



# **Generation Interconnection**

## **Feasibility Study Report**

**for**

### **Queue Project AG1-139**

**CLARK SUMMIT-EMLENTON 34.5 KV**

**4.75 MW Capacity / 5 MW Energy**

January 2021

# Table of Contents

- 1 Introduction..... 4
- 2 Preface..... 4
- 3 General..... 5
- 4 Point of Interconnection..... 6
- 5 Cost Summary ..... 6
- 6 Transmission Owner Scope of Work..... 7
- 7 Schedule..... 8
- 8 Transmission Owner Analysis..... 8
- 9 Interconnection Customer Requirements..... 8
  - 9.1 System Protection..... 8
  - 9.2 General Concerns ..... 9
  - 9.3 Requirements for Owner’s/Developer’s generation IPP Facility..... 9
  - 9.4 Compliance Issues ..... 9
- 10 Revenue Metering and SCADA Requirements ..... 10
  - 10.1 PJM Requirements..... 10
  - 10.2 Meteorological Data Reporting Requirements ..... 10
  - 10.3 Interconnected Transmission Owner Requirements..... 10
- 11 Summer Peak - Load Flow Analysis ..... 11
  - 11.1 Generation Deliverability ..... 12
  - 11.2 Multiple Facility Contingency ..... 12
  - 11.3 Contribution to Previously Identified Overloads..... 12
  - 11.4 Potential Congestion due to Local Energy Deliverability..... 12
  - 11.5 System Reinforcements - Summer Peak Load Flow - Primary POI..... 13
  - 11.6 Flow Gate Details..... 14
  - 11.7 Queue Dependencies ..... 15
  - 11.8 Contingency Descriptions..... 16
- 12 Short Circuit Analysis..... 17
  - 12.1 System Reinforcements - Short Circuit..... 17
- 13 Affected Systems ..... 18
  - 13.1 NYISO ..... 18
  - 13.2 MISO ..... 18

14 Attachment 1: One Line Diagram .....19

## 1 Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Mid-Atlantic Interstate Transmission, LLC (MAIT) (PENELEC Zone).

## 2 Preface

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. Cost allocation rules for network upgrades can be found in PJM Manual 14A, Attachment B. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Interconnection Customer seeking to interconnect a wind or solar generation facility shall maintain meteorological data facilities as well as provide that meteorological data which is required per Schedule H to the Interconnection Service Agreement and Section 8 of Manual 14D.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

### 3 General

The Interconnection Customer (IC) has proposed an uprate to a planned/existing Solar generating facility located in Venango, Pennsylvania. This project is an increase to the Interconnection Customer's AF2-165 project, which will share the same point of interconnection. The AG1-139 queue position is a 5 MW uprate (4.75 MW Capacity uprate) to the previous project. The total installed facilities will have a capability of 25 MW with 16.75 MW of this output being recognized by PJM as Capacity. The proposed in-service date for this uprate project is September 15, 2022. This study does not imply a TO commitment to this in-service date.

<b>Queue Number</b>	<b>AG1-139</b>
<b>Project Name</b>	CLARK SUMMIT-EMLENTON 34.5 KV
<b>State</b>	Pennsylvania
<b>County</b>	Venango
<b>Transmission Owner</b>	MAIT (PENELEC)
<b>MFO</b>	25
<b>MWE</b>	5
<b>MWC</b>	4.75
<b>Fuel</b>	Solar
<b>Basecase Study Year</b>	2024

Any new service customers who can feasibly be commercially operable prior to June 1st of the basecase study year are required to request interim deliverability analysis.

## 4 Point of Interconnection

AG1-139 is a 5MW uprate of AF2-165. AF2-165 is located on the 34.5kV Emlenton feeder @ the Clark Summit substation. At the time, AF2-165 was allowed to proceed. New thresholds for the maximum allowed aggregate generation permitted on this classification of feeder have been adopted as of June 23, 2020 after the close of the AF2 queue, but before the start of the AG1 queue. Had these limitations been in place at the time of the AF2 queue, AF2-165 would not have been permitted to proceed as a direct connect to Penelec’s distribution feeder. Consequently, the 5MW uprate to AF2-165 requested under AG1-139 is not permitted to proceed as an uprate addition. The 5MW uprate requested under AG1-139 will need to be sourced from a dedicated developer constructed, owned, and maintained express feeder that will terminate at the 34.5kV bus at the Clark Summit substation.

Attachment 1 shows a one-line diagram of the proposed primary direct connection facilities for the AG1-139 generation project to connect to the Penelec distribution system. IC will be responsible for constructing all of the facilities on its side of the POI, including the attachment facilities which connect the generator to the Penelec distribution system’s direct connection facilities.

## 5 Cost Summary

The AG1-139 project will be responsible for the following costs:

Description	Total Cost
<b>Total Physical Interconnection Costs</b>	\$1,342,100
<b>Total System Network Upgrade Costs</b>	\$0
<b>Total Costs</b>	\$1,342,100

This cost excludes a Federal Income Tax Gross Up charges. This tax may or may not be charged based on whether this project meets the eligibility requirements of IRS Notice 2016-36, 2016-25 I.R.B. (6/20/2016). If at a future date it is determined that the Federal Income Tax Gross charge is required, the Transmission Owner shall be reimbursed by the Interconnection Customer for such taxes.

Cost allocations for any System Upgrades will be provided in the System Impact Study Report.

## 6 Transmission Owner Scope of Work

AG1-139 is a 5MW uprate of AF2-165. AF2-165 is located on the 34.5kV Emlenton feeder @ the Clark Summit substation. At the time, AF2-165 was allowed to proceed. New thresholds for the maximum allowed aggregate generation permitted on this classification of feeder have been adopted as of June 23, 2020 after the close of the AF2 queue, but before the start of the AG1 queue. Had these limitations been in place at the time of the AF2 queue, AF2-165 would not have been permitted to proceed as a direct connect to Penelec's distribution feeder. Consequently, the 5MW uprate to AF2-165 requested under AG1-139 is not permitted to proceed as an uprate addition. The 5MW uprate requested under AG1-139 will need to be sourced from a dedicated developer constructed, owned, and maintained express feeder that will terminate at the 34.5kV bus at the Clark Summit substation.

The total physical interconnection costs is given in the table below:

Description	Total Cost
New 34.5kV substation breaker and bay position at Clark Summit substation	\$1,200,000
Install a SCADA controlled 34.5kV recloser to interconnect queue project AG1-139. Install 34.5kV metering in customer's facilities. The customer is responsible to build their own line from their site to Penelec's existing facilities	\$102,500
NPs & Cust Dwg Review @ AG1-139	\$25,200
Clark Summit 34.5kV SS. Adjust Remote Relay and Metering Settings.	\$14,400
<b>Total Physical Interconnection Costs</b>	<b>\$1,342,100</b>

## 7 Schedule

Based on the scope of work for the interconnection facilities, it is expected to take a minimum of **18 months** after the signing of an Interconnection Agreement and construction kickoff call to complete the installation. This assumes that there will be no environmental issues with any of the new properties associated with this project, that there will be no delays in acquiring the necessary permits for implementing the defined work and that all system outages will be allowed when requested.

The schedule for the required Network Impact Reinforcements will be more clearly identified in future study phases.

## 8 Transmission Owner Analysis

Due to recently adopted thresholds for total aggregate generation that went into effect after the AF2 queue was completed but before the AG1 queue started, the 5MW uprate requested under AG1-139 to the 20MW solar system that was accepted under AF2-165 is denied. Developer will be responsible for the costs associated with a new, dedicated 34.5kV substation breaker and bay at Penelec's Clark Summit substation that will source the developer's express feeder to AG1-139. No other Penelec facilities were impacted by the addition of AG1-139 as described above.

These thresholds were adopted as of June 23, 2020 after the close of the AF2 queue, but before the start of the AG1 queue, and are now being enforced to limit exposure to the inherent voltage fluctuations the could impact the distribution customers directly sourced from the generation hosting circuit. Having large quantities of generation tied to a given feeder limits the ability of system operators to quickly respond to the switching for planned or emergent events. Having IPP's sourced from a dedicated feeder will offer some level of isolation due to voltage fluctuations stemming from the generator, will provide heightened visibility for the system operators to identify the presence of an IPP and streamline their efforts to isolate the same IPP by opening the substation breaker sourcing the express feeder. Protection coordination between the transmission operator and the IPP will be easier to implement at the substation level.

## 9 Interconnection Customer Requirements

### 9.1 System Protection

Proposed single line diagrams show the developer constructing a generation facility (Clark Summit – Emlenton 34.5kV AG1-139) tapping Penelec's 34.5kV bus @ Clark Summit substation via a dedicated developer constructed, owned, and maintained express feeder that will terminate to a new substation breaker to be installed at the Clark Summit substation.

The 34.5kV interconnection proposal will require Developer to meet applicable "Technical Requirements" as outlined in First Energy's document titled "Technical Requirements for the Interconnection of Customer-

Owned Generation to the FirstEnergy Distribution System". Anti-islanding system shall meet IEEE 1547 and UL 1741 Therefore no Direct Transfer Trip (DTT) will be required.

## 9.2 General Concerns

It is to be understood, for abnormal operation of the Penelec system, which could cause Developer's generation facility to be electrically isolated from the Penelec system synchronous source via the tripping of a interconnecting primary voltage line or device, Developer will, via Penelec's direction, be required to disconnect the generation from Penelec's system and remain disconnected (**units are required to be OFF LINE**), until the Penelec system normal circuitry is restored. These abnormal conditions will be reviewed by Penelec system operators as to the need for the generation facility to be disconnected.

## 9.3 Requirements for Owner's/Developer's generation IPP Facility

The proposed interconnection Owner's/Developer's facilities must be designed in accordance with the document titled FirstEnergy Distribution Engineering Practices Interconnection of Customer-Owned Generation to the FirstEnergy Distribution System dated 11/17/14 located at the following link:

<http://www.pjm.com/planning/design-engineering/to-tech-standards/private-firstenergy.aspx>

The document is referred to as engineering practice EP (# 02-280) with section 4, part C specifically referencing the "interconnection technical requirements". Certain protection requirements are shown.

Additionally, Owner/Developer is responsible to provide adequate protection (for their equipment) under any distribution system operating condition' - which includes 'Separation from supply' (i.e. tripping of F.E. circuit breakers) and 'resynchronizing the generation after electric restoration of the supply' (i.e. reclosing of F.E. circuit breakers).

Owner's/Developer's protection must be designed to coordinate with the reclosing practices of FirstEnergy line protective devices. The generator must cease to energize the FirstEnergy circuit to which it is connected prior to reclosing of any (FE) automatic reclosing devices.

Owners/Developer's electrical protection and control schematics shall be provided to FE for consideration. FE may request modifications, if required, to meet the technical requirements.

## 9.4 Compliance Issues

The Developer will be responsible for meeting a power factor between 0.95 lagging (producing MVARs) to 0.95 leading (absorbing MVARs) and assure that voltage deviation will be less than 1.0 volt as measured at the POI under all Solar Gen operating conditions due to the inherent dynamic reactive power capability of this solar facility.

Generators with no inherent VAR (reactive power) control capability, or those that have a restricted VAR capability less than the defined requirements, must provide dynamic supplementary reactive support located at the generation facility with electrical characteristics equivalent to that provided by a similar sized

synchronous generator. A Dynamic Reactive Compensation (either Static VAR Compensator (SVC) or STATCOM) or other method be applied in order to maintain the required specifications at the POI. The Developer is responsible for the installation of equipment on its side of the POI in order to adhere to the criteria stated above by FirstEnergy.

## **10 Revenue Metering and SCADA Requirements**

### **10.1 PJM Requirements**

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Section 8 of Attachment O.

### **10.2 Meteorological Data Reporting Requirements**

The solar generation facility shall provide the Transmission Provider with site-specific meteorological data including:

- Back Panel temperature (Fahrenheit) - (Required for plants with Maximum Facility Output of 3 MW or higher)
- Irradiance (Watts/meter<sup>2</sup>) - (Required for plants with Maximum Facility Output of 3 MW or higher)
- Ambient air temperature (Fahrenheit) - (Accepted, not required)
- Wind speed (meters/second) - (Accepted, not required)
- Wind direction (decimal degrees from true north) - (Accepted, not required)

### **10.3 Interconnected Transmission Owner Requirements**

The IC will be required to comply with all Interconnected Transmission Owner's revenue metering requirements for generation interconnection customers located at the following link:

<http://www.pjm.com/planning/design-engineering/to-tech-standards/>

## 11 Summer Peak - Load Flow Analysis

The Queue Project AG1-139 was evaluated as a 5 MW (Capacity 4.75 MW) injection as an uprate to AF2-165 which is a direct connection at the Clark Summit 34.5 kV substation in the PENELEC area. Project AG1-139 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AG1-139 was studied with a commercial probability of 53.0 %. Potential network impacts were as follows:

### **11.1 Generation Deliverability**

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

### **11.2 Multiple Facility Contingency**

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

### **11.3 Contribution to Previously Identified Overloads**

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

None

### **11.4 Potential Congestion due to Local Energy Deliverability**

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

None

## 11.5 System Reinforcements - Summer Peak Load Flow - Primary POI

None

## 11.6 Flow Gate Details

The following indices contain additional information about each facility presented in the body of the report. For each index, a description of the flowgate and its contingency was included for convenience. The intent of the indices is to provide more details on which projects/generators have contributions to the flowgate in question. All New Service Queue Requests, through the end of the Queue under study, that are contributors to a flowgate will be listed in the indices. Please note that there may be contributors that are subsequently queued after the queue under study that are not listed in the indices. Although this information is not used "as is" for cost allocation purposes, it can be used to gage the impact of other projects/generators. It should be noted the project/generator MW contributions presented in the body of the report are Full MW Impact contributions which are also noted in the indices column named "Full MW Impact", whereas the loading percentages reported in the body of the report, take into consideration the PJM Generator Deliverability Test rules such as commercial probability of each project as well as the ramping impact of "Adder" contributions. The MW Impact found and used in the analysis is shown in the indices column named "Gendeliv MW Impact".

None

## 11.7 Queue Dependencies

The Queue Projects below are listed in one or more indices for the overloads identified in your report. These projects contribute to the loading of the overloaded facilities identified in your report. The percent overload of a facility and cost allocation you may have towards a particular reinforcement could vary depending on the action of these earlier projects. The status of each project at the time of the analysis is presented in the table. This list may change as earlier projects withdraw or modify their requests.

None

## 11.8 Contingency Descriptions

None

## 12 Short Circuit Analysis

The following Breakers are overdutied:

None

Bus Number	Bus Name	BREAKER	Type	Capacity (Amps)	Duty Percentage Post Queue	Duty Percentage Pre Queue

### 12.1 System Reinforcements - Short Circuit

## **13 Affected Systems**

### **13.1 NYISO**

NYISO Impacts to be determined during later study phases (as applicable).

### **13.2 MISO**

MISO Impacts to be determined during later study phases (as applicable).

**14 Attachment 1: One Line Diagram**