# Transmission Interconnection Facilities Study Report

# For

# PJM Transmission Interconnection Request Queue Position AE2-285

"Maysville 69 kV"

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#### **Preface**

The intent of the Facility Study is to determine a plan, with approximate cost and construction time estimates, to connect the subject generation interconnection project to the PJM network at a location specified by the Interconnection Customer. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system. All facilities required for interconnection of a generation interconnection project must be designed to meet the technical specifications (on PJM web site) for the appropriate transmission owner.

In some instances, an Interconnection Customer may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection or merchant transmission upgrade, may also contribute to the need for the same network reinforcement.

The Facility Study estimates attempt to identify the estimated time required to obtain property rights and permits for construction of the required facilities. The project IC is responsible for the right-of-way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

#### A. Transmission Owner Facilities Study Summary

#### 1. Description of Project

MC Solar I, LLC, (hereinafter referred to as "IC") has proposed a solar generating facility located in Mercer County, Pennsylvania. The installed facilities for AE2-285 will have a total capability of 50 MW with 30 MW of this output being recognized by PJM as capacity. The generation facility will interconnect with American Transmission Systems Inc. (ATSI), a First Energy Company (FE), hereinafter referred to as "Transmission Owner" (TO), at the existing Maysville Substation by extending the Maysville 69 kV bus and installing one 69 kV circuit breaker. The POI is located on an ATSI-owned deadend structure inside the ATSI-owned substation.

#### 2. Amendments to the System Impact Study or System Impact Study Results

No amendments to the System Impact Study or System Impact Study Results were identified.

#### 3. Interconnection Customer's Milestone Schedule

The Commercial Operation Date (COD) for the generation facility is **January 2, 2023**. A Project Kickoff meeting must occur by October 31, 2021 to meet Transmission Owner's Assumed Milestone Schedule listed below.

#### **Milestone Schedule:**

11/01/2022 Initial Back-feed through Project Substation Date

01/02/2023 Project Commercial Operation Date

#### 4. Customer's Scope of Work

IC is responsible for all design and construction related to activities on their side of the Point of Interconnection (POI). This includes, but is not limited to the generation step-up (GSU) transformer, 69 kV (AE2-285) generator lead line and connection to the new 69 kV breaker and expanded bus.

**Point of Interconnection** (POI): The POI will be located within the new 69 kV bus expansion interconnection where IC-owned 69 kV attachment line conductor will terminate on the insulators on the dead-end takeoff structure.

IC is required to own, install, and maintain a fully-rated, fault-interrupting circuit breaker on the high-side of the GSU transformer, as well as the necessary revenue metering equipment. The revenue metering current and voltage transformers shall be installed on the high voltage side of the GSU, on the generation side of the fault-interrupting device, and within the local zone of fault protection for the facility. The protective relaying and metering design must comply with First Energy's applicable standards as well as with PJM requirements.

#### **Assumptions / Notes:**

- The interconnecting 69-34.5kV transformer shall have a delta or ungrounded wye winding on the transmission (69kV) side of the transformer.
- IC will coordinate design and alignment of proposed 69 kV generator lead line with the Transmission Owner for review of any clearance, right-of-way or right-of-way encroachment issues with TO owned facilities.
- IC will coordinate design and construction of proposed 69 kV Lead Line. For these areas, the IC shall provide TO with proposed plan and profile or PLS-CADD drawings prior to construction and as-built drawings, confirmed by as-built survey data post-construction.
- Transmission Owner's preference would be to limit interference and avoid transmission line crossings with new 69 kV terminal positions. As a minimum, IC facilities should not encroach within 100 feet of TO centerline at blowout conditions. If IC's line design does not comply with this requirement TO would need to review this area as a special exception.
- Additional costs will be incurred by the IC, if final alignment of the 69 kV generator lead line causes encroachments, changes, or modifications to any existing or relocated TO facilities.
- PJM and Transmission Owner's Requirements may be found in the *Requirements for Transmission Connected Facilities* document located at the following links:

- o www.firstenergycorp.com/feconnect
- o www.pjm.com/planning/design-engineering/to-tech-standards.aspx

#### 5. Description of Facilities Included in the Facilities Study

#### **Attachment Facilities**

- AE2-285 Generator Lead Termination
  - Transmission Owner will design, furnish and construct the new 69 kV line terminal and take off structure. This work will include, but not be limited to, installation of a 69 kV line exit take-off structure, foundations, disconnect switch and associated equipment to accommodate the termination of the 69 kV generator lead line.

#### **Direct Connection**

None

#### **Non-Direct Connection**

- Maysville Substation
  - To connect the AE2-285 solar project with the ATSI transmission system, Maysville 69 kV bus at Maysville substation will be expanded, and a 69 kV circuit breaker added.
  - Estimated SCADA work at Maysville substation to support breaker and relay installations.
     Estimated in-sub fiber run from Maysville control house to developer ran fiber build for communications and control to AE2-285 Generation Interconnection.
- Project Management
  - Review of scope regarding Project Management, Commissioning, Environmental, Forestry, Real Estate, and Right of Way.
- Sharon Substation
  - o Relay settings will be modified.
- Dilworth Substation
  - Relay settings will be modified.
- McDowell Substation
  - o Relay settings will be modified.
- Masury Substation
  - o Relay settings will be modified.

#### **Other Work**

- AE2-285 Metering:
  - o Customer-owned revenue metering at generation facility.

#### 6. Total Cost of Transmission Owner Facilities Included in the Facilities Study

Description	Total
Attachment Facilities:	\$ 91,700
<b>Total Direct Connection (DC) Costs:</b>	\$ 0
Total Non-Direct Connection (NDC) Upgrade Costs:	\$ 1,500,200
Total Other Charges:	\$2,500
New System Upgrades	<b>\$ 0</b>

TOTAL Costs (ALL Categories) \$ 1,594,400
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#### 7. Summary of the Schedule for Completion of Work for the Facilities Study

Attachment Facility	Timeframe
Engineering, Procurement, and Construction	12 months

#### **B. Transmission Owner Facilities Study Results**

This section describes facilities identified to be installed (attachment facilities), replaced, and/or upgraded (upgrade facilities) by First Energy to accommodate the project. During detailed design and analysis other components may be identified for installation or replacement due to this interconnection.

#### 1. Transmission Lines -New

None

#### 2. Transmission Lines - Upgrade

None

#### 3. New Substation/Switchyard Facilities

None

#### 4. Substation/Switchyard Facility Upgrades

#### Maysville

- Below Grade
  - o Install Foundations, Conduit, and Grounding for New Equipment.

- o Conduit to Control Building for Fiber Termination.
- Above Grade

- o Install (1) 69 kV Box Structure Bay.
- o Install (1) 69 kV Circuit Breaker.
- o Install (6) 69 kV Hook-Stick Breaker Disconnect Switch
- o Install (1) 69 kV GOAB Transfer Switch.
- o Install (3) 69 kV PTs.
- o Install (3) 69 kV Surge Arresters.
- Install (1) Lot of Rigid Bus, Cable Risers, Connectors, and Insulators as Shown on the Proposed Layout
- R&C
  - Install (1) Standard Transmission Line Relaying Panel Consisting of Dual SEL-411L with SEL-501 BFT.
  - o Misc. Relay Changes to Add Breaker into Bus Relaying.
  - o Install (1) Fiber Termination Rack.
- Additional Equipment to be Removed
  - o None
- Assumptions
  - o AC and DC Services and SCADA RTU have Adequate Flexibility for New Equipment.
  - o Control House has Adequate Space for New Relaying.

#### **Sharon**

- Below Grade
  - o None
- Above Grade
  - o None
- R&C
  - o Relay setting changes needed.
- Assumptions
  - o None

#### Dilworth

- Below Grade
  - o None
- Above Grade
  - None
- R&C
  - o Relay setting changes needed.
- Assumptions
  - o None

#### McDowell

- Below Grade
  - o None
- Above Grade
  - o None
- R&C
  - o Relay setting changes needed.
- Assumptions
  - o None

#### Masury

- Below Grade
  - o None
- Above Grade
  - o None
- R&C
  - o Relay setting changes needed.
- Assumptions
  - o None

#### 5. Telecommunications Facilities - Upgrades

IC will design, provide, install, own and maintain a fiber-optic communications cable between the Maysville substation, and IC's **generation** (collector) substation. Two (2) fiber-optic channels are required for each generator protection scheme to obtain high-speed tripping capability for any fault within the zone of protection. Should subsequent/additional PJM studies indicate that stability issues exist, the primary and backup relay fiber-optic communication channels must be in separately-routed cable paths and additional fiber-optic connection costs would apply (not included herein).

Transmission Owner will make the fiber termination connections for its cable(s) at the interconnection substation control house. IC is responsible for obtaining and maintaining all associated Rights-of-Way (ROW), Easements, and Permits for its fiber cable.

#### 6. Metering & Communications

IC shall install, own, operate, test and maintain the necessary revenue metering equipment. IC shall, at its own expense, install, operate, test, and maintain any communications equipment required to transmit data from the revenue metering at the IC's facility.

The revenue metering system (particularly the revenue metering current transformers) shall be designed to accurately meter the light loads that will occur when the facility is not generating power and only backfeeding station service from the Transmission Owner. This may require the use of high accuracy extended range current transformers.

Transmission Owner's Revenue Metering Requirements may be found in the *Requirements for Transmission Connected Facilities* document located at the following links:

www.firstenergycorp.com/feconnect

www.pjm.com/planning/design-engineering/to-tech-standards.aspx

These requirements are in addition to any metering required by PJM.

Transmission Owner will provide the telecommunication circuits for the SCADA RTU and the telephone in the Transmission Owner interconnection substation.

Transmission Owner will obtain real-time, site-specific, generation data from PJM, via the required communication link from IC to PJM. Transmission Owner will work with PJM and IC to ensure the generation data provided to PJM meets Transmission Owner's requirements.

Communications for transmission line protection between the new **interconnection** substation, and IC's **generation** (collector) substation, will be via fiber optics (see "Telecommunication Facilities" section above).

#### 7. Environmental, Real Estate and Permitting

The following are possible environmental, real estate and permitting issues:

- Environmental permitting, Real Estate acquisition, and Pennsylvania Public Utility Commission (PAPUC) notifications vary, some up to twelve (12) months after preliminary engineering is completed to secure the required approvals.
- IC is responsible for all property acquisition (including easements/rights-of-way (ROW)) for transmission, distribution and communication facilities needed for the generator interconnection.
- All work occurs within an existing transmission line right-of-way or on IC's property with access
  to all existing structures possible via that property and the right-of- way following established
  access routes that do not cross wetlands or streams.
- IC will develop, and secure regulatory approval for, all necessary Erosion and Sediment Control (E&SC) plans and National Pollutant Discharge Elimination System (NPDES) permits.
- IC will obtain all necessary permits within their scope of work. IC will not be responsible for permitting of work that is in the TO's scope to complete.
- IC will conduct all necessary wetlands and waterways studies and permits within their scope of work. IC will not be responsible for permitting of work that is in the TO's scope to complete.
- IC will conduct all necessary historical and archaeological studies within their scope of work. IC will not be responsible for studies for work that is in the TO's scope to complete.
- If the IC plans to cross the transmission line right of way with facilities or access roads, please
  refer to the Transmission Rights-of-Way Restrictions information located at:

   <u>https://www.firstenergycorp.com/help/safety/real-estate-power-lines/transmission-right-of-way.html#ROWform</u>

#### 8. Summary of Results of Study

	Direct		Indirect		
Work Description	Labor	Material	Labor	Material	<b>Total Cost</b>
AE2-285 Generator Lead					
<b>Termination</b> : Installation of	\$ 55,300	\$ 17,800	\$ 17,400	\$ 1,200	\$ 91,700
foundations, disconnect switch and	\$ 33,300	\$ 17,800	\$ 17,400	\$ 1,200	\$ 91,700
associated equipment to					
accommodate the termination of					
the 69 kV generator lead line.					

<b>Total Attachment Facilities Cost</b>	\$ 55,300	\$ 17,800	\$ 17,400	\$ 1,200	\$ 91,700
None	_	_	_	_	_
Total Direct Connection Cost	<b>\$ 0</b>	\$ 0	\$ <b>0</b>	\$ 0	<b>\$</b> 0
Total Direct Connection Cost	ΨΨ	ΨΟ	ΨΨ	ΨΟ	Ψ
Maysville: Extend the Maysville					
69 kV bus. Install one 69 kV	\$ 497,500	\$ 160,200	\$ 155,800	\$ 10,400	\$ 823,900
circuit breaker.					
Estimated SCADA work at					
Maysville substation to support					
breaker and relay installations.					
Estimated in-sub fiber run from					
Maysville control house to	\$ 38,900	\$ 4,100	\$ 12,200	\$ 300	\$ 55,500
developer ran fiber build for					
communications and control to					
AE2-285 Generation					
Interconnection.					
<b>Sharon:</b> Modify relay settings.	\$ 72,600	\$ 0	\$ 22,700	\$ 0	\$ 95,300
<b>Dilworth:</b> Modify relay settings.	\$ 72,600	\$ 0	\$ 22,700	\$ 0	\$ 95,300
McDowell: Modify relay settings.	\$ 72,600	\$ 0	\$ 22,700	\$ 0	\$ 95,300
Masury: Modify relay settings.	\$ 72,600	\$ 0	\$ 22,700	\$ 0	\$ 95,300
Project Management: Project	\$ 182,500	\$ 0	\$ 57,100	\$ 0	\$ 239,600
Management	ψ 102,300	\$ 0	\$ 57,100	\$ 0	\$ 239,000
<b>Total Non-Direct Connection</b>					
Network Upgrades	\$ 1,009,300	\$ 164,300	\$ 315,900	\$ 10,700	\$ 1,500,200
Metering: Customer-owned					
revenue metering at generation	\$ 1,900	\$ 0	\$ 600	\$ 0	\$ 2,500
facility.					
<b>Total Other Charges</b>	\$ 1,900	\$ 0	\$ 600	\$ 0	\$ 2,500
<b>Total Project Costs</b>	\$ 1,066,500	\$ 182,100	\$ 333,900	\$ 11,900	\$ 1,594,400

Generation projects meeting IRS "Safe Harbor" provisions generally do not incur "CIAC" (Contribution in Aid to Construction), a tax collected by the utility for the state or federal government. First Energy does not expect to collect CIAC for this project. If for any reason, "CIAC" would be required for this project, it would be the responsibility of the party owning the generator to pay this cost.

First Energy reserves the right to charge the Interconnection Customer operation and maintenance expenses to maintain the Interconnection Customer attachment facilities, including metering facilities, owned by First Energy. This must be included in Schedule E of the Interconnection Service Agreement.

#### 9. Schedules and Assumptions

A proposed **twelve** (12) **month Direct Connection** schedule is estimated to complete the engineering, construction and the associated activities, from the date of a fully executed Interconnection Construction Service Agreement and Construction Kick-Off Meeting. This schedule assumes that all issues covered by the "Environmental, Real Estate and Permitting Issues" section of this document are resolved, and outages (typically not granted from June through September) will occur as planned. Construction cannot begin until after all applicable permits and/or easements have been obtained.

12 month Schedule

Activity	Start Month	End Month
Preliminary Engineering	1	3
Siting, Permits & Real Estate	2	6
Detailed Engineering	2	6
Equipment Delivery	7	8
Below Grade Construction – Substation	8	9
Below Grade Construction – T-Lines	9	10
Above Grade Construction – Substation	9	11
Above Grade Construction – T-Lines	10	11
Testing & Commissioning	12	12

#### PROTECTION SCOPE

#### **Short Circuit Values**

The preliminary 69kV fault values at the AE2-285 interconnection location (Maysville 69kV) are:

Three phase = 10.4kASingle line to ground = 10.1kAZ1= (1.7 + j 7.6)%Z0= (1.6 + j 8.4)%

These values are provided for bolted, symmetrical faults under anticipated normal system conditions and are provided on a 71.07kV, 100MVA base. Future increases in fault currents are possible and it is the customer's responsibility to upgrade their equipment and/or protective equipment coordination when necessary.

#### **Protection Requirements**

The AE2-285 facility shall consist of inverter-based PV and connect directly to the Maysville substation 69kV bus via a dedicated line. It is understood that the customer will be using a single 69-34.5kV transformer rated 33/44/55 MVA.

The developer will need to provide information on the inverters and show that they meet the requirements of UL 1741 certification for anti-islanding protection. Any necessary intertie functions will be incorporated into the line relaying at the customer terminal of the interconnecting line. The customer will not supply fault current to the FE system.

Scope and cost estimates supplied assume that that the AE2-285 facility will meet the requirements as stated above, but documentation must be supplied to FirstEnergy to verify inverters meet these standards.

#### AE2-285 69kV Station

#### Main 69/34.5kV Transformer

- The interconnecting 69-34.5kV transformer shall have a delta or ungrounded wye winding on the transmission (69kV) side of the transformer.
- One 69kV, three-phase circuit breaker will be required on the FE side of the customer's main 69/34.5kV delta/wye grounded transformer.
- The circuit breaker shall be fully rated to interrupt available fault current when calculated according to the latest ANSI standard.
  - Bypass switches shall NOT be installed across the breaker. If the customer desired the
    added reliability benefit of being able to keep the substation energized while performing
    breaker maintenance, a ring bus or dedicated sparing circuit breaker is required.
  - o If the circuit breaker uses gas as an interrupting medium, the device shall be equipped with a low gas pressure alarming/tripping/lockout scheme (as appropriate for the particular device) in order to minimize the possibility of a transmission fault resulting from a loss of insulating gas.
- The interconnecting transformer and all 69kV facilities at the customer substation shall have redundant, high-speed protection inclusive of the 69kV breaker and high-side metering and shall trip, at minimum, this breaker. Separate CTs and tripping paths are required between the primary and backup relaying.
  - Overall Transformer Differential Protection Relay minimum functions: 87OA. (FE standard device is SEL-587 or SEL-487E)
    - The 69kV source for overall transformer differential protection shall be CTs on the utility source side of the transformer breaker. The low side source for primary differential protection shall be CTs on the bus side of the low side transformer breaker
  - o Primary Transformer Differential Protective Relay minimum functions: 87T. (FE standard device is SEL-587 or SEL-487E)
    - The 69kV source for primary transformer differential protection shall be CTs on the utility source side of the transformer or transformer breaker separate from the overall differential relay. The low side source for primary differential protection shall be CTs on the bus side of the low side transformer breaker separate from the overall differential relay
  - Backup Transformer Protective Relay minimum functions: High-side 50, 51, 50N and 51N: Low side - 51G. (FE standard device is SEL-551)
    - The source for the high-side backup transformer protection shall be separate CTs from the overall CTs on the utility source side of the transformer breaker closest to the line.
  - Breaker Failure (BF) Relay Dedicated breaker failure relay with associated hand-reset lock out relay (LOR). Will be wired to trip the breaker at Maysville to isolate from the transmission system if there is a failure to trip operation. (FE standard device is SEL-501).
    - Direct transfer trip for breaker failure, anti-islanding, and other functions as needed shall be communicated via fiber using the associated SEL-411L primary and backup relays. Trip on loss of channel to both the primary and backup schemes.

- CTs used for the zones of protection covering the high voltage portion of the customer's system shall use C800 relay accuracy CTs. These CTs should not saturate for the maximum throughfault current that can be experienced by the relay for the tap ratio in use.
- The relaying system shall have a reliable source of power independent from or immune to disturbances/loss of the AC system (e.g. DC battery and charger) to ensure proper operation of the protection schemes and tripping of the circuit breakers.
- The customer will be required to coordinate with upstream protection. It is solely the customer's
  responsibility to install and design their relaying to ensure adequate protection of their
  equipment.
- Detailed one-line diagrams with proposed protection should be provided well in advance of
  design and engineering to allow for approval of the protection scheme and preliminarily validate
  coordination with FE system.
- The low-side of the transformer shall have a dedicated circuit breaker with CTs adequate for use with, at minimum, the transformer differential relaying.

#### 69kV Line and Intertie Relaying

- The line between Maysville and AE2-285 station will require redundant fiber optic based communications channels to be installed and maintained between the facilities for use with highspeed line current differential protection.
  - Separate primary and backup SEL-411L relays at the AE2-285 station will be required.
     Separate primary and backup SEL-411L relays will also be required at Maysville.
  - o Intertie relay functionality (e.g. overfrequency, underfrequency, phase and ground overvoltage, directional overcurrent, and directional power) will be incorporated into the SEL-411L line relaying at AE2-285 as necessary
  - The source CTs for the line current differential relays at the customer station shall be separate sets of 1200:5 CTs (C800 or better). These shall be located in the transformerside bushings of the customer's high-side breakers
    - Line and transformer zones of protection overlap through the breaker.
  - The primary SEL-411L relays shall be sourced from an inner set of CTs and the backup SEL-411L relays sourced from an outer set of CTs on the transformer side of the customer's high-side breaker such that the backup SEL-411L scheme encompasses the primary.
  - PTs with separate secondary windings on the high/transmission-side of the interconnecting transformer with separate tripping paths are required for the line/intertie relays.

#### **Generator Owner's System Protection**

• The generator owner (GO) is to design their protective system to clear any fault within their zones of protection with one or more of their local breakers.

The Connecting Party shall provide utility-grade relays for protection of the FE Transmission System. FE shall approve all relays specified for the protection of the FE Transmission System, including time delay and auxiliary relays. Relay operation for any of the listed functions that are required shall initiate immediate separation of the parallel generation from the FE Transmission System:

Relay	Function
Frequency	To detect underfrequency and overfrequency operation.

Overvoltage	To detect overvoltage operation.
Undervoltage	To detect undervoltage operation.
Ground Fault Detector	To detect a circuit ground on the FE Transmission System.
Phase Fault Detector	To detect phase to phase faults on the FE Transmission System.
Transfer Trip Receiver	To provide tripping logic to the generation owner for isolation of the
	generation upon opening of the FE supply circuits.
Directional Power	To detect, under all system conditions, a loss of FE primary source. The
	relay shall be sensitive enough to detect transformer magnetizing current
	supplied by the generation.

The Interconnection Customer will be required to comply with all FE Generation Protection Requirements for Generation Interconnection Customers. The Generation Protection Requirements may be found within the "FirstEnergy Requirements for Transmission Connected Facilities" document located at the following links:

www.firstenergycorp.com/feconnect

www.pjm.com/planning/design-engineering/to-tech-standards.aspx

#### **FE System Modifications**

System modifications may be required to make settings changes and/or replace existing relays at FirstEnergy remote substation. Customer relaying will be required to coordinate with upstream transmission system protection.

#### **Maysville Substation**

- Extend the bus to add (1) new breaker for the AE2-285 line exit. Breaker shall be rated 40kAIC, with continuous current rating specified by Transmission Planning
- Relaying on new line exit shall be (2) SEL-411L relays for use with the 87L line protection differential scheme (as well as other protection communication) with AE2-285. Fiber communications path as previously specified.
- o (1) SEL-501 breaker failure relay
- o Incorporate new breaker into both the primary and backup SEL-587Z bus protection schemes.
- o Modifications to aux relays and lockouts as necessary
- Wire sparing breaker B18 CTs into new line exit relaying. Settings changes will be required for B18 relaying. Adjust transfer/sparing switches to incorporate new line exit breaker.

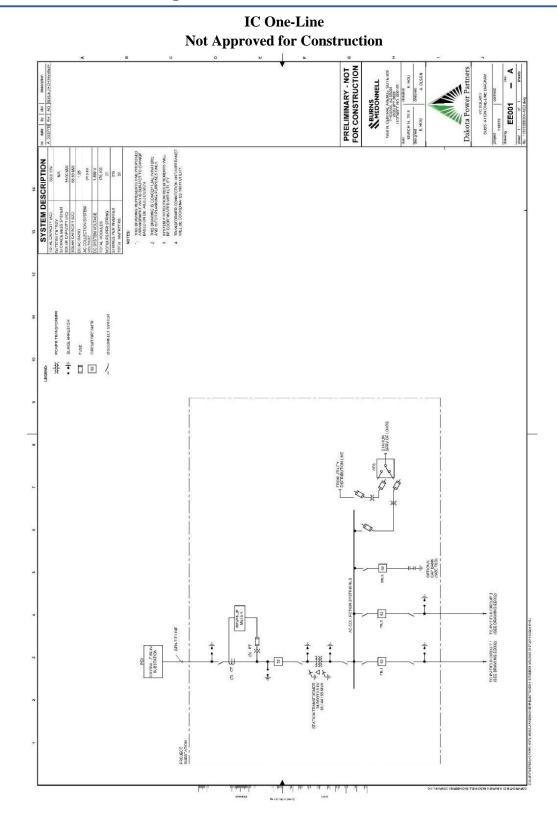
#### **Circuit Breaker Adequacy**

o PJM does not identify any new breakers as overdutied by this project

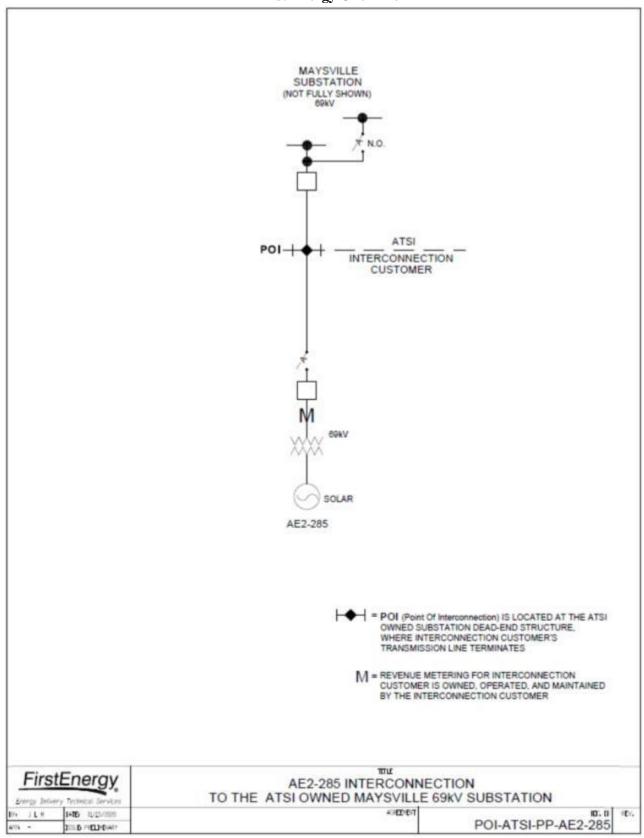
#### **Settings Changes**

Settings changes are possible at, but not limited to, the following stations:

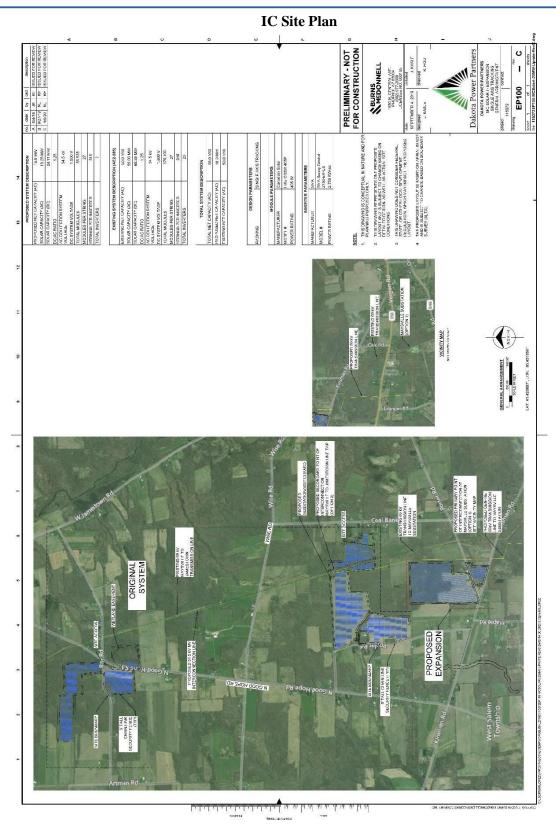
- o Dilworth
- Masury
- o McDowell
- o Maysville
- o Sharon



#### **First Energy One-Line**



## **Attachment #3: IC Site Plan and Substation Attachment Facilities**



# **Generation Connection Requirements**

The proposed interconnection facilities must be designed in accordance with the Transmission Owner's *Requirements for Transmission Connected Facilities* documents located at either of the following links:

www.firstenergycorp.com/feconnect

www.pjm.com/planning/design-engineering/to-tech-standards.aspx

The following is an excerpt taken from Transmission Owner's *Requirements for Transmission Connected Facilities* document:

For all generation facilities, other than wind-powered and other non-synchronous generating facilities, the minimum requirement shall be the provision of a reactive power capability sufficient to maintain a composite power delivery at continuous rated power output at a power factor as defined in the table below. This requirement will be measured at either the POI or generator terminals as specified in the table below. These reactive requirements apply to both the initial installation as well as to any incremental change in unit MW capability. FE will coordinate with the Connecting Party to identify the optimal generator step-up transformer tap to make such a capability available when demanded.

For all wind-powered or other non-synchronous generating facilities the minimum requirement shall be the provision of a reactive power capability sufficient to maintain a composite power delivery at a power factor as defined in the table. This requirement will be measured at either the POI or generator's terminals as specified in the table below. These reactive requirements apply to both the initial installation as well as to any incremental change in unit MW capability. FE will coordinate with the Connecting Party to identify the optimal generator step-up transformer tap to make such a capability available when needed.

For projects that entered PJM's New Service Queue after November 1, 2016, the power factor requirement will be as follows:

Generati on	New / Increa	Size	Power Factor Requirement	Measurement Location
Synchronou	New	> 20 MW	0.95 leading to 0.90	Generator's
Synchronou	New	<= 20 MW	0.95 leading to 0.90	Point of
Wind or Non-	New	All	0.95 leading to 0.95 lagging	High Side of the Facility
Synchronou	Increase		1.0 (unity) to 0.90	Generator's
Synchronou	Increase	<= 20 MW	` ,	Point of
Wind or Non-	Increase	All	0.95 leading to 0.95 lagging	High Side of the Facility

Any different reactive power requirements that FE and/or PJM determines to be appropriate for wind-powered or other non-synchronous generation facilities will be stated in the applicable *interconnection agreement(s).* 

Induction generators and other generators with no inherent VAR (reactive power) control capability, or those that have a restricted VAR capability less than the defined requirements, must provide dynamic supplementary reactive support located at the generation facility with electrical characteristics equivalent to that provided by a similar-sized synchronous generator.

#### **Design Requirements**

IC is responsible for specifying appropriate equipment and facilities such that the parallel generation is compatible with Transmission Owner's Transmission System. IC is also responsible for meeting any applicable federal, state, and local codes.

#### **Transmission Design Requirements**

#### **Design Criteria**

Facilities owned and operated by Transmission Owner shall comply with the applicable Transmission Owner technical requirements and standards posted on the PJM website per the PJM Tariff, and the following criteria. Where there are different requirements for the same criterion, the more restrictive shall apply. IC must abide by any PJM, RFC or NERC criteria imposed that is more restrictive than those of Transmission Owner.

#### **General Design Requirements**

•	System phasing (counter clockwise)	X-Y-Z
•	System frequency:	60 hertz
•	Elevation, AMSL:	Less than 1000 meters
•	Isokeraunic level:	40
•	Maximum ambient temperature:	40 degrees C
•	Minimum ambient temperature:	-40 degrees C
•	Maximum conductor operating temperature:	Contact Transmission Owner
•	Wind Loading (round shapes):	Per ASCE 7-98, per Fig. 6-1
	•	depending on location
•	Ice loading – Substations (no wind):	25 mm
•	Seismic zone:	Per ASCE 7-98, per Fig. 9.4.1.1(a) and (b). Equipment qualification
		per IEEE 693-97

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#### **Voltage and Current Ratings**

•	Nominal phase-to-phase:	69 kV
•	Maximum phase-to-phase:	72.5 kV
•	Basic impulse level (BIL):	350 kV
•	Maximum continuous current carrying capacity:	2000 A

•	Design fault current:	40 kA
Clearances a	nd Spacing	
•	Recommended rigid bus center-to-center phase spacing:	60"
•	Minimum phase-to-phase, metal-to-metal distance:	31"
•	Recommended phase-to-ground:	29"
•	Minimum phase-to-ground:	25"
•	Minimum vertical clearance from live parts to grade:	10'-5"
•	Minimum horizontal clearance from live parts:	4'-11"
•	Minimum bottom of insulator to top of foundation:	8'-6"