



**Generation Interconnection  
Feasibility Study Report  
for  
Queue Project AF2-165  
CLARK SUMMIT-EMLENTON 34.5 KV  
12 MW Capacity / 20 MW Energy**

July 2020

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## 1 Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Mid-Atlantic Interstate Transmission (MAIT, PENELEC zone).

## 2 Preface

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. Cost allocation rules for network upgrades can be found in PJM Manual 14A, Attachment B. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Interconnection Customer seeking to interconnect a wind or solar generation facility shall maintain meteorological data facilities as well as provide that meteorological data which is required per Schedule H to the Interconnection Service Agreement and Section 8 of Manual 14D.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

### 3 General

The Interconnection Customer (IC), has proposed a Solar generating facility located in Venango County, Pennsylvania. The installed facilities will have a total capability of 20 MW with 12 MW of this output being recognized by PJM as Capacity. The proposed in-service date for this project is March 15, 2022. This study does not imply a TO commitment to this in-service date.

<b>Queue Number</b>	<b>AF2-165</b>
<b>Project Name</b>	CLARK SUMMIT-EMLENTON 34.5 KV
<b>State</b>	Pennsylvania
<b>County</b>	Venango
<b>Transmission Owner</b>	MAIT (PENELEC zone)
<b>MFO</b>	20
<b>MWE</b>	20
<b>MWC</b>	12
<b>Fuel</b>	Solar
<b>Basecase Study Year</b>	2023

Any new service customers who can feasibly be commercially operable prior to June 1st of the basecase study year are required to request interim deliverability analysis.

#### 4 Point of Interconnection

AF2-165 will interconnect with the PENELEC distribution system via a tap on the Clark Summit Substation 34.5 kV Emlenton circuit #00456-51 at pole # OE-8451 (Attachment 1). The IC's proposed generating unit site is located at GPC: 41.336990, -79.729311

Attachment 1 shows a one-line diagram of the proposed primary direct connection facilities for the AF2-165 generation project to connect to the Penelec distribution system. IC will be responsible for constructing all the facilities on its side of the POI, including the attachment facilities which connect the generator to the Penelec distribution system's direct connection facilities.

#### 5 Cost Summary

The AF2-165 project will be responsible for the following costs:

Description	Total Cost
<b>Total Physical Interconnection Costs</b>	\$113,400
<b>Total System Network Upgrade Costs</b>	\$0
<b>Total Costs</b>	<b>\$113,400</b>

This cost excludes a Federal Income Tax Gross Up charges. This tax may or may not be charged based on whether this project meets the eligibility requirements of IRS Notice 88-129. If at a future date it is determined that the Federal Income Tax Gross charge is required, the Transmission Owner shall be reimbursed by the Interconnection Customer for such taxes.

Cost allocations for any System Upgrades will be provided in the System Impact Study Report.

## 6 Transmission Owner Scope of Work

AF2-165 will interconnect with the PENELEC distribution system via a tap on the Clark Summit Substation 34.5 kV Emlenton circuit #00456-51 at pole # OE-8451 (Attachment 1). The IC's proposed generating unit site is located at GPC: 41.336990, -79.729311.

Attachment 1 shows a one-line diagram of the proposed primary direct connection facilities for the AF2-165 generation project to connect to the Penelec distribution system. IC will be responsible for constructing all the facilities on its side of the POI, including the attachment facilities which connect the generator to the Penelec distribution system's direct connection facilities.

The total physical interconnection costs is given in the table below:

Description	Total Cost
Tap the existing Clark Summit 34.5kV Emlenton line at an existing pole or interspersed pole on Penelec's existing distribution circuit #00456-51 near pole OE-8451, new SCADA recloser tap to interconnect queue project AF2-165. Install 34.5 kV metering in customer's facilities. The customer will have to provide Penelec with permanent access/roadway to this off-road location/equipment. The customer is responsible to build their own line from their site to Penelec's existing facilities.	\$100,000
Clark Summit 34.5kV SS. Adjust Remote Relay and Metering Settings.	\$13,400
<b>Total Physical Interconnection Costs</b>	<b>\$113,400</b>

## 7 Schedule

Based on the scope of work for the Direct and Non-Direct Connection facilities, it is expected to take a minimum of **6 months** after the signing of an Interconnection Construction Service Agreement to complete the installation. This includes the requirement for the IC to make a preliminary payment that compensates FE for the first three months of the engineering design work that is related to the construction of the interconnection substation. This assumes that there will be no environmental issues with any of the new properties associated with this project, that there will be no delays in acquiring the necessary permits for implementing the defined direct connection and that any distribution system outages will be allowed when requested.

## 8 Transmission Owner Analysis

Penelec performed an analysis of its distribution system. The AF2-165 project did not contribute to any overloads on the distribution system.

## 9 Interconnection Customer Requirements

### 9.1 System Protection

An analysis was conducted to assess the impact of the Clark Summit-Emlenton 34.5 kV (AF2-165) Project on the system protection requirements in the area. The results of this review show that the following relay additions will be required:

Proposed single line diagrams show the Interconnection Customer constructing a generation facility tapping Penelec's Clark Summit Substation 34.5 kV Emlenton circuit #00456-51 at pole OE-8451.

The 34.5kV interconnection proposal will require Developer to meet applicable "Technical Requirements" as outlined in First Energy's document titled "Technical Requirements for the Interconnection of Customer-Owned Generation to the FirstEnergy Distribution System". Anti-islanding system shall meet IEEE 1547 and UL 1741 Therefore no Direct Transfer Trip (DTT) will be required.

### 9.2 General Concerns

It is to be understood, for abnormal operation of the Penelec system, which could cause Developer's generation facility to be electrically isolated from the Penelec system synchronous source via the tripping of a interconnecting primary voltage line or device, Developer will, via Penelec's direction, be required to disconnect the generation from Penelec's system and remain disconnected (**units are required to be OFF LINE**), until the Penelec system normal circuitry is restored. These abnormal conditions will be reviewed by Penelec system operators as to the need for the generation facility to be disconnected.

### 9.3 Requirements for Owner's/Developer's generation IPP Facility

The proposed interconnection Owner's/Developer's facilities must be designed in accordance with the document titled *FirstEnergy Distribution Engineering Practices Interconnection of Customer-Owned Generation to the FirstEnergy Distribution System* dated 11/17/14 located at the following link:

<http://www.pjm.com/planning/design-engineering/to-tech-standards/private-firstenergy.aspx>

The document is referred to as engineering practice EP (# 02-280) with section 4, part C specifically referencing the "interconnection technical requirements". Certain protection requirements are shown.

Additionally, Owner/Developer is responsible to provide adequate protection (for their equipment) under any distribution system operating condition' - which includes 'Separation from supply' (i.e. tripping of F.E. circuit breakers) and 'resynchronizing the generation after electric restoration of the supply' (i.e. reclosing of F.E. circuit breakers).

Owner's/Developer's protection must be designed to coordinate with the reclosing practices of FirstEnergy line protective devices. The generator must cease to energize the FirstEnergy circuit to which it is connected prior to reclosing of any (FE) automatic reclosing devices.

Owners/Developer's electrical protection and control schematics shall be provided to FE for consideration. FE may request modifications, if required, to meet the technical requirements.

### 9.4 Compliance Issues

The Interconnection Customer will be responsible for meeting a power factor between 0.90 lagging (producing MVARs) to 0.95 leading (absorbing MVARs) and assure that voltage deviation will be less than 1.0 volt as measured at the POI under all Solar Gen operating conditions due to the inherent dynamic reactive power capability of this solar facility.

Generators with no inherent VAR (reactive power) control capability, or those that have a restricted VAR capability less than the defined requirements, must provide dynamic supplementary reactive support located at the generation facility with electrical characteristics equivalent to that provided by a similar sized synchronous generator. A Dynamic Reactive Compensation (either Static VAR Compensator (SVC) or STATCOM) or other method be applied in order to maintain the required specifications at the POI. The Interconnection Customer is responsible for the installation of equipment on its side of the POI in order to adhere to the criteria stated above by FirstEnergy.

## 10 Revenue Metering and SCADA Requirements

### 10.1 PJM Requirements

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Section 8 of Attachment O.

### 10.2 Meteorological Data Reporting Requirements

The solar generation facility shall provide the Transmission Provider with site-specific meteorological data including:

- Back Panel temperature (Fahrenheit)
- Irradiance (Watts/meter<sup>2</sup>)
- Ambient air temperature (Fahrenheit) – (Accepted, not required)
- Wind speed (meters/second) – (Accepted, not required)
- Wind direction (decimal degrees from true north) – (Accepted, not required)

### 10.3 PENELEC Requirements

The Interconnection Customer will be required to comply with all FE Revenue Metering Requirements for Generation Interconnection Customers. These FE requirements are the following:

The FE operating company (Penelec) shall provide, own, operate, test, and maintain the revenue metering equipment at the Interconnection Customer's (IC) expense. The revenue metering equipment includes, but is not limited to, current transformers, voltage transformers, secondary wires, meter socket, bidirectional revenue meter, and associated devices. The IC shall mount the instrument transformers unless otherwise agreed to by Penelec. The instrument transformers and meter socket shall be installed in a location that is readily accessible to authorized Penelec representatives. Penelec will provide the IC access to bidirectional kWh and kVARh pulses from the Penelec meter at the IC's expense if requested. The IC shall, at its expense, install, own, operate, test, and maintain any metering and telemetry equipment that may be required to provide real-time meter data to FE or PJM.

## 11 Summer Peak - Load Flow Analysis

The Queue Project AF2-165 was evaluated as a 20.0 MW (Capacity 12.0 MW) injection at the Clark Summit 34.5 kV substation in the PENELEC area. Project AF2-165 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AF2-165 was studied with a commercial probability of 53.0 %. Potential network impacts were as follows:

### 11.1 Generation Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None.

### 11.2 Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None.

### 11.3 Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADIN G %	POST PROJECT LOADIN G %	AC D C	MW IMPACT
10109858	957160	AF2-010 TAP	115.0	PENELEC	200571	26UNIONCY	115.0	PENELEC	1	PN-P1-2-PN-345-001	single	120.0	110.12	111.75	DC	1.95

### 11.4 Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADIN G %	POST PROJECT LOADIN G %	AC D C	MW IMPACT
111853628	200575	26MRGANST	115.0	PENELEC	200573	26VENGOJT	115.0	PENELEC	1	PN-P1-2-PN-345-001	operation	149.0	110.55	111.01	DC	1.5
101098931	200576	26UTICA JT	115.0	PENELEC	200598	26WAYNE	115.0	PENELEC	1	PN-P1-2-PN-345-003	operation	277.0	100.91	103.55	DC	7.31
101098836	200584	26GRANDVW	115.0	PENELEC	946400	AF1-304 TAP	115.0	PENELEC	1	PN-P1-2-PN-345-001	operation	149.0	139.26	139.28	DC	3.25

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CON T NAME	Type	Ratin g MVA	PRE PROJEC T LOADIN G %	POST PROJEC T LOADIN G %	AC D C	MW IMPAC T
101098875	200585	26TITUSVIL	115.0	PENELE C	957160	AF2-010 TAP	115.0	PENELE C	1	PN-P1-2-PN-345-001	operati on	120.0	105.1	107.81	DC	3.25
101098904	200586	26ECLIPSE	115.0	PENELE C	200576	26UTICA JT	115.0	PENELE C	1	PN-P1-2-PN-345-003	operati on	277.0	103.98	106.62	DC	7.31
100586966	235139	01AL&D6T	138.0	AP	235138	01AL 4J	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	151.0	138.01	138.47	DC	1.56
100586967	235139	01AL&D6T	138.0	AP	235138	01AL 4J	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	151.0	138.01	138.47	DC	1.56
100586846	235197	01KARNSC	138.0	AP	235152	01BUTLER	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	179.0	234.95	236.43	DC	2.66
100586847	235197	01KARNSC	138.0	AP	235152	01BUTLER	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	179.0	234.95	236.43	DC	2.66
100586883	235203	01KISSNG	138.0	AP	235197	01KARNSC	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	268.0	181.15	182.19	DC	2.81
100586884	235203	01KISSNG	138.0	AP	235197	01KARNSC	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	268.0	181.15	182.19	DC	2.81
100586972	235204	01KITTAN	138.0	AP	235139	01AL&D6T	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	151.0	133.92	134.38	DC	1.56
100586973	235204	01KITTAN	138.0	AP	235139	01AL&D6T	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	151.0	133.92	134.38	DC	1.56
100586890	235240	01COLMBG PN	138.0	AP	235202	01KISKIV	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	151.0	188.36	188.91	DC	1.85
100586891	235240	01COLMBG PN	138.0	AP	235202	01KISKIV	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	151.0	188.36	188.91	DC	1.85
100586875	235282	01GAR RN	138.0	AP	235240	01COLMBG PN	138.0	AP	1	PN-P1-2-PN-345-107T	operati on	151.0	196.84	197.39	DC	1.85

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CON T NAME	Type	Ratin g MVA	PRE PROJEC T LOADIN G %	POST PROJEC T LOADIN G %	AC D C	MW IMPAC T
100586876	235282	01GAR RN	138.0	AP	235240	01COLMBG PN	138.0	AP	1	ATSI-P1-2-CEI-345-700T	operati on	151.0	196.84	197.39	DC	1.85
101098654	957160	AF2-010 TAP	115.0	PENELE C	200571	26UNION CY	115.0	PENELE C	1	PN-P1-2-PN-345-001	operati on	120.0	149.98	152.69	DC	3.25
101098657	957160	AF2-010 TAP	115.0	PENELE C	200571	26UNION CY	115.0	PENELE C	1	Base Case	operati on	120.0	107.77	110.2	DC	2.92

### 11.5 System Reinforcements - Summer Peak Load Flow - Primary POI

ID	Idx	Facility	Upgrade Description	Cost
101098658	1	AF2-010 TAP 115.0 kV - 26UNION CY 115.0 kV Ckt 1	s1887.1_s1887.2 (1895) : Replace line relaying and line trap on the Titusville 115 kV Line exit at the Union City Substation (s1887.1) Replace line relaying and line trap on the Union City 115 kV line exit at the Titusville substation. (s1887.2) Project Type : FAC Cost : \$0	\$0
			TOTAL COST	\$0

## 11.6 Flow Gate Details

The following indices contain additional information about each facility presented in the body of the report. For each index, a description of the flowgate and its contingency was included for convenience. The intent of the indices is to provide more details on which projects/generators have contributions to the flowgate in question. All New Service Queue Requests, through the end of the Queue under study, that are contributors to a flowgate will be listed in the indices. Please note that there may be contributors that are subsequently queued after the queue under study that are not listed in the indices. Although this information is not used "as is" for cost allocation purposes, it can be used to gage the impact of other projects/generators. It should be noted the project/generator MW contributions presented in the body of the report are Full MW Impact contributions which are also noted in the indices column named "Full MW Impact", whereas the loading percentages reported in the body of the report, take into consideration the PJM Generator Deliverability Test rules such as commercial probability of each project as well as the ramping impact of "Adder" contributions. The MW Impact found and used in the analysis is shown in the indices column named "Gendeliv MW Impact".

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### 11.6.1 Index 1

ID	FROM BUS#	FROM BUS	FROM BUS AREA	TO BUS#	TO BUS	TO BUS AREA	CKT ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADING %	POST PROJECT LOADING %	AC DC	MW IMPACT
101098658	957160	AF2-010 TAP	PENELEC	200571	26UNION CY	PENELEC	1	PN-P1-2-PN-345-001	single	120.0	110.12	111.75	DC	1.95

Bus #	Bus	Gendeliv MW Impact	Type	Full MW Impact
200608	26PINEY #1	0.4476	80/20	0.4476
200662	26SCRUB GR	1.8511	80/20	1.8511
935191	AD1-154	1.1368	80/20	1.1368
938951	AE1-123	1.4477	80/20	1.4477
939291	AE1-160 C	4.5773	80/20	4.5773
944281	AF1-096 C	4.3250	80/20	4.3250
945751	AF1-240 C O1	0.6821	80/20	0.6821
946401	AF1-304 C	17.0772	80/20	17.0772
957161	AF2-010 C	32.2957	80/20	32.2957
957951	AF2-089 C	1.1894	80/20	1.1894
958361	AF2-130 C	1.5420	80/20	1.5420
958741	AF2-165 C	1.9508	80/20	1.9508
958751	AF2-166 C	1.5420	80/20	1.5420
959441	AF2-235 C	2.1625	80/20	2.1625
959521	AF2-243 C	1.4631	80/20	1.4631
NEWTON	NEWTON	0.2439	Confirmed LTF	0.2439
FARMERCITY	FARMERCITY	0.0125	Confirmed LTF	0.0125
G-007A	G-007A	0.6425	Confirmed LTF	0.6425
VFT	VFT	1.7286	Confirmed LTF	1.7286
CALDERWOOD	CALDERWOOD	0.0785	Confirmed LTF	0.0785
PRAIRIE	PRAIRIE	0.5631	Confirmed LTF	0.5631
CHEOAH	CHEOAH	0.0781	Confirmed LTF	0.0781
EDWARDS	EDWARDS	0.0851	Confirmed LTF	0.0851
TILTON	TILTON	0.1499	Confirmed LTF	0.1499
MADISON	MADISON	0.0040	Confirmed LTF	0.0040
GIBSON	GIBSON	0.1245	Confirmed LTF	0.1245
BLUEG	BLUEG	0.3854	Confirmed LTF	0.3854
TRIMBLE	TRIMBLE	0.1241	Confirmed LTF	0.1241
CATAWBA	CATAWBA	0.0385	Confirmed LTF	0.0385

## 11.7 Queue Dependencies

The Queue Projects below are listed in one or more indices for the overloads identified in your report. These projects contribute to the loading of the overloaded facilities identified in your report. The percent overload of a facility and cost allocation you may have towards a particular reinforcement could vary depending on the action of these earlier projects. The status of each project at the time of the analysis is presented in the table. This list may change as earlier projects withdraw or modify their requests.

Queue Number	Project Name	Status
AD1-154	Timblin 34.5 kV	Active
AE1-123	Emlenton 34.5 kV	Engineering and Procurement
AE1-160	Venango 34.5 kV	Engineering and Procurement
AF1-096	Titusville-Oil Creek 34.5 kV	Active
AF1-240	Timblin 34.5 kV	Active
AF1-304	Titusville-Grandview 115 kV	Active
AF2-010	Union City-Titusville 115 kV	Active
AF2-089	Titusville 34.5 kV	Active
AF2-130	Wolfs Corners 34.5 kV	Active
AF2-165	Clark Summit-Emlenton 34.5 kV	Active
AF2-166	Clark Summit-Emlenton 34 kV	Active
AF2-235	Titusville-Oil Creek 34.5 kV	Active
AF2-243	Clark Summit 34.5 kV	Active

## 11.8 Contingency Descriptions

Contingency Name	Contingency Definition
Base Case	
PN-P1-2-PN-345-003	CONTINGENCY 'PN-P1-2-PN-345-003' /* HANDSOME LAKE - WAYNE 345KV DISCONNECT BRANCH FROM BUS 200826 TO BUS 200595 CKT 1 /* 26HANDSMLK 345 26WAYNE 345 END
PN-P1-2-PN-345-001	CONTINGENCY 'PN-P1-2-PN-345-001' /* ERIE WEST - WAYNE 345KV DISCONNECT BRANCH FROM BUS 200599 TO BUS 200595 CKT 1 /* 26ERIE W 345 26WAYNE 345 END
PN-P1-2-PN-345-107T	CONTINGENCY 'PN-P1-2-PN-345-107T' /* ERIE WEST - ASHTABULA - PERRY 345KV DISCONNECT BRANCH FROM BUS 200599 TO BUS 238547 CKT 1 /* 26ERIE W 345 02AT 345 DISCONNECT BRANCH FROM BUS 238547 TO BUS 239082 CKT 1 /* 02AT 345 02S8-ATT 345 DISCONNECT BRANCH FROM BUS 238547 TO BUS 239036 CKT 1 /* 02AT 345 02PERRY 345 DISCONNECT BUS 238547 /* 02AT 345 END
ATSI-P1-2-CEI-345-700T	CONTINGENCY 'ATSI-P1-2-CEI-345-700T' /* PN/ATSI ERIE WEST - ASHTABULA - PERRY 345KV DISCONNECT BRANCH FROM BUS 239036 TO BUS 238547 CKT 1 /* 02PERRY 345 02AT 345 DISCONNECT BRANCH FROM BUS 238547 TO BUS 239082 CKT 1 /* 02AT 345 02S8-ATT 345 DISCONNECT BRANCH FROM BUS 239082 TO BUS 238544 CKT 8 /* 02S8-ATT 345 02ASH_3 138 DISCONNECT BRANCH FROM BUS 238547 TO BUS 200599 CKT 1 /* 02AT 345 26ERIE W 345 END

## 12 Short Circuit Analysis

To be performed in System Impact phase.

## 13 Affected Systems

### 13.1 NYISO

NYISO Impacts to be determined during later study phases (as applicable).

**14 Attachment 1: One Line Diagram**