAN</i>	<i>3.44</i>
<i>LTF</i>	<i>NEWTON</i>	<i>1.68</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>3.63</i>
<i>LTF</i>	<i>ROWAN</i>	<i>2.41</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.33</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.32</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.82</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.73</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.38</i>
<i>LTF</i>	<i>TVA</i>	<i>1.45</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>2.09</i>
<i>900671</i>	<i>V4-068 C</i>	<i>0.06</i>
<i>LTF</i>	<i>VFT</i>	<i>2.1</i>
<i>901081</i>	<i>W1-029C</i>	<i>0.38</i>
<i>913391</i>	<i>Y1-086 C</i>	<i>0.07</i>
<i>916041</i>	<i>Z1-036 C</i>	<i>0.45</i>
<i>917121</i>	<i>Z2-027 C</i>	<i>0.13</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.34</i>
<i>917341</i>	<i>Z2-044 C</i>	<i>0.31</i>
<i>917511</i>	<i>Z2-088 C OP1</i>	<i>1.58</i>
<i>918411</i>	<i>AA1-050</i>	<i>1.33</i>
<i>918491</i>	<i>AA1-063AC OP</i>	<i>1.13</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>1.1</i>
<i>918531</i>	<i>AA1-067 C</i>	<i>0.23</i>
<i>918561</i>	<i>AA1-072 C</i>	<i>0.05</i>
<i>919691</i>	<i>AA2-053 C</i>	<i>1.26</i>

<i>919701</i>	<i>AA2-057 C</i>	<i>1.5</i>
<i>920041</i>	<i>AA2-088 C</i>	<i>0.7</i>
<i>920591</i>	<i>AA2-165 C</i>	<i>0.21</i>
<i>920671</i>	<i>AA2-174 C</i>	<i>0.06</i>
<i>920691</i>	<i>AA2-178 C</i>	<i>4.34</i>
<i>930051</i>	<i>AB1-013 C</i>	<i>1.31</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>14.26</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>15.74</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>1.62</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>1.62</i>
<i>923801</i>	<i>AB2-015 C O1</i>	<i>4.04</i>
<i>923851</i>	<i>AB2-025 C</i>	<i>0.19</i>
<i>923911</i>	<i>AB2-031 C O1</i>	<i>1.61</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.67</i>
<i>923991</i>	<i>AB2-040 C O1</i>	<i>5.28</i>
<i>924151</i>	<i>AB2-059 C O1</i>	<i>16.8</i>
<i>924391</i>	<i>AB2-088 C</i>	<i>0.86</i>
<i>924401</i>	<i>AB2-089 C</i>	<i>0.72</i>
<i>924491</i>	<i>AB2-098 C</i>	<i>0.42</i>
<i>924501</i>	<i>AB2-099 C</i>	<i>0.4</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>8.39</i>
<i>925121</i>	<i>AB2-169 C</i>	<i>4.01</i>
<i>925171</i>	<i>AB2-174 C O1</i>	<i>4.92</i>
<i>925281</i>	<i>AB2-186 C</i>	<i>0.21</i>
<i>925291</i>	<i>AB2-188 C O1</i>	<i>1.07</i>
<i>925591</i>	<i>AC1-034 C</i>	<i>10.88</i>

<i>925781</i>	<i>ACI-054 C</i>	<i>2.81</i>
<i>926071</i>	<i>ACI-086 C</i>	<i>23.17</i>
<i>926201</i>	<i>ACI-098 C</i>	<i>5.9</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>1.98</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>1.31</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>12.14</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>8.71</i>

Appendix 2

(DVP - CPLE) The 3BTLEBRO-3ROCKYMT115T 115 kV line (from bus 314554 to bus 304223 ckt 1) loads from 419.24% to 433.61% (**DC power flow**) of its emergency rating (93 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 2058-2181'. This project contributes approximately 13.14 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 2058-2181'

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*

6ROCKYMT230T230.00 - 6HATHAWAY 230.00

OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00

OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-

RMOUNT#4230.00 - 6NASH 230.00

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY
230.00 - 6NASH 230.00

OPEN BUS 314591 /* ISLAND: 6NASH 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	13.41
315132	1EDGECEMB	13.41
315139	1GASTONA	2.36
315141	1GASTONB	2.36
315126	1ROARAP2	0.98
315128	1ROARAP4	0.95
315136	1ROSEMG1	1.92
315138	1ROSEMG2	0.9
315137	1ROSEMS1	1.19
314557	3BETHEL C	0.88
314554	3BTLEBRO	1.96
314572	3EMPORIA	0.2
314578	3HORNRTN	2.51
314582	3KELFORD	0.69

<i>314603</i>	<i>3SCOT NK</i>	<i>3.67</i>
<i>314617</i>	<i>3TUNIS</i>	<i>0.44</i>
<i>314541</i>	<i>3WATKINS</i>	<i>0.26</i>
<i>314620</i>	<i>6CASHIE</i>	<i>0.32</i>
<i>314574</i>	<i>6EVERETS</i>	<i>1.04</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>11.33</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>5.58</i>
<i>934201</i>	<i>AD1-047 C</i>	<i>4.29</i>
<i>934202</i>	<i>AD1-047 E</i>	<i>2.86</i>
<i>934331</i>	<i>AD1-057 C O1</i>	<i>11.1</i>
<i>934332</i>	<i>AD1-057 E O1</i>	<i>5.92</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>4.83</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>2.07</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>7.89</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>5.26</i>
<i>936711</i>	<i>AD2-090 C O1</i>	<i>2.85</i>
<i>936712</i>	<i>AD2-090 E O1</i>	<i>1.9</i>
<i>LTF</i>	<i>AMIL</i>	<i>0.25</i>
<i>LTF</i>	<i>BAYOU</i>	<i>1.34</i>
<i>LTF</i>	<i>BIG_CAJUN1</i>	<i>2.12</i>
<i>LTF</i>	<i>BIG_CAJUN2</i>	<i>4.26</i>
<i>LTF</i>	<i>BLUEG</i>	<i>1.34</i>
<i>LTF</i>	<i>CALDERWOOD</i>	<i>0.79</i>
<i>LTF</i>	<i>CANNELTON</i>	<i>0.25</i>
<i>LTF</i>	<i>CARR</i>	<i>< 0.01</i>
<i>LTF</i>	<i>CATAWBA</i>	<i>0.78</i>

<i>LTF</i>	<i>CELEVELAND</i>	<i>2.21</i>
<i>LTF</i>	<i>CHEOAH</i>	<i>0.74</i>
<i>LTF</i>	<i>CHILHOWEE</i>	<i>0.26</i>
<i>LTF</i>	<i>CHOCTAW</i>	<i>1.44</i>
<i>LTF</i>	<i>CLIFTY</i>	<i>4.9</i>
<i>LTF</i>	<i>COTTONWOOD</i>	<i>5.26</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.48</i>
<i>LTF</i>	<i>EDWARDS</i>	<i>0.41</i>
<i>LTF</i>	<i>ELMERSMITH</i>	<i>0.75</i>
<i>LTF</i>	<i>FARMERCITY</i>	<i>0.32</i>
<i>LTF</i>	<i>G-007A</i>	<i>0.51</i>
<i>LTF</i>	<i>GIBSON</i>	<i>0.47</i>
<i>LTF</i>	<i>HAMLET</i>	<i>3.13</i>
<i>LTF</i>	<i>MORGAN</i>	<i>2.33</i>
<i>LTF</i>	<i>NEWTON</i>	<i>1.13</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>2.45</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>< 0.01</i>
<i>LTF</i>	<i>ROSETON</i>	<i>< 0.01</i>
<i>LTF</i>	<i>ROWAN</i>	<i>1.62</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.22</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.22</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.55</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.49</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.25</i>
<i>LTF</i>	<i>TVA</i>	<i>0.98</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>1.41</i>

900672	V4-068 E	0.15
<i>LTF</i>	<i>VFT</i>	<i>1.35</i>
917331	Z2-043 C	0.36
917332	Z2-043 E	0.82
917341	Z2-044 C	0.54
917342	Z2-044 E	1.25
917511	Z2-088 C OPI	0.87
917512	Z2-088 E OPI	3.69
918411	AA1-050	0.73
918492	AA1-063AE OP	2.28
918512	AA1-065 E OP	1.94
918532	AA1-067 E	0.31
918561	AA1-072 C	0.05
918562	AA1-072 E	0.14
919691	AA2-053 C	1.01
919692	AA2-053 E	2.32
919701	AA2-057 C	2.47
919702	AA2-057 E	6.64
920042	AA2-088 E	4.77
920591	AA2-165 C	0.34
920592	AA2-165 E	0.87
920671	AA2-174 C	0.05
920672	AA2-174 E	0.27
930401	AB1-081 C	20.04
930402	AB1-081 E	8.59
930861	AB1-132 C	9.71

930862	<i>ABI-132 E</i>	<i>4.16</i>
931231	<i>ABI-173 C</i>	<i>1.21</i>
931232	<i>ABI-173 E</i>	<i>0.56</i>
931241	<i>ABI-173AC</i>	<i>1.21</i>
931242	<i>ABI-173AE</i>	<i>0.56</i>
923911	<i>AB2-031 C O1</i>	<i>1.2</i>
923912	<i>AB2-031 E O1</i>	<i>0.59</i>
923941	<i>AB2-035 C</i>	<i>0.37</i>
923942	<i>AB2-035 E</i>	<i>0.16</i>
923991	<i>AB2-040 C O1</i>	<i>3.93</i>
923992	<i>AB2-040 E O1</i>	<i>3.22</i>
924151	<i>AB2-059 C O1</i>	<i>23.62</i>
924152	<i>AB2-059 E O1</i>	<i>12.17</i>
924391	<i>AB2-088 C</i>	<i>0.47</i>
924392	<i>AB2-088 E</i>	<i>0.23</i>
924491	<i>AB2-098 C</i>	<i>0.24</i>
924492	<i>AB2-098 E</i>	<i>0.1</i>
924501	<i>AB2-099 C</i>	<i>0.31</i>
924502	<i>AB2-099 E</i>	<i>0.13</i>
924511	<i>AB2-100 C</i>	<i>5.31</i>
924512	<i>AB2-100 E</i>	<i>2.62</i>
925171	<i>AB2-174 C O1</i>	<i>3.6</i>
925172	<i>AB2-174 E O1</i>	<i>3.26</i>
925591	<i>AC1-034 C</i>	<i>15.3</i>
925592	<i>AC1-034 E</i>	<i>11.54</i>
926071	<i>AC1-086 C</i>	<i>14.3</i>

<i>926072</i>	<i>ACI-086 E</i>	<i>6.51</i>
<i>926201</i>	<i>ACI-098 C</i>	<i>7.95</i>
<i>926202</i>	<i>ACI-098 E</i>	<i>4.74</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>2.66</i>
<i>926212</i>	<i>ACI-099 E</i>	<i>1.56</i>
<i>LTF</i>	<i>ACI-133</i>	<i>9.34</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>1.04</i>
<i>926772</i>	<i>ACI-163 E</i>	<i>0.48</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>6.74</i>
<i>927022</i>	<i>ACI-189 E</i>	<i>3.36</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>11.27</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>5.</i>

Appendix 3

(DVP - DVP) The 6CLUBHSE-6SAPONY 230 kV line (from bus 314563 to bus 314435 ckt 1) loads from 133.25% to 135.39% (**DC power flow**) of its load dump rating (637 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 246T247'. This project contributes approximately 13.55 MW to the thermal violation.

```

CONTINGENCY 'DVP_P4-2: 246T247'                /* SUFFOLK 230 KV
  OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1    /* 6SUFFOLK
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1    /* 6EARLEYS
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1    /* 6NUCO TP
230.00 - 6NUCOR 230.00
  OPEN BUS 314575                                /* ISLAND: 6NUCO TP 230.00
  OPEN BUS 314590                                /* ISLAND: 6NUCOR 230.00
  OPEN BRANCH FROM BUS 314537 TO BUS 314648 CKT 1    /* 6SUFFOLK
230.00 - 6SUNBURY 230.00
  OPEN BRANCH FROM BUS 314648 TO BUS 901080 CKT 1    /* 6SUNBURY
230.00 - W1-029 230.00
  OPEN BUS 314648                                /* ISLAND: 6SUNBURY 230.00
END
  
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315150	1BUGGS 1	8.64
315151	1BUGGS 2	8.64
315131	1EDGECMA	10.81
315132	1EDGECMB	10.81
315139	1GASTONA	7.18
315141	1GASTONB	7.18
315126	1ROARAP2	2.57
315128	1ROARAP4	2.47
315136	1ROSEMG1	4.85
315138	1ROSEMG2	2.27
315137	1ROSEMS1	3.01

<i>314557</i>	<i>3BETHELC</i>	<i>0.9</i>
<i>314554</i>	<i>3BTLEBRO</i>	<i>0.91</i>
<i>314566</i>	<i>3CRESWEL</i>	<i>1.69</i>
<i>314572</i>	<i>3EMPORIA</i>	<i>1.04</i>
<i>314578</i>	<i>3HORNRTN</i>	<i>5.4</i>
<i>314582</i>	<i>3KELFORD</i>	<i>1.09</i>
<i>314704</i>	<i>3LAWRENC</i>	<i>0.78</i>
<i>314603</i>	<i>3SCOT NK</i>	<i>4.39</i>
<i>314617</i>	<i>3TUNIS</i>	<i>1.</i>
<i>314541</i>	<i>3WATKINS</i>	<i>0.48</i>
<i>314620</i>	<i>6CASHIE</i>	<i>0.87</i>
<i>314574</i>	<i>6EVERETS</i>	<i>2.55</i>
<i>314594</i>	<i>6PLYMOTH</i>	<i>0.72</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>11.81</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>5.82</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>12.48</i>
<i>933992</i>	<i>AD1-023 E</i>	<i>6.8</i>
<i>934201</i>	<i>AD1-047 C</i>	<i>17.56</i>
<i>934202</i>	<i>AD1-047 E</i>	<i>11.71</i>
<i>934231</i>	<i>AD1-050 C</i>	<i>5.08</i>
<i>934232</i>	<i>AD1-050 E</i>	<i>2.78</i>
<i>934331</i>	<i>AD1-057 C OI</i>	<i>15.84</i>
<i>934332</i>	<i>AD1-057 E OI</i>	<i>8.45</i>
<i>934521</i>	<i>AD1-076 C OI</i>	<i>47.19</i>
<i>934522</i>	<i>AD1-076 E OI</i>	<i>24.03</i>
<i>LTF</i>	<i>AD1-120</i>	<i>4.44</i>

<i>LTF</i>	<i>AD1-121</i>	<i>4.42</i>
<i>936261</i>	<i>AD2-033 C</i>	<i>9.73</i>
<i>936262</i>	<i>AD2-033 E</i>	<i>6.49</i>
<i>936361</i>	<i>AD2-046 C O1</i>	<i>8.38</i>
<i>936362</i>	<i>AD2-046 E O1</i>	<i>3.85</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>11.34</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>4.87</i>
<i>936481</i>	<i>AD2-063 C O1</i>	<i>11.53</i>
<i>936482</i>	<i>AD2-063 E O1</i>	<i>7.68</i>
<i>936531</i>	<i>AD2-068 C</i>	<i>4.92</i>
<i>936532</i>	<i>AD2-068 E</i>	<i>2.53</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>8.13</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>5.42</i>
<i>936711</i>	<i>AD2-090 C O1</i>	<i>5.56</i>
<i>936712</i>	<i>AD2-090 E O1</i>	<i>3.71</i>
<i>LTF</i>	<i>AD2-099</i>	<i>3.35</i>
<i>937441</i>	<i>AD2-195 C</i>	<i>8.63</i>
<i>937442</i>	<i>AD2-195 E</i>	<i>3.72</i>
<i>LTF</i>	<i>CARR</i>	<i>0.12</i>
<i>LTF</i>	<i>CBM-S1</i>	<i>5.43</i>
<i>LTF</i>	<i>CBM-S2</i>	<i>10.9</i>
<i>LTF</i>	<i>CBM-W1</i>	<i>12.02</i>
<i>LTF</i>	<i>CBM-W2</i>	<i>29.4</i>
<i>LTF</i>	<i>CIN</i>	<i>2.7</i>
<i>LTF</i>	<i>CPL</i>	<i>3.68</i>
<i>LTF</i>	<i>G-007</i>	<i>0.77</i>

<i>LTF</i>	<i>IPL</i>	<i>1.72</i>
<i>LTF</i>	<i>LGEE</i>	<i>0.58</i>
<i>LTF</i>	<i>MEC</i>	<i>6.07</i>
<i>LTF</i>	<i>MECS</i>	<i>2.72</i>
<i>LTF</i>	<i>O-066</i>	<i>4.92</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.09</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.68</i>
<i>900671</i>	<i>V4-068 C</i>	<i>0.11</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.33</i>
<i>LTF</i>	<i>WEC</i>	<i>0.74</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.57</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>1.31</i>
<i>917341</i>	<i>Z2-044 C</i>	<i>0.3</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.7</i>
<i>917511</i>	<i>Z2-088 C OP1</i>	<i>1.01</i>
<i>917512</i>	<i>Z2-088 E OP1</i>	<i>4.28</i>
<i>918411</i>	<i>AA1-050</i>	<i>0.85</i>
<i>918491</i>	<i>AA1-063AC OP</i>	<i>2.23</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>5.65</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>2.12</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>5.62</i>
<i>918531</i>	<i>AA1-067 C</i>	<i>0.33</i>
<i>918532</i>	<i>AA1-067 E</i>	<i>0.76</i>
<i>918561</i>	<i>AA1-072 C</i>	<i>0.09</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.22</i>
<i>919691</i>	<i>AA2-053 C</i>	<i>2.58</i>

919692	AA2-053 E	5.95
919701	AA2-057 C	1.68
919702	AA2-057 E	4.51
LTF	AA2-074	2.5
920041	AA2-088 C	1.17
920042	AA2-088 E	10.3
920591	AA2-165 C	0.23
920592	AA2-165 E	0.6
920671	AA2-174 C	0.12
920672	AA2-174 E	0.69
920691	AA2-178 C	6.77
920692	AA2-178 E	2.9
930051	AB1-013 C	2.04
930052	AB1-013 E	13.67
930401	AB1-081 C	10.25
930402	AB1-081 E	4.39
930861	AB1-132 C	29.52
930862	AB1-132 E	12.65
931231	AB1-173 C	4.94
931232	AB1-173 E	2.31
931241	AB1-173AC	4.94
931242	AB1-173AE	2.31
923801	AB2-015 C O1	5.47
923802	AB2-015 E O1	4.49
923911	AB2-031 C O1	4.9
923912	AB2-031 E O1	2.41

923941	AB2-035 C	0.38
923942	AB2-035 E	0.16
923991	AB2-040 C OI	16.1
923992	AB2-040 E OI	13.17
924021	AB2-043 C OI	2.67
924022	AB2-043 E OI	4.39
924151	AB2-059 C OI	12.08
924152	AB2-059 E OI	6.22
924161	AB2-060 C OI	7.59
924162	AB2-060 E OI	3.57
924301	AB2-077 C OI	1.68
924302	AB2-077 E OI	1.12
924311	AB2-078 C OI	1.68
924312	AB2-078 E OI	1.12
924321	AB2-079 C OI	1.68
924322	AB2-079 E OI	1.12
924391	AB2-088 C	0.49
924392	AB2-088 E	0.23
924401	AB2-089 C	2.3
924402	AB2-089 E	1.19
924411	AB2-090 C	3.37
924412	AB2-090 E	1.73
924491	AB2-098 C	0.59
924492	AB2-098 E	0.25
924501	AB2-099 C	0.73
924502	AB2-099 E	0.31

924511	AB2-100 C	35.9
924512	AB2-100 E	17.68
925121	AB2-169 C	6.14
925122	AB2-169 E	5.51
925171	AB2-174 C O1	16.16
925172	AB2-174 E O1	14.62
925221	AB2-176 C	1.39
925222	AB2-176 E	0.59
925291	AB2-188 C O1	1.67
925292	AB2-188 E O1	0.75
925591	AC1-034 C	7.83
925592	AC1-034 E	5.9
925611	AC1-036 C	0.64
925612	AC1-036 E	1.04
925781	AC1-054 C	8.28
925782	AC1-054 E	3.81
926071	AC1-086 C	43.47
926072	AC1-086 E	19.78
926201	AC1-098 C	8.28
926202	AC1-098 E	4.94
926211	AC1-099 C	2.78
926212	AC1-099 E	1.63
926771	AC1-163 C	2.41
926772	AC1-163 E	1.13
927021	AC1-189 C	9.38
927022	AC1-189 E	4.67

<i>927141</i>	<i>ACI-208 C</i>	<i>13.11</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>5.82</i>

Appendix 4

(DVP - DVP) The 6EARLEYS-6NUCO TP 230 kV line (from bus 314569 to bus 314575 ckt 1) loads from 102.84% to 104.33% (**DC power flow**) of its emergency rating (572 MVA) for the single line contingency outage of 'DVP_P1-2: LN 2131A'. This project contributes approximately 8.51 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 2131A'

OPEN BRANCH FROM BUS 314662 TO BUS 916040 CKT 1 /* 6S HERTFORD
230.00 - Z1-036 TAP 230.00

OPEN BRANCH FROM BUS 314651 TO BUS 314662 CKT 1 /* 6WINFALL
230.00 - 6S HERTFORD 230.00

OPEN BUS 314662 /* ISLAND

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	4.52
315292	1DOMTR78	3.05
315293	1DOMTR9	2.49
315131	1EDGECEMA	9.02
315132	1EDGECEMB	9.02
315139	1GASTONA	3.69
315141	1GASTONB	3.69
315159	1KERR 2	0.81
315163	1KERR 6	0.79
315164	1KERR 7	0.79
315126	1ROARAP2	1.5
315128	1ROARAP4	1.44
315136	1ROSEMG1	2.6
315138	1ROSEMG2	1.22
315137	1ROSEMS1	1.61
314704	3LAWRENC	0.21

932631	AC2-084 C	11.32
933991	AD1-023 C	27.83
934201	AD1-047 C	6.39
934231	AD1-050 C	2.75
934331	AD1-057 C OI	10.19
934521	AD1-076 C OI	112.88
LTF	AD1-120	4.28
LTF	AD1-121	4.24
936401	AD2-051 C OI	16.62
936531	AD2-068 C	6.81
936701	AD2-089 C	8.51
LTF	AD2-099	3.34
937441	AD2-195 C	17.93
LTF	CARR	0.08
LTF	CBM-S1	5.28
LTF	CBM-S2	10.69
LTF	CBM-W1	11.81
LTF	CBM-W2	28.66
LTF	CIN	2.64
LTF	CPLE	3.68
LTF	IPL	1.69
LTF	LGEE	0.57
LTF	MEC	5.93
LTF	MECS	2.71
LTF	RENSSELAER	0.07
LTF	ROSETON	0.48

900671	V4-068 C	0.11
LTF	WEC	0.73
916041	Z1-036 C	2.55
917331	Z2-043 C	0.72
917341	Z2-044 C	0.26
917511	Z2-088 C OPI	1.14
918411	AA1-050	0.96
918491	AA1-063AC OP	1.36
918511	AA1-065 C OP	3.8
918531	AA1-067 C	0.49
918561	AA1-072 C	0.11
919691	AA2-053 C	1.91
919701	AA2-057 C	1.42
LTF	AA2-074	2.51
920041	AA2-088 C	0.79
920591	AA2-165 C	0.19
920671	AA2-174 C	0.09
920691	AA2-178 C	19.71
930051	AB1-013 C	5.95
930401	AB1-081 C	8.64
930861	AB1-132 C	15.15
931231	AB1-173 C	1.8
931241	AB1-173AC	1.8
923911	AB2-031 C OI	1.78
923941	AB2-035 C	0.4
923991	AB2-040 C OI	5.86

<i>924151</i>	<i>AB2-059 C OI</i>	<i>10.18</i>
<i>924391</i>	<i>AB2-088 C</i>	<i>0.51</i>
<i>924401</i>	<i>AB2-089 C</i>	<i>1.25</i>
<i>924491</i>	<i>AB2-098 C</i>	<i>0.88</i>
<i>924501</i>	<i>AB2-099 C</i>	<i>0.99</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>7.31</i>
<i>925121</i>	<i>AB2-169 C</i>	<i>11.96</i>
<i>925171</i>	<i>AB2-174 C OI</i>	<i>5.33</i>
<i>925291</i>	<i>AB2-188 C OI</i>	<i>4.86</i>
<i>925591</i>	<i>AC1-034 C</i>	<i>6.59</i>
<i>925781</i>	<i>AC1-054 C</i>	<i>4.54</i>
<i>926071</i>	<i>AC1-086 C</i>	<i>22.31</i>
<i>926201</i>	<i>AC1-098 C</i>	<i>7.94</i>
<i>926211</i>	<i>AC1-099 C</i>	<i>2.66</i>
<i>926771</i>	<i>AC1-163 C</i>	<i>3.28</i>
<i>927021</i>	<i>AC1-189 C</i>	<i>11.67</i>
<i>927141</i>	<i>AC1-208 C</i>	<i>9.96</i>

Appendix 5

(DVP - DVP) The 6EVERETS-AD2-068 TAP 230 kV line (from bus 314574 to bus 936530 ckt 1) loads from 127.94% to 131.48% (**DC power flow**) of its load dump rating (485 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 2058-2181'. This project contributes approximately 17.18 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 2058-2181'

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*

6ROCKYMT230T230.00 - 6HATHAWAY 230.00

OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00

OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-

RMOUNT#4230.00 - 6NASH 230.00

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY
230.00 - 6NASH 230.00

OPEN BUS 314591 /* ISLAND: 6NASH 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	2.96
315292	1DOMTR78	2.
315293	1DOMTR9	1.63
315131	1EDGECEMA	9.28
315132	1EDGECEMB	9.28
315136	1ROSEMG1	1.88
315138	1ROSEMG2	0.88
315137	1ROSEMS1	1.17
314557	3BETHEL	1.15
314554	3BTLEBRO	0.43
314566	3CRESWEL	2.04
314572	3EMPORIA	0.21
314578	3HORNRTN	2.04
314582	3KELFORD	0.72

<i>314603</i>	<i>3SCOT NK</i>	<i>2.51</i>
<i>314617</i>	<i>3TUNIS</i>	<i>0.7</i>
<i>314539</i>	<i>3UNCAMP</i>	<i>1.18</i>
<i>314541</i>	<i>3WATKINS</i>	<i>0.36</i>
<i>314620</i>	<i>6CASHIE</i>	<i>0.88</i>
<i>314574</i>	<i>6EVERETS</i>	<i>5.39</i>
<i>314594</i>	<i>6PLYMOTH</i>	<i>0.83</i>
<i>314648</i>	<i>6SUNBURY</i>	<i>0.4</i>
<i>314651</i>	<i>6WINFALL</i>	<i>0.97</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>6.17</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>3.04</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>13.47</i>
<i>933992</i>	<i>AD1-023 E</i>	<i>7.33</i>
<i>934201</i>	<i>AD1-047 C</i>	<i>4.29</i>
<i>934202</i>	<i>AD1-047 E</i>	<i>2.86</i>
<i>934331</i>	<i>AD1-057 C O1</i>	<i>8.81</i>
<i>934332</i>	<i>AD1-057 E O1</i>	<i>4.7</i>
<i>934521</i>	<i>AD1-076 C O1</i>	<i>54.77</i>
<i>934522</i>	<i>AD1-076 E O1</i>	<i>27.89</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>8.4</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>3.61</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>10.31</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>6.87</i>
<i>936711</i>	<i>AD2-090 C O1</i>	<i>3.91</i>
<i>936712</i>	<i>AD2-090 E O1</i>	<i>2.61</i>
<i>937441</i>	<i>AD2-195 C</i>	<i>12.87</i>

937442	AD2-195 E	5.55
<i>LTF</i>	<i>AMIL</i>	0.48
<i>LTF</i>	<i>BAYOU</i>	2.63
<i>LTF</i>	<i>BIG_CAJUN1</i>	4.15
<i>LTF</i>	<i>BIG_CAJUN2</i>	8.36
<i>LTF</i>	<i>BLUEG</i>	2.48
<i>LTF</i>	<i>CALDERWOOD</i>	1.54
<i>LTF</i>	<i>CANNELTON</i>	0.48
<i>LTF</i>	<i>CATAWBA</i>	1.5
<i>LTF</i>	<i>CBM-N</i>	< 0.01
<i>LTF</i>	<i>CELEVELAND</i>	4.26
<i>LTF</i>	<i>CHEOAH</i>	1.43
<i>LTF</i>	<i>CHILHOWEE</i>	0.5
<i>LTF</i>	<i>CHOCTAW</i>	2.83
<i>LTF</i>	<i>CLIFTY</i>	8.97
<i>LTF</i>	<i>COTTONWOOD</i>	10.28
<i>LTF</i>	<i>DEARBORN</i>	0.89
<i>LTF</i>	<i>EDWARDS</i>	0.77
<i>LTF</i>	<i>ELMERSMITH</i>	1.41
<i>LTF</i>	<i>FARMERCITY</i>	0.62
<i>LTF</i>	<i>G-007A</i>	1.06
<i>LTF</i>	<i>GIBSON</i>	0.87
<i>LTF</i>	<i>HAMLET</i>	6.46
<i>LTF</i>	<i>MORGAN</i>	4.55
<i>LTF</i>	<i>NEWTON</i>	2.14
<i>LTF</i>	<i>NYISO</i>	0.09

<i>LTF</i>	<i>PRAIRIE</i>	<i>4.66</i>
<i>LTF</i>	<i>ROWAN</i>	<i>2.98</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.43</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.42</i>
<i>LTF</i>	<i>TATANKA</i>	<i>1.04</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.91</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.47</i>
<i>LTF</i>	<i>TVA</i>	<i>1.91</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>2.73</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.21</i>
<i>LTF</i>	<i>VFT</i>	<i>2.82</i>
<i>901082</i>	<i>W1-029E</i>	<i>23.4</i>
<i>907092</i>	<i>X1-038 E</i>	<i>2.96</i>
<i>913392</i>	<i>Y1-086 E</i>	<i>1.05</i>
<i>916042</i>	<i>Z1-036 E</i>	<i>29.14</i>
<i>917122</i>	<i>Z2-027 E</i>	<i>0.51</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.37</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.86</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.33</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>1.44</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>6.13</i>
<i>918411</i>	<i>AA1-050</i>	<i>1.22</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>2.44</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>1.83</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>4.84</i>
<i>918531</i>	<i>AA1-067 C</i>	<i>0.7</i>

918532	AA1-067 E	1.62
918561	AA1-072 C	0.06
918562	AA1-072 E	0.14
919692	AA2-053 E	2.58
919702	AA2-057 E	2.12
920042	AA2-088 E	6.25
920592	AA2-165 E	0.28
920672	AA2-174 E	0.3
920691	AA2-178 C	8.16
920692	AA2-178 E	3.5
930051	AB1-013 C	2.46
930052	AB1-013 E	16.48
930401	AB1-081 C	5.64
930402	AB1-081 E	2.42
930861	AB1-132 C	10.36
930862	AB1-132 E	4.44
931231	AB1-173 C	1.21
931232	AB1-173 E	0.56
931241	AB1-173AC	1.21
931242	AB1-173AE	0.56
923801	AB2-015 C O1	4.4
923802	AB2-015 E O1	3.61
923831	AB2-022 C	1.02
923832	AB2-022 E	0.55
923911	AB2-031 C O1	1.2
923912	AB2-031 E O1	0.59

923941	AB2-035 C	0.48
923942	AB2-035 E	0.21
923991	AB2-040 C OI	3.93
923992	AB2-040 E OI	3.22
924151	AB2-059 C OI	6.65
924152	AB2-059 E OI	3.42
924391	AB2-088 C	0.62
924392	AB2-088 E	0.3
924491	AB2-098 C	1.26
924492	AB2-098 E	0.54
924501	AB2-099 C	0.53
924502	AB2-099 E	0.23
924511	AB2-100 C	5.85
924512	AB2-100 E	2.88
925121	AB2-169 C	10.02
925122	AB2-169 E	8.99
925171	AB2-174 C OI	3.64
925172	AB2-174 E OI	3.29
925281	AB2-186 C	0.37
925282	AB2-186 E	0.16
925291	AB2-188 C OI	2.01
925292	AB2-188 E OI	0.9
925591	ACI-034 C	4.3
925592	ACI-034 E	3.25
926071	ACI-086 C	15.26
926072	ACI-086 E	6.95

<i>926201</i>	<i>ACI-098 C</i>	<i>4.33</i>
<i>926202</i>	<i>ACI-098 E</i>	<i>2.58</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>1.45</i>
<i>926212</i>	<i>ACI-099 E</i>	<i>0.85</i>
<i>LTF</i>	<i>ACI-133</i>	<i>22.45</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>1.74</i>
<i>926772</i>	<i>ACI-163 E</i>	<i>0.81</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>15.46</i>
<i>927022</i>	<i>ACI-189 E</i>	<i>7.7</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>5.75</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>2.55</i>

Appendix 6

(DVP - DVP) The 6LAKEVEW-6CAROLNA 230 kV line (from bus 314583 to bus 314561 ckt 1) loads from 133.23% to 134.79% (**DC power flow**) of its emergency rating (375 MVA) for the single line contingency outage of 'DVP_P1-2: LN 254-A'. This project contributes approximately 5.87 MW to the thermal violation.

CONTINGENCY 'DVP_P1-2: LN 254-A'

OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1

/* 6CLUBHSE

230.00 - AB2-100 TAP 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	11.03
315132	1EDGECEMB	11.03
315139	1GASTONA	12.78
315141	1GASTONB	12.78
315136	1ROSEMG1	8.37
315138	1ROSEMG2	3.92
315137	1ROSEMS1	5.19
934331	AD1-057 C O1	23.31
936701	AD2-089 C	5.87
LTF	CARR	0.05
LTF	CBM-S1	2.87
LTF	CBM-S2	5.9
LTF	CBM-W1	6.26
LTF	CBM-W2	15.53
LTF	CIN	1.4
LTF	CPLE	1.98
LTF	IPL	0.89
LTF	LGEE	0.3

<i>LTF</i>	<i>MEC</i>	<i>3.17</i>
<i>LTF</i>	<i>MECS</i>	<i>1.4</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.04</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.31</i>
<i>LTF</i>	<i>WEC</i>	<i>0.39</i>
<i>917341</i>	<i>Z2-044 C</i>	<i>0.14</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>0.61</i>
<i>918411</i>	<i>AA1-050</i>	<i>0.51</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>8.22</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>52.51</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.27</i>
<i>924151</i>	<i>AB2-059 C OI</i>	<i>9.69</i>
<i>924391</i>	<i>AB2-088 C</i>	<i>0.35</i>
<i>924511</i>	<i>AB2-100 C</i>	<i>41.88</i>
<i>925591</i>	<i>AC1-034 C</i>	<i>6.28</i>
<i>926071</i>	<i>AC1-086 C</i>	<i>77.32</i>
<i>927021</i>	<i>AC1-189 C</i>	<i>4.16</i>

Appendix 7

(DVP - DVP) The 6LAKEVEW-AB2-100 TAP 230 kV line (from bus 314583 to bus 924510 ckt 1) loads from 127.88% to 130.73% (**DC power flow**) of its load dump rating (459 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 246T247'. This project contributes approximately 13.05 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 246T247' /* SUFFOLK 230 KV
 OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* 6SUFFOLK
 230.00 - 6NUCO TP 230.00
 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 6EARLEYS
 230.00 - 6NUCO TP 230.00
 OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 6NUCO TP
 230.00 - 6NUCOR 230.00
 OPEN BUS 314575 /* ISLAND: 6NUCO TP 230.00
 OPEN BUS 314590 /* ISLAND: 6NUCOR 230.00
 OPEN BRANCH FROM BUS 314537 TO BUS 314648 CKT 1 /* 6SUFFOLK
 230.00 - 6SUNBURY 230.00
 OPEN BRANCH FROM BUS 314648 TO BUS 901080 CKT 1 /* 6SUNBURY
 230.00 - W1-029 230.00
 OPEN BUS 314648 /* ISLAND: 6SUNBURY 230.00
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	2.01
315131	1EDGECMA	10.47
315132	1EDGECMB	10.47
315139	1GASTONA	7.52
315141	1GASTONB	7.52
315126	1ROARAP2	1.54
315128	1ROARAP4	1.48
315136	1ROSEMG1	5.05
315138	1ROSEMG2	2.36
315137	1ROSEMS1	3.13
314557	3BETHELC	0.87

<i>314554</i>	<i>3BTLEBRO</i>	<i>0.84</i>
<i>314566</i>	<i>3CRESWEL</i>	<i>1.63</i>
<i>314578</i>	<i>3HORNRTN</i>	<i>3.35</i>
<i>314582</i>	<i>3KELFORD</i>	<i>0.91</i>
<i>314603</i>	<i>3SCOT NK</i>	<i>3.54</i>
<i>314617</i>	<i>3TUNIS</i>	<i>0.81</i>
<i>314541</i>	<i>3WATKINS</i>	<i>0.32</i>
<i>314620</i>	<i>6CASHIE</i>	<i>0.83</i>
<i>314574</i>	<i>6EVERETS</i>	<i>2.43</i>
<i>314594</i>	<i>6PLYMOTH</i>	<i>0.69</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>9.33</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>4.59</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>11.94</i>
<i>933992</i>	<i>AD1-023 E</i>	<i>6.5</i>
<i>934331</i>	<i>AD1-057 C O1</i>	<i>16.07</i>
<i>934332</i>	<i>AD1-057 E O1</i>	<i>8.57</i>
<i>934521</i>	<i>AD1-076 C O1</i>	<i>45.25</i>
<i>934522</i>	<i>AD1-076 E O1</i>	<i>23.04</i>
<i>LTF</i>	<i>AD1-120</i>	<i>3.74</i>
<i>LTF</i>	<i>AD1-121</i>	<i>3.71</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>9.84</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>4.22</i>
<i>936531</i>	<i>AD2-068 C</i>	<i>4.66</i>
<i>936532</i>	<i>AD2-068 E</i>	<i>2.4</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>7.83</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>5.22</i>

936711	AD2-090 C OI	3.74
936712	AD2-090 E OI	2.49
LTF	AD2-099	2.89
937441	AD2-195 C	8.25
937442	AD2-195 E	3.56
LTF	CARR	0.09
LTF	CBM-S1	4.48
LTF	CBM-S2	9.25
LTF	CBM-W1	9.73
LTF	CBM-W2	24.21
LTF	CIN	2.18
LTF	CPL	3.17
LTF	G-007	0.62
LTF	IPL	1.39
LTF	LGEE	0.47
LTF	MEC	4.95
LTF	MECS	2.17
LTF	O-066	3.92
LTF	RENSSELAER	0.08
LTF	ROSETON	0.55
900672	V4-068 E	0.24
LTF	WEC	0.6
916042	Z1-036 E	21.78
917331	Z2-043 C	0.48
917332	Z2-043 E	1.1
917341	Z2-044 C	0.26

917342	Z2-044 E	0.61
917511	Z2-088 C OPI	0.97
917512	Z2-088 E OPI	4.12
918411	AA1-050	0.82
918491	AA1-063AC OP	1.38
918492	AA1-063AE OP	3.51
918511	AA1-065 C OP	2.01
918512	AA1-065 E OP	5.34
918531	AA1-067 C	0.32
918532	AA1-067 E	0.73
918561	AA1-072 C	0.07
918562	AA1-072 E	0.18
919691	AA2-053 C	1.67
919692	AA2-053 E	3.86
919701	AA2-057 C	1.39
919702	AA2-057 E	3.73
LTF	AA2-074	2.16
920042	AA2-088 E	6.94
920591	AA2-165 C	0.19
920592	AA2-165 E	0.49
920671	AA2-174 C	0.08
920672	AA2-174 E	0.45
920691	AA2-178 C	6.54
920692	AA2-178 E	2.8
930051	ABI-013 C	1.97
930052	ABI-013 E	13.2

930401	ABI-081 C	9.52
930402	ABI-081 E	4.08
930861	ABI-132 C	30.89
930862	ABI-132 E	13.24
923941	AB2-035 C	0.37
923942	AB2-035 E	0.16
924151	AB2-059 C OI	11.22
924152	AB2-059 E OI	5.78
924391	AB2-088 C	0.47
924392	AB2-088 E	0.23
924491	AB2-098 C	0.57
924492	AB2-098 E	0.24
924501	AB2-099 C	0.61
924502	AB2-099 E	0.26
925121	AB2-169 C	5.87
925122	AB2-169 E	5.27
925281	AB2-186 C	0.27
925282	AB2-186 E	0.12
925291	AB2-188 C OI	1.61
925292	AB2-188 E OI	0.72
925591	ACI-034 C	7.27
925592	ACI-034 E	5.48
925781	ACI-054 C	3.7
925782	ACI-054 E	1.71
926071	ACI-086 C	45.48
926072	ACI-086 E	20.7

<i>926201</i>	<i>ACI-098 C</i>	<i>6.54</i>
<i>926202</i>	<i>ACI-098 E</i>	<i>3.9</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>2.19</i>
<i>926212</i>	<i>ACI-099 E</i>	<i>1.29</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>2.03</i>
<i>926772</i>	<i>ACI-163 E</i>	<i>0.95</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>8.99</i>
<i>927022</i>	<i>ACI-189 E</i>	<i>4.48</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>9.4</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>4.18</i>

Appendix 8

(DVP - DVP) The 6ELIZ CT-6SHAWBRO 230 kV line (from bus 314638 to bus 314647 ckt 1) loads from 134.93% to 136.22% (**DC power flow**) of its load dump rating (699 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 246T247'. This project contributes approximately 9.0 MW to the thermal violation.

```

CONTINGENCY 'DVP_P4-2: 246T247'                               /* SUFFOLK 230 KV
  OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1           /* 6SUFFOLK
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1           /* 6EARLEYS
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1           /* 6NUCO TP
230.00 - 6NUCOR 230.00
  OPEN BUS 314575                                             /* ISLAND: 6NUCO TP 230.00
  OPEN BUS 314590                                             /* ISLAND: 6NUCOR 230.00
  OPEN BRANCH FROM BUS 314537 TO BUS 314648 CKT 1           /* 6SUFFOLK
230.00 - 6SUNBURY 230.00
  OPEN BRANCH FROM BUS 314648 TO BUS 901080 CKT 1           /* 6SUNBURY
230.00 - W1-029 230.00
  OPEN BUS 314648                                             /* ISLAND: 6SUNBURY 230.00
END
  
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	4.65
315292	1DOMTR78	3.14
315293	1DOMTR9	2.57
315139	1GASTONA	2.11
315141	1GASTONB	2.11
315136	1ROSEMG1	1.5
315138	1ROSEMG2	0.7
315137	1ROSEMS1	0.93
314557	3BETHELC	0.6
314566	3CRESWEL	6.73
314582	3KELFORD	0.78

<i>314603</i>	<i>3SCOT NK</i>	<i>2.7</i>
<i>314617</i>	<i>3TUNIS</i>	<i>0.7</i>
<i>314620</i>	<i>6CASHIE</i>	<i>1.59</i>
<i>314574</i>	<i>6EVERETS</i>	<i>2.49</i>
<i>314594</i>	<i>6PLYMOTH</i>	<i>2.03</i>
<i>314651</i>	<i>6WINFALL</i>	<i>6.57</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>6.53</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>3.22</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>27.52</i>
<i>933992</i>	<i>AD1-023 E</i>	<i>14.98</i>
<i>934521</i>	<i>AD1-076 C O1</i>	<i>125.48</i>
<i>934522</i>	<i>AD1-076 E O1</i>	<i>63.89</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>9.28</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>3.99</i>
<i>936531</i>	<i>AD2-068 C</i>	<i>4.44</i>
<i>936532</i>	<i>AD2-068 E</i>	<i>2.29</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>5.4</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>3.6</i>
<i>937441</i>	<i>AD2-195 C</i>	<i>17.9</i>
<i>937442</i>	<i>AD2-195 E</i>	<i>7.72</i>
<i>LTF</i>	<i>CARR</i>	<i>0.06</i>
<i>LTF</i>	<i>CBM-S1</i>	<i>3.22</i>
<i>LTF</i>	<i>CBM-S2</i>	<i>6.64</i>
<i>LTF</i>	<i>CBM-W1</i>	<i>7.05</i>
<i>LTF</i>	<i>CBM-W2</i>	<i>17.42</i>
<i>LTF</i>	<i>CIN</i>	<i>1.58</i>

<i>LTF</i>	<i>CPLE</i>	<i>2.3</i>
<i>LTF</i>	<i>G-007</i>	<i>0.43</i>
<i>LTF</i>	<i>IPL</i>	<i>1.01</i>
<i>LTF</i>	<i>LGEE</i>	<i>0.34</i>
<i>LTF</i>	<i>MEC</i>	<i>3.58</i>
<i>LTF</i>	<i>MECS</i>	<i>1.59</i>
<i>LTF</i>	<i>O-066</i>	<i>2.73</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.05</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.37</i>
<i>900671</i>	<i>V4-068 C</i>	<i>0.06</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.18</i>
<i>901081</i>	<i>W1-029C</i>	<i>4.76</i>
<i>901082</i>	<i>W1-029E</i>	<i>171.41</i>
<i>LTF</i>	<i>WEC</i>	<i>0.43</i>
<i>913391</i>	<i>Y1-086 C</i>	<i>1.02</i>
<i>913392</i>	<i>Y1-086 E</i>	<i>8.99</i>
<i>916041</i>	<i>Z1-036 C</i>	<i>4.38</i>
<i>916042</i>	<i>Z1-036 E</i>	<i>157.7</i>
<i>917121</i>	<i>Z2-027 C</i>	<i>1.89</i>
<i>917122</i>	<i>Z2-027 E</i>	<i>4.35</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.41</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.94</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>0.73</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>3.1</i>
<i>918411</i>	<i>AA1-050</i>	<i>0.62</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>2.11</i>

918512	AA1-065 E OP	5.58
918531	AA1-067 C	0.32
918532	AA1-067 E	0.75
918561	AA1-072 C	0.06
918562	AA1-072 E	0.16
919691	AA2-053 C	1.09
919692	AA2-053 E	2.52
919701	AA2-057 C	0.84
919702	AA2-057 E	2.26
LTF	AA2-074	1.57
920591	AA2-165 C	0.11
920592	AA2-165 E	0.3
920671	AA2-174 C	0.05
920672	AA2-174 E	0.29
920691	AA2-178 C	26.93
920692	AA2-178 E	11.54
930051	AB1-013 C	8.13
930052	AB1-013 E	54.39
930861	AB1-132 C	8.68
930862	AB1-132 E	3.72
923831	AB2-022 C	9.92
923832	AB2-022 E	5.34
923941	AB2-035 C	0.25
923942	AB2-035 E	0.11
924391	AB2-088 C	0.32
924392	AB2-088 E	0.16

924491	AB2-098 C	0.58
924492	AB2-098 E	0.25
924501	AB2-099 C	0.56
924502	AB2-099 E	0.24
925121	AB2-169 C	11.25
925122	AB2-169 E	10.1
925281	AB2-186 C	2.19
925282	AB2-186 E	0.94
925291	AB2-188 C OI	6.64
925292	AB2-188 E OI	2.98
926071	AC1-086 C	12.79
926072	AC1-086 E	5.82
926201	AC1-098 C	4.58
926202	AC1-098 E	2.73
926211	AC1-099 C	1.54
926212	AC1-099 E	0.9
926771	AC1-163 C	1.84
926772	AC1-163 E	0.86
927021	AC1-189 C	7.54
927022	AC1-189 E	3.75
927141	AC1-208 C	5.8
927142	AC1-208 E	2.58

Appendix 9

(DVP - DVP) The 6S HERTFORD-6WINFALL 230 kV line (from bus 314662 to bus 314651 ckt 1) loads from 107.32% to 108.48% (**DC power flow**) of its load dump rating (897 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 24682'. This project contributes approximately 10.4 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 24682' /* 24682 @ SUFFOLK
 OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* SUFFOLK -
 NUCOR TAP
 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* NUCOR TAP -
 EARLEYS
 OPEN BRANCH FROM BUS 314536 TO BUS 314537 CKT 2 /* SUFFOLK 230-
 115 TX#5
 OPEN BRANCH FROM BUS 314928 TO BUS 314537 CKT 2 /* SUFFOLK 500-
 230 TX#8
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	5.38
315292	1DOMTR78	3.64
315293	1DOMTR9	2.97
315131	1EDGECEMA	6.42
315132	1EDGECEMB	6.42
315139	1GASTONA	2.44
315141	1GASTONB	2.44
315136	1ROSEMG1	1.73
315138	1ROSEMG2	0.81
315137	1ROSEMS1	1.07
314557	3BETHEL	0.69
314554	3BTLEBRO	0.54
314566	3CRESWEL	7.79
314578	3HORNRTN	2.19

314582	3KELFORD	0.9
314603	3SCOT NK	3.1
314617	3TUNIS	0.8
314620	6CASHIE	1.83
314574	6EVERETS	2.87
314594	6PLYMOTH	2.34
932631	AC2-084 C	7.52
932632	AC2-084 E	3.7
933991	AD1-023 C	31.82
933992	AD1-023 E	17.32
934331	AD1-057 C O1	7.
934332	AD1-057 E O1	3.74
934521	AD1-076 C O1	145.1
934522	AD1-076 E O1	73.89
936401	AD2-051 C O1	10.69
936402	AD2-051 E O1	4.59
936531	AD2-068 C	5.13
936532	AD2-068 E	2.65
936701	AD2-089 C	6.24
936702	AD2-089 E	4.16
LTF	AD2-099	2.43
937441	AD2-195 C	20.7
937442	AD2-195 E	8.92
LTF	CARR	0.06
LTF	CBM-S1	3.82
LTF	CBM-S2	7.76

<i>LTF</i>	<i>CBM-W1</i>	<i>8.49</i>
<i>LTF</i>	<i>CBM-W2</i>	<i>20.69</i>
<i>LTF</i>	<i>CIN</i>	<i>1.9</i>
<i>LTF</i>	<i>CPLE</i>	<i>2.68</i>
<i>LTF</i>	<i>G-007</i>	<i>0.47</i>
<i>LTF</i>	<i>IPL</i>	<i>1.21</i>
<i>LTF</i>	<i>LGEE</i>	<i>0.41</i>
<i>LTF</i>	<i>MEC</i>	<i>4.27</i>
<i>LTF</i>	<i>MECS</i>	<i>1.94</i>
<i>LTF</i>	<i>O-066</i>	<i>2.95</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.05</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.36</i>
<i>900671</i>	<i>V4-068 C</i>	<i>0.07</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.21</i>
<i>LTF</i>	<i>WEC</i>	<i>0.52</i>
<i>916041</i>	<i>Z1-036 C</i>	<i>5.06</i>
<i>916042</i>	<i>Z1-036 E</i>	<i>182.46</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.47</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>1.08</i>
<i>917341</i>	<i>Z2-044 C</i>	<i>0.18</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.41</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>0.84</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>3.58</i>
<i>918411</i>	<i>AA1-050</i>	<i>0.71</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>2.43</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>6.44</i>

918531	AA1-067 C	0.37
918532	AA1-067 E	0.86
918561	AA1-072 C	0.07
918562	AA1-072 E	0.18
919691	AA2-053 C	1.25
919692	AA2-053 E	2.9
919701	AA2-057 C	0.97
919702	AA2-057 E	2.6
LTF	AA2-074	1.83
920591	AA2-165 C	0.13
920592	AA2-165 E	0.34
920671	AA2-174 C	0.06
920672	AA2-174 E	0.33
920691	AA2-178 C	31.15
920692	AA2-178 E	13.35
930051	AB1-013 C	9.4
930052	AB1-013 E	62.92
930401	AB1-081 C	6.09
930402	AB1-081 E	2.61
930861	AB1-132 C	10.01
930862	AB1-132 E	4.29
923941	AB2-035 C	0.29
923942	AB2-035 E	0.12
924151	AB2-059 C OI	7.18
924152	AB2-059 E OI	3.7
924391	AB2-088 C	0.37

924392	<i>AB2-088 E</i>	<i>0.18</i>
924491	<i>AB2-098 C</i>	<i>0.67</i>
924492	<i>AB2-098 E</i>	<i>0.29</i>
924501	<i>AB2-099 C</i>	<i>0.64</i>
924502	<i>AB2-099 E</i>	<i>0.27</i>
925121	<i>AB2-169 C</i>	<i>13.01</i>
925122	<i>AB2-169 E</i>	<i>11.67</i>
925281	<i>AB2-186 C</i>	<i>2.54</i>
925282	<i>AB2-186 E</i>	<i>1.09</i>
925291	<i>AB2-188 C OI</i>	<i>7.68</i>
925292	<i>AB2-188 E OI</i>	<i>3.45</i>
925591	<i>ACI-034 C</i>	<i>4.65</i>
925592	<i>ACI-034 E</i>	<i>3.51</i>
926071	<i>ACI-086 C</i>	<i>14.73</i>
926072	<i>ACI-086 E</i>	<i>6.71</i>
926201	<i>ACI-098 C</i>	<i>5.27</i>
926202	<i>ACI-098 E</i>	<i>3.14</i>
926211	<i>ACI-099 C</i>	<i>1.77</i>
926212	<i>ACI-099 E</i>	<i>1.04</i>
926771	<i>ACI-163 C</i>	<i>2.11</i>
926772	<i>ACI-163 E</i>	<i>0.99</i>
927021	<i>ACI-189 C</i>	<i>8.71</i>
927022	<i>ACI-189 E</i>	<i>4.34</i>
927141	<i>ACI-208 C</i>	<i>6.67</i>
927142	<i>ACI-208 E</i>	<i>2.96</i>

Appendix 10

(DVP - DVP) The Z1-036 TAP-6S HERTFORD 230 kV line (from bus 916040 to bus 314662 ckt 1) loads from 108.68% to 109.84% (**DC power flow**) of its load dump rating (897 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 24682'. This project contributes approximately 10.4 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 24682' /* 24682 @ SUFFOLK
 OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1 /* SUFFOLK -
 NUCOR TAP
 OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* NUCOR TAP -
 EARLEYS
 OPEN BRANCH FROM BUS 314536 TO BUS 314537 CKT 2 /* SUFFOLK 230-
 115 TX#5
 OPEN BRANCH FROM BUS 314928 TO BUS 314537 CKT 2 /* SUFFOLK 500-
 230 TX#8
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	5.38
315292	1DOMTR78	3.64
315293	1DOMTR9	2.97
315131	1EDGECEMA	6.42
315132	1EDGECEMB	6.42
315139	1GASTONA	2.44
315141	1GASTONB	2.44
315136	1ROSEMG1	1.73
315138	1ROSEMG2	0.81
315137	1ROSEMS1	1.07
314557	3BETHEL	0.69
314554	3BTLEBRO	0.54
314566	3CRESWEL	7.79
314578	3HORNRTN	2.19

314582	3KELFORD	0.9
314603	3SCOT NK	3.1
314617	3TUNIS	0.8
314620	6CASHIE	1.83
314574	6EVERETS	2.87
314594	6PLYMOTH	2.34
932631	AC2-084 C	7.52
932632	AC2-084 E	3.7
933991	AD1-023 C	31.82
933992	AD1-023 E	17.32
934331	AD1-057 C O1	7.
934332	AD1-057 E O1	3.74
934521	AD1-076 C O1	145.1
934522	AD1-076 E O1	73.89
936401	AD2-051 C O1	10.69
936402	AD2-051 E O1	4.59
936531	AD2-068 C	5.13
936532	AD2-068 E	2.65
936701	AD2-089 C	6.24
936702	AD2-089 E	4.16
LTF	AD2-099	2.43
937441	AD2-195 C	20.7
937442	AD2-195 E	8.92
LTF	CARR	0.06
LTF	CBM-S1	3.82
LTF	CBM-S2	7.76

<i>LTF</i>	<i>CBM-W1</i>	8.49
<i>LTF</i>	<i>CBM-W2</i>	20.69
<i>LTF</i>	<i>CIN</i>	1.9
<i>LTF</i>	<i>CPLE</i>	2.68
<i>LTF</i>	<i>G-007</i>	0.47
<i>LTF</i>	<i>IPL</i>	1.21
<i>LTF</i>	<i>LGEE</i>	0.41
<i>LTF</i>	<i>MEC</i>	4.27
<i>LTF</i>	<i>MECS</i>	1.94
<i>LTF</i>	<i>O-066</i>	2.95
<i>LTF</i>	<i>RENSSELAER</i>	0.05
<i>LTF</i>	<i>ROSETON</i>	0.36
900671	<i>V4-068 C</i>	0.07
900672	<i>V4-068 E</i>	0.21
<i>LTF</i>	<i>WEC</i>	0.52
916041	<i>Z1-036 C</i>	5.06
916042	<i>Z1-036 E</i>	182.46
917331	<i>Z2-043 C</i>	0.47
917332	<i>Z2-043 E</i>	1.08
917341	<i>Z2-044 C</i>	0.18
917342	<i>Z2-044 E</i>	0.41
917511	<i>Z2-088 C OPI</i>	0.84
917512	<i>Z2-088 E OPI</i>	3.58
918411	<i>AA1-050</i>	0.71
918511	<i>AA1-065 C OP</i>	2.43
918512	<i>AA1-065 E OP</i>	6.44

918531	AAI-067 C	0.37
918532	AAI-067 E	0.86
918561	AAI-072 C	0.07
918562	AAI-072 E	0.18
919691	AA2-053 C	1.25
919692	AA2-053 E	2.9
919701	AA2-057 C	0.97
919702	AA2-057 E	2.6
LTF	AA2-074	1.83
920591	AA2-165 C	0.13
920592	AA2-165 E	0.34
920671	AA2-174 C	0.06
920672	AA2-174 E	0.33
920691	AA2-178 C	31.15
920692	AA2-178 E	13.35
930051	ABI-013 C	9.4
930052	ABI-013 E	62.92
930401	ABI-081 C	6.09
930402	ABI-081 E	2.61
930861	ABI-132 C	10.01
930862	ABI-132 E	4.29
923941	AB2-035 C	0.29
923942	AB2-035 E	0.12
924151	AB2-059 C OI	7.18
924152	AB2-059 E OI	3.7
924391	AB2-088 C	0.37

924392	<i>AB2-088 E</i>	<i>0.18</i>
924491	<i>AB2-098 C</i>	<i>0.67</i>
924492	<i>AB2-098 E</i>	<i>0.29</i>
924501	<i>AB2-099 C</i>	<i>0.64</i>
924502	<i>AB2-099 E</i>	<i>0.27</i>
925121	<i>AB2-169 C</i>	<i>13.01</i>
925122	<i>AB2-169 E</i>	<i>11.67</i>
925291	<i>AB2-188 C OI</i>	<i>7.68</i>
925292	<i>AB2-188 E OI</i>	<i>3.45</i>
925591	<i>ACI-034 C</i>	<i>4.65</i>
925592	<i>ACI-034 E</i>	<i>3.51</i>
926071	<i>ACI-086 C</i>	<i>14.73</i>
926072	<i>ACI-086 E</i>	<i>6.71</i>
926201	<i>ACI-098 C</i>	<i>5.27</i>
926202	<i>ACI-098 E</i>	<i>3.14</i>
926211	<i>ACI-099 C</i>	<i>1.77</i>
926212	<i>ACI-099 E</i>	<i>1.04</i>
926771	<i>ACI-163 C</i>	<i>2.11</i>
926772	<i>ACI-163 E</i>	<i>0.99</i>
927021	<i>ACI-189 C</i>	<i>8.71</i>
927022	<i>ACI-189 E</i>	<i>4.34</i>
927141	<i>ACI-208 C</i>	<i>6.67</i>
927142	<i>ACI-208 E</i>	<i>2.96</i>

Appendix 11

(DVP - DVP) The AB2-100 TAP-6CLUBHSE 230 kV line (from bus 924510 to bus 314563 ckt 1) loads from 141.69% to 144.54% (**DC power flow**) of its load dump rating (459 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 246T247'. This project contributes approximately 13.05 MW to the thermal violation.

```

CONTINGENCY 'DVP_P4-2: 246T247'                               /* SUFFOLK 230 KV
  OPEN BRANCH FROM BUS 314537 TO BUS 314575 CKT 1           /* 6SUFFOLK
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1           /* 6EARLEYS
230.00 - 6NUCO TP 230.00
  OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1           /* 6NUCO TP
230.00 - 6NUCOR 230.00
  OPEN BUS 314575                                             /* ISLAND: 6NUCO TP 230.00
  OPEN BUS 314590                                             /* ISLAND: 6NUCOR 230.00
  OPEN BRANCH FROM BUS 314537 TO BUS 314648 CKT 1           /* 6SUFFOLK
230.00 - 6SUNBURY 230.00
  OPEN BRANCH FROM BUS 314648 TO BUS 901080 CKT 1           /* 6SUNBURY
230.00 - W1-029 230.00
  OPEN BUS 314648                                             /* ISLAND: 6SUNBURY 230.00
END
  
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	2.01
315131	1EDGECEMA	10.47
315132	1EDGECEMB	10.47
315139	1GASTONA	7.52
315141	1GASTONB	7.52
315126	1ROARAP2	1.54
315128	1ROARAP4	1.48
315136	1ROSEMG1	5.05
315138	1ROSEMG2	2.36
315137	1ROSEMS1	3.13
314557	3BETHEL C	0.87

<i>314554</i>	<i>3BTLEBRO</i>	<i>0.84</i>
<i>314566</i>	<i>3CRESWEL</i>	<i>1.63</i>
<i>314578</i>	<i>3HORNRTN</i>	<i>3.35</i>
<i>314582</i>	<i>3KELFORD</i>	<i>0.91</i>
<i>314603</i>	<i>3SCOT NK</i>	<i>3.54</i>
<i>314617</i>	<i>3TUNIS</i>	<i>0.81</i>
<i>314541</i>	<i>3WATKINS</i>	<i>0.32</i>
<i>314620</i>	<i>6CASHIE</i>	<i>0.83</i>
<i>314574</i>	<i>6EVERETS</i>	<i>2.43</i>
<i>314594</i>	<i>6PLYMOTH</i>	<i>0.69</i>
<i>932631</i>	<i>AC2-084 C</i>	<i>9.33</i>
<i>932632</i>	<i>AC2-084 E</i>	<i>4.59</i>
<i>933991</i>	<i>AD1-023 C</i>	<i>11.94</i>
<i>933992</i>	<i>AD1-023 E</i>	<i>6.5</i>
<i>934331</i>	<i>AD1-057 C O1</i>	<i>16.07</i>
<i>934332</i>	<i>AD1-057 E O1</i>	<i>8.57</i>
<i>934521</i>	<i>AD1-076 C O1</i>	<i>45.25</i>
<i>934522</i>	<i>AD1-076 E O1</i>	<i>23.04</i>
<i>LTF</i>	<i>AD1-120</i>	<i>3.74</i>
<i>LTF</i>	<i>AD1-121</i>	<i>3.71</i>
<i>936401</i>	<i>AD2-051 C O1</i>	<i>9.84</i>
<i>936402</i>	<i>AD2-051 E O1</i>	<i>4.22</i>
<i>936531</i>	<i>AD2-068 C</i>	<i>4.66</i>
<i>936532</i>	<i>AD2-068 E</i>	<i>2.4</i>
<i>936701</i>	<i>AD2-089 C</i>	<i>7.83</i>
<i>936702</i>	<i>AD2-089 E</i>	<i>5.22</i>

936711	AD2-090 C OI	3.74
936712	AD2-090 E OI	2.49
LTF	AD2-099	2.89
937441	AD2-195 C	8.25
937442	AD2-195 E	3.56
LTF	CARR	0.09
LTF	CBM-S1	4.48
LTF	CBM-S2	9.25
LTF	CBM-W1	9.73
LTF	CBM-W2	24.21
LTF	CIN	2.18
LTF	CPL	3.17
LTF	G-007	0.62
LTF	IPL	1.39
LTF	LGEE	0.47
LTF	MEC	4.95
LTF	MECS	2.17
LTF	O-066	3.92
LTF	RENSSELAER	0.08
LTF	ROSETON	0.55
900672	V4-068 E	0.24
LTF	WEC	0.6
916042	Z1-036 E	21.78
917331	Z2-043 C	0.48
917332	Z2-043 E	1.1
917341	Z2-044 C	0.26

917342	Z2-044 E	0.61
917511	Z2-088 C OPI	0.97
917512	Z2-088 E OPI	4.12
918411	AA1-050	0.82
918491	AA1-063AC OP	1.38
918492	AA1-063AE OP	3.51
918511	AA1-065 C OP	2.01
918512	AA1-065 E OP	5.34
918531	AA1-067 C	0.32
918532	AA1-067 E	0.73
918561	AA1-072 C	0.07
918562	AA1-072 E	0.18
919691	AA2-053 C	1.67
919692	AA2-053 E	3.86
919701	AA2-057 C	1.39
919702	AA2-057 E	3.73
LTF	AA2-074	2.16
920042	AA2-088 E	6.94
920591	AA2-165 C	0.19
920592	AA2-165 E	0.49
920671	AA2-174 C	0.08
920672	AA2-174 E	0.45
920691	AA2-178 C	6.54
920692	AA2-178 E	2.8
930051	ABI-013 C	1.97
930052	ABI-013 E	13.2

930401	ABI-081 C	9.52
930402	ABI-081 E	4.08
930861	ABI-132 C	30.89
930862	ABI-132 E	13.24
923941	AB2-035 C	0.37
923942	AB2-035 E	0.16
924151	AB2-059 C OI	11.22
924152	AB2-059 E OI	5.78
924391	AB2-088 C	0.47
924392	AB2-088 E	0.23
924491	AB2-098 C	0.57
924492	AB2-098 E	0.24
924501	AB2-099 C	0.61
924502	AB2-099 E	0.26
924511	AB2-100 C	42.68
924512	AB2-100 E	21.02
925121	AB2-169 C	5.87
925122	AB2-169 E	5.27
925291	AB2-188 C OI	1.61
925292	AB2-188 E OI	0.72
925591	ACI-034 C	7.27
925592	ACI-034 E	5.48
925781	ACI-054 C	3.7
925782	ACI-054 E	1.71
926071	ACI-086 C	45.48
926072	ACI-086 E	20.7

<i>926201</i>	<i>ACI-098 C</i>	<i>6.54</i>
<i>926202</i>	<i>ACI-098 E</i>	<i>3.9</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>2.19</i>
<i>926212</i>	<i>ACI-099 E</i>	<i>1.29</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>2.03</i>
<i>926772</i>	<i>ACI-163 E</i>	<i>0.95</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>8.99</i>
<i>927022</i>	<i>ACI-189 E</i>	<i>4.48</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>9.4</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>4.18</i>

Appendix 12

(DVP - CPLE) The AD2-068 TAP-6GREENVILE T 230 kV line (from bus 936530 to bus 304451 ckt 1) loads from 135.19% to 138.78% (**DC power flow**) of its emergency rating (478 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 2058-2181'. This project contributes approximately 17.18 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 2058-2181'

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*

6ROCKYMT230T230.00 - 6HATHAWAY 230.00

OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00

OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-

RMOUNT#4230.00 - 6NASH 230.00

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY
230.00 - 6NASH 230.00

OPEN BUS 314591 /* ISLAND: 6NASH 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315294	1DOMTR10	2.96
315292	1DOMTR78	2.
315293	1DOMTR9	1.63
315131	1EDGECEMA	9.28
315132	1EDGECEMB	9.28
315136	1ROSEMG1	1.88
315138	1ROSEMG2	0.88
315137	1ROSEMS1	1.17
314557	3BETHEL	1.15
314554	3BTLEBRO	0.43
314566	3CRESWEL	2.04
314572	3EMPORIA	0.21
314578	3HORNRTN	2.04
314582	3KELFORD	0.72

314603	3SCOT NK	2.51
314617	3TUNIS	0.7
314539	3UNCAMP	1.18
314541	3WATKINS	0.36
314620	6CASHIE	0.88
314574	6EVERETS	5.39
314594	6PLYMOTH	0.83
314648	6SUNBURY	0.4
314651	6WINFALL	0.97
932631	AC2-084 C	6.17
932632	AC2-084 E	3.04
933991	AD1-023 C	13.47
933992	AD1-023 E	7.33
934201	AD1-047 C	4.29
934202	AD1-047 E	2.86
934331	AD1-057 C O1	8.81
934332	AD1-057 E O1	4.7
934521	AD1-076 C O1	54.77
934522	AD1-076 E O1	27.89
936401	AD2-051 C O1	8.4
936402	AD2-051 E O1	3.61
936531	AD2-068 C	17.02
936532	AD2-068 E	8.77
936701	AD2-089 C	10.31
936702	AD2-089 E	6.87
936711	AD2-090 C O1	3.91

936712	AD2-090 E O1	2.61
937441	AD2-195 C	12.87
937442	AD2-195 E	5.55
LTF	AMIL	0.48
LTF	BAYOU	2.63
LTF	BIG_CAJUN1	4.15
LTF	BIG_CAJUN2	8.36
LTF	BLUEG	2.48
LTF	CALDERWOOD	1.54
LTF	CANNELTON	0.48
LTF	CATAWBA	1.5
LTF	CBM-N	< 0.01
LTF	CELEVELAND	4.26
LTF	CHEOAH	1.43
LTF	CHILHOWEE	0.5
LTF	CHOCTAW	2.83
LTF	CLIFTY	8.97
LTF	COTTONWOOD	10.28
LTF	DEARBORN	0.89
LTF	EDWARDS	0.77
LTF	ELMERSMITH	1.41
LTF	FARMERCITY	0.62
LTF	G-007A	1.06
LTF	GIBSON	0.87
LTF	HAMLET	6.46
LTF	MORGAN	4.55

<i>LTF</i>	<i>NEWTON</i>	<i>2.14</i>
<i>LTF</i>	<i>NYISO</i>	<i>0.09</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>4.66</i>
<i>LTF</i>	<i>ROWAN</i>	<i>2.98</i>
<i>LTF</i>	<i>SANTEETLA</i>	<i>0.43</i>
<i>LTF</i>	<i>SMITHLAND</i>	<i>0.42</i>
<i>LTF</i>	<i>TATANKA</i>	<i>1.04</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.91</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.47</i>
<i>LTF</i>	<i>TVA</i>	<i>1.91</i>
<i>LTF</i>	<i>UNIONPOWER</i>	<i>2.73</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.21</i>
<i>LTF</i>	<i>VFT</i>	<i>2.82</i>
<i>901082</i>	<i>W1-029E</i>	<i>23.4</i>
<i>907092</i>	<i>X1-038 E</i>	<i>2.96</i>
<i>913392</i>	<i>Y1-086 E</i>	<i>1.05</i>
<i>916042</i>	<i>Z1-036 E</i>	<i>29.14</i>
<i>917122</i>	<i>Z2-027 E</i>	<i>0.51</i>
<i>917331</i>	<i>Z2-043 C</i>	<i>0.37</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.86</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.33</i>
<i>917511</i>	<i>Z2-088 C OPI</i>	<i>1.44</i>
<i>917512</i>	<i>Z2-088 E OPI</i>	<i>6.13</i>
<i>918411</i>	<i>AA1-050</i>	<i>1.22</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>2.44</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>1.83</i>

918512	AA1-065 E OP	4.84
918531	AA1-067 C	0.7
918532	AA1-067 E	1.62
918561	AA1-072 C	0.06
918562	AA1-072 E	0.14
919692	AA2-053 E	2.58
919702	AA2-057 E	2.12
920042	AA2-088 E	6.25
920592	AA2-165 E	0.28
920672	AA2-174 E	0.3
920691	AA2-178 C	8.16
920692	AA2-178 E	3.5
930051	AB1-013 C	2.46
930052	AB1-013 E	16.48
930401	AB1-081 C	5.64
930402	AB1-081 E	2.42
930861	AB1-132 C	10.36
930862	AB1-132 E	4.44
931231	AB1-173 C	1.21
931232	AB1-173 E	0.56
931241	AB1-173AC	1.21
931242	AB1-173AE	0.56
923801	AB2-015 C OI	4.4
923802	AB2-015 E OI	3.61
923831	AB2-022 C	1.02
923832	AB2-022 E	0.55

923911	AB2-031 C OI	1.2
923912	AB2-031 E OI	0.59
923941	AB2-035 C	0.48
923942	AB2-035 E	0.21
923991	AB2-040 C OI	3.93
923992	AB2-040 E OI	3.22
924151	AB2-059 C OI	6.65
924152	AB2-059 E OI	3.42
924391	AB2-088 C	0.62
924392	AB2-088 E	0.3
924491	AB2-098 C	1.26
924492	AB2-098 E	0.54
924501	AB2-099 C	0.53
924502	AB2-099 E	0.23
924511	AB2-100 C	5.85
924512	AB2-100 E	2.88
925121	AB2-169 C	10.02
925122	AB2-169 E	8.99
925171	AB2-174 C OI	3.64
925172	AB2-174 E OI	3.29
925281	AB2-186 C	0.37
925282	AB2-186 E	0.16
925291	AB2-188 C OI	2.01
925292	AB2-188 E OI	0.9
925591	AC1-034 C	4.3
925592	AC1-034 E	3.25

<i>926071</i>	<i>ACI-086 C</i>	<i>15.26</i>
<i>926072</i>	<i>ACI-086 E</i>	<i>6.95</i>
<i>926201</i>	<i>ACI-098 C</i>	<i>4.33</i>
<i>926202</i>	<i>ACI-098 E</i>	<i>2.58</i>
<i>926211</i>	<i>ACI-099 C</i>	<i>1.45</i>
<i>926212</i>	<i>ACI-099 E</i>	<i>0.85</i>
<i>LTF</i>	<i>ACI-133</i>	<i>22.45</i>
<i>926771</i>	<i>ACI-163 C</i>	<i>1.74</i>
<i>926772</i>	<i>ACI-163 E</i>	<i>0.81</i>
<i>927021</i>	<i>ACI-189 C</i>	<i>15.46</i>
<i>927022</i>	<i>ACI-189 E</i>	<i>7.7</i>
<i>927141</i>	<i>ACI-208 C</i>	<i>5.75</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>2.55</i>

Appendix 13

(AEP - AEP) The 05EDAN 1-05DANVL2 138 kV line (from bus 242631 to bus 242620 ckt 1) loads from 136.58% to 137.15% (**DC power flow**) of its emergency rating (415 MVA) for the line fault with failed breaker contingency outage of 'AEP_P4_#7589_05J.FERR 765'. This project contributes approximately 5.29 MW to the thermal violation.

CONTINGENCY 'AEP_P4_#7589_05J.FERR 765'

OPEN BRANCH FROM BUS 242514 TO BUS 242520 CKT 1 / 242514 05J.FERR
765 242520 05J.FERR 500 1

OPEN BRANCH FROM BUS 242514 TO BUS 242684 CKT 2 / 242514 05J.FERR
765 242684 05J.FERR 138 2

OPEN BRANCH FROM BUS 242520 TO BUS 306719 CKT 1 / 242520 05J.FERR
500 306719 8ANTIOCH 500 1

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
244012	05PINNACLE	-2.08
315150	1BUGGS 1	4.75
315151	1BUGGS 2	4.75
315131	1EDGECEMA	4.26
315132	1EDGECEMB	4.26
314557	3BETHEL C	0.35
314554	3BTLEBRO	0.37
314572	3EMPORIA	0.14
314578	3HORNRTN	1.22
314582	3KELFORD	0.3
314603	3SCOT NK	1.24
314617	3TUNIS	0.28
314620	6CASHIE	0.27
314574	6EVERETS	0.98
314594	6PLYMOTH	0.26

932631	AC2-084 C	3.43
932632	AC2-084 E	1.69
932701	AC2-093 C	24.45
932702	AC2-093 E	13.99
932761	AC2-100 C	3.67
932762	AC2-100 E	1.79
932821	AC2-107 C	3.49
932822	AC2-107 E	1.63
933941	AD1-017 C	0.84
933942	AD1-017 E	1.37
933991	AD1-023 C	4.11
933992	AD1-023 E	2.24
934201	AD1-047 C	2.75
934202	AD1-047 E	1.83
934231	AD1-050 C	2.02
934232	AD1-050 E	1.1
934311	AD1-055 C	1.07
934312	AD1-055 E	0.28
934331	AD1-057 C OI	4.11
934332	AD1-057 E OI	2.19
934341	AD1-058 C	3.99
934342	AD1-058 E	1.01
934521	AD1-076 C OI	16.75
934522	AD1-076 E OI	8.53
934611	AD1-087 C OI	3.38
934612	AD1-087 E OI	1.59

934621	ADI-088 C	4.01
934622	ADI-088 E	1.88
LTF	ADI-120	7.56
LTF	ADI-121	7.62
934911	ADI-123 C	0.47
934912	ADI-123 E	0.24
934991	ADI-131 C	1.31
934992	ADI-131 E	0.87
935171	ADI-152 C OI	3.36
935172	ADI-152 E OI	2.24
935221	ADI-157 C	0.46
935222	ADI-157 E	0.31
935231	ADI-160 C	0.34
935232	ADI-160 E	0.47
936161	AD2-022 C OI	10.78
936162	AD2-022 E OI	6.47
936171	AD2-023 C OI	6.2
936172	AD2-023 E OI	3.37
936261	AD2-033 C	4.76
936262	AD2-033 E	3.17
936331	AD2-043 C	2.
936332	AD2-043 E	2.37
936361	AD2-046 C OI	3.84
936362	AD2-046 E OI	1.76
936401	AD2-051 C OI	2.97
936402	AD2-051 E OI	1.27

936481	AD2-063 C OI	5.55
936482	AD2-063 E OI	3.7
936531	AD2-068 C	2.28
936532	AD2-068 E	1.17
936641	AD2-081 C	2.56
936642	AD2-081 E	1.15
936651	AD2-082 C	0.52
936652	AD2-082 E	0.25
936701	AD2-089 C	3.17
936702	AD2-089 E	2.12
936711	AD2-090 C OI	2.13
936712	AD2-090 E OI	1.42
LTF	AD2-099	4.99
937441	AD2-195 C	3.15
937442	AD2-195 E	1.36
937461	AD2-200 C	0.51
937462	AD2-200 E	0.24
937481	AD2-202 C OI	0.93
937482	AD2-202 E OI	0.47
LTF	AMIL	0.17
LTF	BLUEG	2.05
LTF	CANNELTON	0.27
LTF	CARR	0.07
LTF	CBM-S1	1.16
LTF	CBM-S2	16.95
LTF	CBM-W2	3.27

<i>LTF</i>	<i>CLIFTY</i>	<i>10.69</i>
<i>LTF</i>	<i>CPL</i>	<i>5.58</i>
<i>LTF</i>	<i>DEARBORN</i>	<i>0.97</i>
<i>LTF</i>	<i>EDWARDS</i>	<i>0.44</i>
<i>LTF</i>	<i>ELMERSMITH</i>	<i>0.7</i>
<i>LTF</i>	<i>FARMERCITY</i>	<i>0.12</i>
<i>LTF</i>	<i>G-007A</i>	<i>0.82</i>
<i>LTF</i>	<i>GIBSON</i>	<i>0.58</i>
<i>LTF</i>	<i>NEWTON</i>	<i>0.95</i>
<i>LTF</i>	<i>PRAIRIE</i>	<i>0.83</i>
<i>LTF</i>	<i>RENSSELAER</i>	<i>0.05</i>
<i>LTF</i>	<i>ROSETON</i>	<i>0.36</i>
<i>LTF</i>	<i>TATANKA</i>	<i>0.33</i>
<i>LTF</i>	<i>TILTON</i>	<i>0.6</i>
<i>LTF</i>	<i>TRIMBLE</i>	<i>0.4</i>
<i>900672</i>	<i>V4-068 E</i>	<i>0.1</i>
<i>LTF</i>	<i>VFT</i>	<i>2.17</i>
<i>917332</i>	<i>Z2-043 E</i>	<i>0.36</i>
<i>917342</i>	<i>Z2-044 E</i>	<i>0.26</i>
<i>917512</i>	<i>Z2-088 E OP1</i>	<i>1.67</i>
<i>918492</i>	<i>AA1-063AE OP</i>	<i>1.37</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>1.46</i>
<i>918532</i>	<i>AA1-067 E</i>	<i>0.29</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.06</i>
<i>919692</i>	<i>AA2-053 E</i>	<i>1.33</i>
<i>919702</i>	<i>AA2-057 E</i>	<i>1.51</i>

<i>LTF</i>	<i>AA2-074</i>	<i>3.79</i>
<i>920042</i>	<i>AA2-088 E</i>	<i>3.28</i>
<i>920592</i>	<i>AA2-165 E</i>	<i>0.2</i>
<i>920672</i>	<i>AA2-174 E</i>	<i>0.15</i>
<i>930401</i>	<i>AB1-081 C</i>	<i>4.1</i>
<i>930402</i>	<i>AB1-081 E</i>	<i>1.76</i>
<i>930861</i>	<i>AB1-132 C</i>	<i>4.94</i>
<i>930862</i>	<i>AB1-132 E</i>	<i>2.12</i>
<i>931231</i>	<i>AB1-173 C</i>	<i>0.77</i>
<i>931232</i>	<i>AB1-173 E</i>	<i>0.36</i>
<i>931241</i>	<i>AB1-173AC</i>	<i>0.77</i>
<i>931242</i>	<i>AB1-173AE</i>	<i>0.36</i>
<i>923911</i>	<i>AB2-031 C O1</i>	<i>0.77</i>
<i>923912</i>	<i>AB2-031 E O1</i>	<i>0.38</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.15</i>
<i>923942</i>	<i>AB2-035 E</i>	<i>0.06</i>
<i>923991</i>	<i>AB2-040 C O1</i>	<i>2.52</i>
<i>923992</i>	<i>AB2-040 E O1</i>	<i>2.06</i>
<i>924021</i>	<i>AB2-043 C O1</i>	<i>1.22</i>
<i>924022</i>	<i>AB2-043 E O1</i>	<i>2.</i>
<i>924151</i>	<i>AB2-059 C O1</i>	<i>4.83</i>
<i>924152</i>	<i>AB2-059 E O1</i>	<i>2.49</i>
<i>924161</i>	<i>AB2-060 C O1</i>	<i>3.48</i>
<i>924162</i>	<i>AB2-060 E O1</i>	<i>1.64</i>
<i>924301</i>	<i>AB2-077 C O1</i>	<i>0.78</i>
<i>924302</i>	<i>AB2-077 E O1</i>	<i>0.52</i>

924311	AB2-078 C OI	0.78
924312	AB2-078 E OI	0.52
924321	AB2-079 C OI	0.78
924322	AB2-079 E OI	0.52
924391	AB2-088 C	0.19
924392	AB2-088 E	0.09
924401	AB2-089 C	0.91
924402	AB2-089 E	0.47
924411	AB2-090 C	1.53
924412	AB2-090 E	0.79
924491	AB2-098 C	0.23
924492	AB2-098 E	0.1
924501	AB2-099 C	0.2
924502	AB2-099 E	0.08
924511	AB2-100 C	3.51
924512	AB2-100 E	1.73
925121	AB2-169 C	2.27
925122	AB2-169 E	2.03
925171	AB2-174 C OI	2.38
925172	AB2-174 E OI	2.16
925221	AB2-176 C	0.63
925222	AB2-176 E	0.27
925591	ACI-034 C	3.13
925592	ACI-034 E	2.36
925611	ACI-036 C	0.33
925612	ACI-036 E	0.54

925781	ACI-054 C	3.04
925782	ACI-054 E	1.4
925991	ACI-075 C	1.96
925992	ACI-075 E	1.11
926021	ACI-080 C	0.66
926022	ACI-080 E	0.37
926051	ACI-083 C	4.18
926052	ACI-083 E	6.83
926071	ACI-086 C	7.28
926072	ACI-086 E	3.31
926201	ACI-098 C	2.4
926202	ACI-098 E	1.43
926211	ACI-099 C	0.81
926212	ACI-099 E	0.47
926271	ACI-105 C	2.39
926272	ACI-105 E	1.19
926771	ACI-163 C	0.65
926772	ACI-163 E	0.3
927021	ACI-189 C	3.63
927022	ACI-189 E	1.81
927141	ACI-208 C	3.55
927142	ACI-208 E	1.58
927251	ACI-221 C	1.59
927252	ACI-221 E	1.59
927261	ACI-222 C	1.54
927262	ACI-222 E	1.47