

Generation Interconnection Feasibility Study Report Queue Position AB2-136

The Interconnection Customer (IC) has proposed a 60 MW (24.8 MWC) solar generating facility to be located in Cambridge, Maryland. PJM studied the AB2-136 project at both a Primary and Secondary Point of Interconnection. The study results are provided below. The planned in-service date, as requested by the IC during the project kick-off call, is May 1, 2018. This date may not be attainable due to required additional studies and construction schedules.

Point(s) of Interconnection

The Interconnection Customer requested a Primary and Secondary Point of Interconnection (POI) be evaluated for the AB2-136 project. Both POIs are at the 69 kV transmission level.

Primary Point of Interconnection

PJM studied the AB2-136 project into the Delmarva Power and Light Company (DPL) system as a direct connection into the West Cambridge 69 kV Substation and evaluated it for compliance with reliability criteria for summer peak conditions in 2020.

Transmission Owner Scope of Attachment Facilities Work

Substation Interconnection Estimate

Scope: Reconfigure West Cambridge 69 kV Substation to be a 5 position ring bus. This will include adding 3 new 69 kV circuit breakers, disconnect switches, CVTs, line relays, breaker relays, and associated bus equipment and support structures.

Estimate: \$2,974,000

Construction Time: 24 months

Major Equipment Included in Estimate:

- | | |
|--|---------|
| • Power Circuit Breaker, 69 kV, 2000A, 40kA, 3 cycle | Qty. 3 |
| • Disconnect Switch, 69 kV, 2000A, Manual Wormgear, Arcing Horns | Qty. 10 |
| • CT/VT Combination Units, 69 kV | Qty. 3 |
| • CVTs | Qty. 6 |
| • Disconnect Switch Stand, High, 69 kV, Steel | Qty. 6 |
| • Disconnect Switch Stand, Low, 69 kV, Steel | Qty. 4 |
| • CT/VT Stand, Single Phase, Low, 69 kV, Steel | Qty. 3 |
| • CVT Stand, Single Phase, Low, 69 kV, Steel | Qty. 6 |
| • Relay Panel, Transmission Line, FL/BU (20") | Qty. 3 |
| • Control Panel, 69 kV Circuit Breaker (10") | Qty. 3 |
| • Bus Support Structure, 3 phase, 69 kV, Steel | Qty. 8 |

Estimate Assumptions:

- Property and substation within existing fence line is large enough to allow construction of a 69 kV ring bus.
- Permitting will be performed by DPL.
- No additional purchase of property required.
- No expansion of the existing control house is required.

Required Relaying and Communications

New protection relays are required for the new terminals. An SEL-487 will be required for primary protection and an SEL-387 will be required for back-up protection. One 20" relay panel for each line terminal will be required for front line and back-up protection.

An SEL-451 relay on a 20" breaker control panel will be required for the control and operation of each new 69 kV circuit breaker.

The project will require re-wiring and adjustment of existing relay schemes to accommodate the new 69 kV arrangement.

The cost of the required relay and communications is included in the Substation Interconnection Estimate.

Metering

Three phase 69 kV revenue metering points will need to be established. DPL will purchase and install all metering instrument transformers as well as construct a metering structure. The secondary wiring connections at the instrument transformers will be completed by DPL's metering technicians. The metering control cable and meter cabinets will be supplied and installed by DPL. DPL will install conduit for the control cable between the instrument transformers and the metering enclosure. The location of the metering enclosure will be determined in the construction phase. DPL will provide both the Primary and the Backup meters. DPL's meter technicians will program and install the Primary & Backup solid state multi-function meters for each new metering position. Each meter will be equipped with load profile, telemetry, and DNP outputs. The IC will be provided with one meter DNP output for each meter. DPL will own the metering equipment for the interconnection point, unless the IC asserts its right to install, own, and operate the metering system.

The Interconnection Customer will be required to make provisions for a voice quality phone line within approximately 3 feet of each Company metering position to facilitate remote interrogation and data collection.

It is the IC's responsibility to send the data that PJM and DPL requires directly to PJM. The IC will grant permission for PJM to send DPL the following telemetry that the IC sends to PJM: real time MW, MVAR, volts, amperes, generator status, and interval MWH and MVARH.

The estimate for DPL to design, purchase, and install metering as specified in the aforementioned scope for metering is included in the Substation Interconnection Estimate.

Interconnection Customer Scope of Work

The Interconnection Customer is responsible for all design and construction related to activities on their side of the Point of Interconnection. Site preparation, including grading and an access road, as necessary, is assumed to be by the IC. Route selection, line design, and right-of-way acquisition of the direct connect facilities is not included in this report, and is the responsibility of the IC. The IC is also required to provide revenue metering and real-time telemetering data to PJM in conformance with the requirements contained in PJM Manuals M-01 and M-14 and the PJM Tariff.

DPL Interconnection Customer Scope of Direct Connection Work Requirements

- DPL requires that an IC circuit breaker is located within 500 feet of West Cambridge substation to facilitate the relay protection scheme between DPL and the IC at the Point of Interconnection (POI).

Special Operating Requirements

1. DPL will require the capability to remotely disconnect the generator from the grid by communication from its System Operations facility. Such disconnection may be facilitated by a generator breaker, or other method depending upon the specific circumstances and the evaluation by DPL.
2. DPL reserves the right to charge the Interconnection Customer operation and maintenance expenses to maintain the Interconnection Customer attachment facilities, including metering and telecommunications facilities, owned by DPL.

Summer Peak Analysis – 2020

Transmission Network Impacts

Potential transmission network impacts are as follows:

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

1. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 55.38% to 74.81% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.07 MW to the thermal violation.

CONTINGENCY 'DP11'/*STEELE BUS BREAKER TO MILFORD
 DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
 230 230
 DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1/*STEELE VIENNA
 230 230
 END

Please refer to Appendix 1 for a table containing the generators having contribution to this flowgate.

2. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 61.3% to 80.73% (**DC power flow**) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.07 MW to the thermal violation.

CONTINGENCY 'DP11'/*STEELE BUS BREAKER TO MILFORD
 DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
 230 230
 DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1/*STEELE VIENNA
 230 230
 END

Please refer to Appendix 2 for a table containing the generators having contribution to this flowgate.

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. “Network Impacts”, identified for earlier generation or transmission interconnection projects in the PJM Queue)

1. (DP&L – DP&L) The MILF_230-STEELE 230 kV line (from bus 232004 to bus 232000 ckt 1) loads from 143.78% to 145.28% (DC power flow) of its emergency rating (551 MVA) for the tower line contingency outage of 'DBL_4NC'. This project contributes approximately 18.4 MW to the thermal violation.

CONTINGENCY 'DBL_4NC'* RED LION-CEDAR CREEK 230;RED LION-CARTANZA
 230
 OPEN LINE FROM BUS 231004 TO BUS 232002 CKT 1
 OPEN LINE FROM BUS 231004 TO BUS 232003 CKT 1
 END

Please refer to Appendix 5 for a table containing the generators having contribution to this flowgate.

Summer Peak Load Flow Analysis Reinforcements

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

1. To mitigate the (DP&L) PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) overload will require the replacement of a disconnect switch at Preston Substation. The estimate to perform this work is **\$36,000** and will take approximately **1 year** to complete.
2. To mitigate the (DP&L) TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) overload will require substation reinforcements at Preston Substation and Todd Substation. The estimate to perform this work is **\$67,000** and will take approximately **1 year** to complete.

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

(Summary form of Cost allocation for transmission lines and transformers will be inserted here if any)

1. To mitigate the (DP&L) MILF_230-STEELE 230 kV line (from bus 232004 to bus 232000 ckt 1) overload will require rebuilding of the circuit including the replacement of poles to increase the emergency rating. The estimate to perform this work is **\$43,965,000** and will take **4 years** to complete.

Steady-State Voltage Requirements

To be performed during later study phases.

Short Circuit

No issues identified.

Stability and Reactive Power Requirement

To be performed during later study phases.

Light Load Analysis - 2020

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

1. (DP&L - DP&L) The SHARPTWN-W1-070TAP1 69 kV line (from bus 232239 to bus 901490 ckt 1) loads from 66.94% to 92.74% (DC power flow) of its emergency rating (43 MVA) for the single line contingency outage of 'CKT 6708'. This project contributes approximately 11.09 MW to the thermal violation.

CONTINGENCY 'CKT 6708'

DISCONNECT BUS 232270/ MARDELA - HEBRON 69 & HEBRON XFMR

DISCONNECT BUS 232838/ VIENNA - MARDELA 69

DISCONNECT BUS 232644/ HEBRON 12

DISCONNECT BUS 232291/ ROCKAWALKIN - NORTH SALISBURY 69

END

2. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 81.07% to 96.09% (DC power flow) of its emergency rating (58 MVA) for the single line contingency outage of 'CKT 6728'. This project contributes approximately 8.71 MW to the thermal violation.

CONTINGENCY 'CKT 6728'

OPEN LINE FROM BUS 232272 TO BUS 232274 CIRCUIT 1/MOUNT HERMON - PINEY GROVE 69

DISCONNECT BUS 230912 PINEY GROVE 69 CAP

END

3. (DP&L - DP&L) The W1-070TAP1-LAUREL 69 kV line (from bus 901490 to bus 232249 ckt 1) loads from 66.71% to 92.5% (DC power flow) of its emergency rating (43 MVA) for the single line contingency outage of 'CKT 6708'. This project contributes approximately 11.09 MW to the thermal violation.

CONTINGENCY 'CKT 6708'

DISCONNECT BUS 232270/ MARDELA - HEBRON 69 & HEBRON XFMR

DISCONNECT BUS 232838/ VIENNA - MARDELA 69

DISCONNECT BUS 232644/ HEBRON 12

DISCONNECT BUS 232291/ ROCKAWALKIN - NORTH SALISBURY 69

END

Facilities Study Estimate

(If a Facilities Study is required, provide the estimated duration and cost estimate to perform Facilities Study)

7 months; \$100,000

Delmarva Power and Light Costs

Cost estimates will further be refined as a part of the Impact Study and Facilities Study for this project. The Interconnection Customer will be responsible for all costs incurred by DPL in connection with the AB2-136 project. Such costs may include, but are not limited to, any transmission system assets currently in DPL's rate base that are prematurely retired due to the AB2-136 project. PJM shall work with DPL to identify these retirement costs and any additional expenses. DPL reserves the right to reassess issues presented in this document and, upon appropriate justification, submit additional costs related to the AB2-136 project.

Secondary Point of Interconnection

PJM studied the AB2-136 project into the Delmarva Power and Light Company (DPL) system at a tap of the West Cambridge-Bayly 69 kV circuit and evaluated it for compliance with reliability criteria for summer peak conditions in 2020.

Summer Peak Analysis - 2020

Transmission Network Impacts

Potential transmission network impacts are as follows:

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

1. (DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 55.28% to 74.91% (DC power flow) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.26 MW to the thermal violation.

CONTINGENCY 'DP11'/*STEELE BUS BREAKER TO MILFORD

DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
230 230

DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1/*STEELE VIENNA
230 230
END

Please refer to Appendix 1 for a table containing the generators having contribution to this flowgate.

2. (DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 61.19% to 80.83% (DC power flow) of its emergency rating (93 MVA) for the line fault

with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.26 MW to the thermal violation.

CONTINGENCY 'DP11'/*STEELE BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1/*MILFORD STEELE
230 230
DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1/*STEELE VIENNA
230 230
END

Please refer to Appendix 2 for a table containing the generators having contribution to this flowgate.

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

1. (DP&L - DP&L) The MILF_230-STEELE 230 kV line (from bus 232004 to bus 232000 ckt 1) loads from 143.82% to 145.32% (DC power flow) of its emergency rating (551 MVA) for the tower line contingency outage of 'DBL_4NC'. This project contributes approximately 18.31 MW to the thermal violation.

CONTINGENCY 'DBL_4NC'/* RED LION-CEDAR CREEK 230;RED LION-CARTANZA
230
OPEN LINE FROM BUS 231004 TO BUS 232002 CKT 1
OPEN LINE FROM BUS 231004 TO BUS 232003 CKT 1
END

Please refer to Appendix 5 for a table containing the generators having contribution to this flowgate.

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

1. (DP&L - DP&L) The SHARPTWN-W1-070TAP1 69 kV line (from bus 232239 to bus 901490 ckt 1) loads from 66.94% to 92.61% (DC power flow) of its emergency rating (43 MVA) for the single line contingency outage of 'CKT 6708'. This project contributes approximately 11.04 MW to the thermal violation.

CONTINGENCY 'CKT 6708'

DISCONNECT BUS 232270 / MARDELA - HEBRON 69 & HEBRON XFMR

DISCONNECT BUS 232838 / VIENNA - MARDELA 69

DISCONNECT BUS 232644 / HEBRON 12

DISCONNECT BUS 232291/ ROCKAWALKIN - NORTH SALISBURY 69

END

2. (DP&L - DP&L) The ROCKAWLKN-NSALSBRV 69 kV line (from bus 232291 to bus 232271 ckt 1) loads from 81.07% to 96.01% (DC power flow) of its emergency rating (58 MVA) for the single line contingency outage of 'CKT 6728'. This project contributes approximately 8.67 MW to the thermal violation.

CONTINGENCY 'CKT 6728'

OPEN LINE FROM BUS 232272 TO BUS 232274 CIRCUIT 1/MOUNT HERMON - PINEY GROVE 69

DISCONNECT BUS 230912/ PINEY GROVE 69 CAP

END

3. (DP&L - DP&L) The W1-070TAP1-LAUREL 69 kV line (from bus 901490 to bus 232249 ckt 1) loads from 66.71% to 92.38% (DC power flow) of its emergency rating (43 MVA) for the single line contingency outage of 'CKT 6708'. This project contributes approximately 11.04 MW to the thermal violation.

CONTINGENCY 'CKT 6708'

DISCONNECT BUS 232270 / MARDELA - HEBRON 69 & HEBRON XFMR

DISCONNECT BUS 232838/ VIENNA - MARDELA 69

DISCONNECT BUS 232644 / HEBRON 12

DISCONNECT BUS 232291/ ROCKAWALKIN - NORTH SALISBURY 69

END

Appendices

(Primary Point of Interconnection)

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 55.38% to 74.81% (DC power flow) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.07 MW to the thermal violation.

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CONTINGENCY 'DP11'                                /*STEELE BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1      /*MILFORD
STEELE 230 230
DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1      /*STEELE
VIENNA 230 230
END
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<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232926	CRISFLD1	1.20
293670	O-025 C	0.80
297076	V2-028 C	0.50
297077	V2-028 E	0.81
904212	V4-022E	0.36
232919	VN10	3.11
232907	VN8	22.70
901003	W1-003 C	0.87
901004	W1-003 E	0.52
901013	W1-004 C	0.87
901014	W1-004 E	0.52
901023	W1-005 C	0.87
901024	W1-005 E	0.52

901033	W1-006 C	0.87
901034	W1-006 E	0.52
907052	X1-032 E	0.47
907323	X1-096 C	2.35
907324	X1-096 E	11.19
910571	X3-008 C	2.93
910572	X3-008 E	4.78
910591	X3-015 C	2.10
910592	X3-015 E	3.43
913411	Y1-080 C	0.35
913412	Y1-080 E	0.56
915541	Y3-058 C	0.88
915542	Y3-058 E	1.43
920582	Z1-076 C	0.61
920583	Z1-076 E	1.00
920592	Z1-077 C	0.44
920593	Z1-077 E	0.71
916441	Z1-100	0.48
916451	Z1-101	0.48
916461	Z1-102	0.48
920602	Z1-103	0.48
917082	Z2-012 E	1.42
920763	Z2-076 E	0.18
920773	Z2-077 E	0.18
920952	AA1-025	0.42
920962	AA1-026	0.42
920972	AA1-027	0.42
920982	AA1-028	0.42
921122	AA1-059 C	0.52
921123	AA1-059 E	0.20
921142	AA1-061 C	4.87
921143	AA1-061 E	2.40
918831	AA1-102	4.51
921592	AA1-140 C	0.67
921593	AA1-140 E	1.10
921602	AA1-141 C	0.65
921603	AA1-141 E	1.07

922213	AA2-129 E	2.29
922222	AA2-130	0.24
922752	AB1-056 C OP	4.91
922753	AB1-056 E OP	13.99
922762	AB1-057 C	4.99
922763	AB1-057 E	14.22
923282	AB1-137 C	1.14
923283	AB1-137 E	0.49
923902	AB2-030 E	0.46
923931	AB2-033 C	0.82
923932	AB2-033 E	0.32
924361	AB2-084 C	0.45
924362	AB2-084 E	0.73
924461	AB2-095 C	1.16
924462	AB2-095 E	1.89
924681	AB2-120 C OP	4.32
924682	AB2-120 E OP	7.04
924781	AB2-130 C OP	4.57
924782	AB2-130 E OP	7.45
924831	AB2-136 C OP	7.47
924832	AB2-136 E OP	10.60
925091	AB2-166 C	0.26
925092	AB2-166 E	0.45
925101	AB2-167 C	0.61
925102	AB2-167 E	1.00
925151	AB2-172 C OP	7.33
925152	AB2-172 E OP	11.96
925231	AB2-177 C	0.29

925232	AB2-177 E	0.47
925261	AB2-180 C	2.15
925262	AB2-180 E	0.92

Appendix 2

(DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 61.3% to 80.73% (DC power flow) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.07 MW to the thermal violation.

CONTINGENCY 'DP11' /*STEELE BUS BREAKER TO MILFORD
DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1 /*MILFORD
STEELE 230 230
DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1 /*STEELE
VIENNA 230 230
END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232926	CRISFLD1	1.20
293670	O-025 C	0.80
297076	V2-028 C	0.50
297077	V2-028 E	0.81
904212	V4-022E	0.36
232919	VN10	3.11
232907	VN8	22.70
901003	W1-003 C	0.87
901004	W1-003 E	0.52
901013	W1-004 C	0.87
901014	W1-004 E	0.52
901023	W1-005 C	0.87
901024	W1-005 E	0.52
901033	W1-006 C	0.87
901034	W1-006 E	0.52
907052	X1-032 E	0.47
907323	X1-096 C	2.35
907324	X1-096 E	11.19
910571	X3-008 C	2.93
910572	X3-008 E	4.78

910591	X3-015 C	2.10
910592	X3-015 E	3.43
913411	Y1-080 C	0.35
913412	Y1-080 E	0.56
915541	Y3-058 C	0.88
915542	Y3-058 E	1.43
920582	Z1-076 C	0.61
920583	Z1-076 E	1.00
920592	Z1-077 C	0.44
920593	Z1-077 E	0.71
916441	Z1-100	0.48
916451	Z1-101	0.48
916461	Z1-102	0.48
920602	Z1-103	0.48
917082	Z2-012 E	1.42
920763	Z2-076 E	0.18
920773	Z2-077 E	0.18
920952	AA1-025	0.42
920962	AA1-026	0.42
920972	AA1-027	0.42
920982	AA1-028	0.42
921122	AA1-059 C	0.52
921123	AA1-059 E	0.20
921142	AA1-061 C	4.87
921143	AA1-061 E	2.40
918831	AA1-102	4.51
921592	AA1-140 C	0.67
921593	AA1-140 E	1.10
921602	AA1-141 C	0.65
921603	AA1-141 E	1.07
922213	AA2-129 E	2.29
922222	AA2-130	0.24
922752	AB1-056 C OP	4.91
922753	AB1-056 E OP	13.99
922762	AB1-057 C	4.99

922763	AB1-057 E	14.22
923282	AB1-137 C	1.14
923283	AB1-137 E	0.49
923902	AB2-030 E	0.46
923931	AB2-033 C	0.82
923932	AB2-033 E	0.32
924361	AB2-084 C	0.45
924362	AB2-084 E	0.73
924461	AB2-095 C	1.16
924462	AB2-095 E	1.89
924681	AB2-120 C OP	4.32
924682	AB2-120 E OP	7.04
924781	AB2-130 C OP	4.57
924782	AB2-130 E OP	7.45
924831	AB2-136 C OP	7.47
924832	AB2-136 E OP	10.60
925091	AB2-166 C	0.26
925092	AB2-166 E	0.45
925101	AB2-167 C	0.61
925102	AB2-167 E	1.00
925151	AB2-172 C OP	7.33
925152	AB2-172 E OP	11.96
925231	AB2-177 C	0.29
925232	AB2-177 E	0.47
925261	AB2-180 C	2.15
925262	AB2-180 E	0.92

Appendix 5

(DP&L - DP&L) The MILF_230-STEELE 230 kV line (from bus 232004 to bus 232000 ckt 1) loads from 143.78% to 145.28% (DC power flow) of its emergency rating (551 MVA) for the tower line contingency outage of 'DBL_4NC'. This project contributes approximately 18.4 MW to the thermal violation.

CONTINGENCY 'DBL_4NC'

/* RED LION-CEDAR CREEK

230;RED LION-CARTANZA 230

OPEN LINE FROM BUS 231004 TO BUS 232002 CKT 1

OPEN LINE FROM BUS 231004 TO BUS 232003 CKT 1

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232900	DEMECSMY	30.59
232616	GEN FOOD	11.20
232904	IR4	269.47
232923	MR1	12.53
232924	MR2	12.53
232922	MR3	75.16
232901	NORTHST	33.16
297077	V2-028 E	1.28
904212	V4-022E	1.52
901004	W1-003 E	2.21
901014	W1-004 E	2.21
901024	W1-005 E	2.21
901034	W1-006 E	2.21
901411	W1-062	32.50
903511	W3-032A	227.70
907052	X1-032 E	1.89
907324	X1-096 E	42.96
910572	X3-008 E	3.32
910592	X3-015 E	3.81
913412	Y1-080 E	0.68
920543	Y3-054 E	8.30
915542	Y3-058 E	4.10
920582	Z1-076 C	2.63
920583	Z1-076 E	4.31
920592	Z1-077 C	1.88

920593	Z1-077 E	3.07
917082	Z2-012 E	6.09
920763	Z2-076 E	1.21
920773	Z2-077 E	1.21
921122	AA1-059 C	1.99
921123	AA1-059 E	0.79
921142	AA1-061 C	3.72
921143	AA1-061 E	1.83
921592	AA1-140 C	4.60
921593	AA1-140 E	7.51
921602	AA1-141 C	2.84
921603	AA1-141 E	4.63
921872	AA2-069	390.55
922213	AA2-129 E	9.83
922222	AA2-130	0.92
922752	AB1-056 C OP	41.90
922753	AB1-056 E OP	119.31
922762	AB1-057 C	42.55
922763	AB1-057 E	121.27
923282	AB1-137 C	8.78
923283	AB1-137 E	3.76
923902	AB2-030 E	1.96
923931	AB2-033 C	3.54
923932	AB2-033 E	1.37
924361	AB2-084 C	1.79
924362	AB2-084 E	2.93
924461	AB2-095 C	6.46
924462	AB2-095 E	10.53
924681	AB2-120 C OP	18.82
924682	AB2-120 E OP	30.70
924781	AB2-130 C OP	19.74

924782	AB2-130 E OP	32.21
924831	AB2-136 C OP	7.60
924832	AB2-136 E OP	10.79
925091	AB2-166 C	0.95
925092	AB2-166 E	1.66
925101	AB2-167 C	2.63
925102	AB2-167 E	4.31
925151	AB2-172 C OP	5.08
925152	AB2-172 E OP	8.29
925231	AB2-177 C	1.25
925232	AB2-177 E	2.04
925261	AB2-180 C	6.18
925262	AB2-180 E	2.65

Appendices

(Secondary Point of Interconnection)

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DP&L - DP&L) The PRESTON-TANYARD 69 kV line (from bus 232233 to bus 232821 ckt 1) loads from 55.28% to 74.91% (DC power flow) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.26 MW to the thermal violation.

CONTINGENCY 'DP11'

/*STEELE BUS BREAKER TO MILFORD

DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1 /*MILFORD
 STEELE 230 230
 DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1 /*STEELE
 VIENNA 230 230
 END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232926	CRISFLD1	1.2031
293670	O-025 C	0.80076
297076	V2-028 C	0.500411
297077	V2-028 E	0.805009
904212	V4-022E	0.355167
232919	VN10	3.111251
232907	VN8	22.69755
901003	W1-003 C	0.871568
901004	W1-003 E	0.51606
901013	W1-004 C	0.871568
901014	W1-004 E	0.51606
901023	W1-005 C	0.871568
901024	W1-005 E	0.51606
901033	W1-006 C	0.871568
901034	W1-006 E	0.51606
907052	X1-032 E	0.47312
907323	X1-096 C	2.346045
907324	X1-096 E	11.18883
910571	X3-008 C	2.93094
910572	X3-008 E	4.78206
910591	X3-015 C	2.098418
910592	X3-015 E	3.431197
913411	Y1-080 C	0.345774
913412	Y1-080 E	0.558558
915541	Y3-058 C	0.875292
915542	Y3-058 E	1.428108
920582	Z1-076 C	0.607645
920583	Z1-076 E	0.997455
920592	Z1-077 C	0.43567
920593	Z1-077 E	0.71083
916441	Z1-100	0.481656
916451	Z1-101	0.481656
916461	Z1-102	0.481656
920602	Z1-103	0.481656
917082	Z2-012 E	1.420668
920763	Z2-076 E	0.17734
920773	Z2-077 E	0.17734
920952	AA1-025	0.424316

920962	AA1-026	0.424316
920972	AA1-027	0.424316
920982	AA1-028	0.424316
921122	AA1-059 C	0.517333
921123	AA1-059 E	0.204527
921142	AA1-061 C	4.870766
921143	AA1-061 E	2.399034
918831	AA1-102	4.511625
921592	AA1-140 C	0.673892
921593	AA1-140 E	1.099508
921602	AA1-141 C	0.654645
921603	AA1-141 E	1.068105
922213	AA2-129 E	2.287
922222	AA2-130	0.24062
922752	AB1-056 C OP	4.91372
922753	AB1-056 E OP	13.99342
922762	AB1-057 C	4.99002
922763	AB1-057 E	14.22232
923282	AB1-137 C	1.14142
923283	AB1-137 E	0.48918
923902	AB2-030 E	0.45828
923931	AB2-033 C	0.824904
923932	AB2-033 E	0.320796
924361	AB2-084 C	0.449464
924362	AB2-084 E	0.733336
924461	AB2-095 C	1.160634
924462	AB2-095 E	1.893666
924681	AB2-120 C OP	4.30844
924682	AB2-120 E OP	7.02956
924781	AB2-130 C OP	4.53568
924782	AB2-130 E OP	7.40032
924831	AB2-136 C OP	7.54912
924832	AB2-136 E OP	10.71488
925091	AB2-166 C	0.2577
925092	AB2-166 E	0.450975
925101	AB2-167 C	0.607645
925102	AB2-167 E	0.997455
925151	AB2-172 C OP	7.23387
925152	AB2-172 E OP	11.80263
925231	AB2-177 C	0.287125
925232	AB2-177 E	0.470885
925261	AB2-180 C	2.14984
925262	AB2-180 E	0.92136

Appendix 2

(DP&L - DP&L) The TODD-PRESTON 69 kV line (from bus 232234 to bus 232233 ckt 1) loads from 61.19% to 80.83% (DC power flow) of its emergency rating (93 MVA) for the line fault with failed breaker contingency outage of 'DP11'. This project contributes approximately 18.26 MW to the thermal violation.

```
CONTINGENCY 'DP11'                                /*STEELE BUS BREAKER TO MILFORD
  DISCONNECT BRANCH FROM BUS 232004 TO BUS 232000 CKT 1      /*MILFORD
STEELE 230 230
  DISCONNECT BRANCH FROM BUS 232000 TO BUS 232005 CKT 1      /*STEELE
VIENNA 230 230
  END
```

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232926	CRISFLD1	1.2031
293670	O-025 C	0.80076
297076	V2-028 C	0.500411
297077	V2-028 E	0.805009
904212	V4-022E	0.355167
232919	VN10	3.111251
232907	VN8	22.69755
901003	W1-003 C	0.871568
901004	W1-003 E	0.51606
901013	W1-004 C	0.871568
901014	W1-004 E	0.51606
901023	W1-005 C	0.871568
901024	W1-005 E	0.51606
901033	W1-006 C	0.871568
901034	W1-006 E	0.51606
907052	X1-032 E	0.47312
907323	X1-096 C	2.346045
907324	X1-096 E	11.18883
910571	X3-008 C	2.93094
910572	X3-008 E	4.78206
910591	X3-015 C	2.098418
910592	X3-015 E	3.431197
913411	Y1-080 C	0.345774
913412	Y1-080 E	0.558558
915541	Y3-058 C	0.875292
915542	Y3-058 E	1.428108
920582	Z1-076 C	0.607645
920583	Z1-076 E	0.997455
920592	Z1-077 C	0.43567

920593	Z1-077 E	0.71083
916441	Z1-100	0.481656
916451	Z1-101	0.481656
916461	Z1-102	0.481656
920602	Z1-103	0.481656
917082	Z2-012 E	1.420668
920763	Z2-076 E	0.17734
920773	Z2-077 E	0.17734
920952	AA1-025	0.424316
920962	AA1-026	0.424316
920972	AA1-027	0.424316
920982	AA1-028	0.424316
921122	AA1-059 C	0.517333
921123	AA1-059 E	0.204527
921142	AA1-061 C	4.870766
921143	AA1-061 E	2.399034
918831	AA1-102	4.511625
921592	AA1-140 C	0.673892
921593	AA1-140 E	1.099508
921602	AA1-141 C	0.654645
921603	AA1-141 E	1.068105
922213	AA2-129 E	2.287
922222	AA2-130	0.24062
922752	AB1-056 C OP	4.91372
922753	AB1-056 E OP	13.99342
922762	AB1-057 C	4.99002
922763	AB1-057 E	14.22232
923282	AB1-137 C	1.14142
923283	AB1-137 E	0.48918
923902	AB2-030 E	0.45828
923931	AB2-033 C	0.824904
923932	AB2-033 E	0.320796
924361	AB2-084 C	0.449464
924362	AB2-084 E	0.733336
924461	AB2-095 C	1.160634
924462	AB2-095 E	1.893666
924681	AB2-120 C OP	4.30844
924682	AB2-120 E OP	7.02956
924781	AB2-130 C OP	4.53568
924782	AB2-130 E	7.40032

	<i>OP</i>	
924831	AB2-136 C <i>OP</i>	7.54912
924832	AB2-136 E <i>OP</i>	10.71488
925091	AB2-166 C	0.2577
925092	AB2-166 E	0.450975
925101	AB2-167 C	0.607645
925102	AB2-167 E	0.997455
925151	AB2-172 C <i>OP</i>	7.23387
925152	AB2-172 E <i>OP</i>	11.80263
925231	AB2-177 C	0.287125
925232	AB2-177 E	0.470885
925261	AB2-180 C	2.14984
925262	AB2-180 E	0.92136

Appendix 5

(DP&L - DP&L) The MILF_230-STEELE 230 kV line (from bus 232004 to bus 232000 ckt 1) loads from 143.82% to 145.32% (DC power flow) of its emergency rating (551 MVA) for the tower line contingency outage of 'DBL_4NC'. This project contributes approximately 18.31 MW to the thermal violation.

CONTINGENCY 'DBL_4NC'

/* RED LION-CEDAR CREEK

230;RED LION-CARTANZA 230

OPEN LINE FROM BUS 231004 TO BUS 232002 CKT 1

OPEN LINE FROM BUS 231004 TO BUS 232003 CKT 1

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
232900	DEMECSMY	30.59184
232616	GEN FOOD	11.200576
232904	IR4	269.466094
232923	MR1	12.52696
232924	MR2	12.52696
232922	MR3	75.16176
232901	NORTHST	33.1596
297077	V2-028 E	1.277832
904212	V4-022E	1.5221
901004	W1-003 E	2.205225
901014	W1-004 E	2.205225

901024	W1-005 E	2.205225
901034	W1-006 E	2.205225
901411	W1-062	32.50383
903511	W3-032A	227.69592
907052	X1-032 E	1.8882
907324	X1-096 E	42.96228
910572	X3-008 E	3.317248
910592	X3-015 E	3.80908
913412	Y1-080 E	0.678174
920543	Y3-054 E	8.30388
915542	Y3-058 E	4.104276
920582	Z1-076 C	2.625991
920583	Z1-076 E	4.310589
920592	Z1-077 C	1.882786
920593	Z1-077 E	3.071914
917082	Z2-012 E	6.0884
920763	Z2-076 E	1.21142
920773	Z2-077 E	1.21142
921122	AA1-059 C	1.986428
921123	AA1-059 E	0.785332
921142	AA1-061 C	3.722252
921143	AA1-061 E	1.833348
921592	AA1-140 C	4.603396
921593	AA1-140 E	7.510804
921602	AA1-141 C	2.839797
921603	AA1-141 E	4.633353
921872	AA2-069	390.5464
922213	AA2-129 E	9.8316
922222	AA2-130	0.92392
922752	AB1-056 C OP	41.896708
922753	AB1-056 E OP	119.314538
922762	AB1-057 C	42.547278
922763	AB1-057 E	121.266248
923282	AB1-137 C	8.77814
923283	AB1-137 E	3.76206
923902	AB2-030 E	1.964
923931	AB2-033 C	3.5352
923932	AB2-033 E	1.3748
924361	AB2-084 C	1.79379
924362	AB2-084 E	2.92671
924461	AB2-095 C	6.456276
924462	AB2-095 E	10.533924
924681	AB2-120 C	18.8594

	<i>OP</i>	
924682	<i>AB2-120 E OP</i>	30.7706
924781	<i>AB2-130 C OP</i>	19.84664
924782	<i>AB2-130 E OP</i>	32.38136
924831	<i>AB2-136 C OP</i>	7.56772
924832	<i>AB2-136 E OP</i>	10.74128
925091	<i>AB2-166 C</i>	0.95074
925092	<i>AB2-166 E</i>	1.663795
925101	<i>AB2-167 C</i>	2.625991
925102	<i>AB2-167 E</i>	4.310589
925151	<i>AB2-172 C OP</i>	5.1262
925152	<i>AB2-172 E OP</i>	8.3638
925231	<i>AB2-177 C</i>	1.245525
925232	<i>AB2-177 E</i>	2.042661
925261	<i>AB2-180 C</i>	6.17848
925262	<i>AB2-180 E</i>	2.64792