PJM Generator Interconnection Request Queue AB2-145 Axton 765 kV Feasibility Study Report

Preface

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

General

The Interconnection Customer (IC) proposes to install PJM Project #AB2-145, a 572.0 MW (572.0 MW Capacity) 1x1 Combined Cycle natural gas generating facility connecting to the American Electric Power (AEP) Transmission system at two (2) alternative points located in Pittsylvania County, Virginia. The primary point of interconnection is located at the Axton 765 kV yard of the Axton substation. The secondary point of interconnection is located at the 138 kV yard of the Axton substation.

AB2-145 has the potential to affect City of Danville facilities therefore PJM will have to coordinate studies of Danville facilities.

The requested Backfeed date is January 1, 2020. The requested in service date is January 1, 2021.

Attachment Facilities

Primary Point of Interconnection (Axton Substation 765 kV Yard)

To accommodate the interconnection at the Axton Substation 765 kV Yard, the substation will have to be expanded requiring the installation of two (2) new 765 kV circuit breakers, extending the 765 kV Bus #1 and installing a new 765 kV Bus #2. Installation of associated protection and control equipment, SCADA, and 765 kV revenue metering will also be required.

Direct Connection to the Axton Substation 765 kV Yard Work and Cost:

- Expand the substation, install two (2) new 765 kV circuit breakers, extend the 765 kV Bus #1, and install a new 765 kV Bus #2. Installation of associated protection and control equipment, SCADA, and 765 kV revenue metering will also be required.
- Estimated Station Cost: \$12,000,000
- Note: Protection and Control Engineering may require that we install a circuit breaker on the Jackson's Ferry 765 kV Line, engineering will determine that in later studies.

Protection and Relay Work and Cost:

- Install line protection and controls at the Axton Substation 765 kV Yard.
- Estimated Cost: \$1,000,000

Secondary Point of Interconnection (Axton Substation 138 kV Yard)

To accommodate the interconnection at the Axton Substation 138 kV Yard, the substation will have to be expanded requiring the installation of two (2) new 138 kV circuit breakers. Installation of associated protection and control equipment, SCADA, and 138 kV revenue metering will also be required.

Direct Connection to the Axton Substation 138 kV Yard Work and Cost:

 Expand the substation, install two (2) new 138 kV circuit breakers. Installation of associated protection and control equipment, SCADA, and 138 kV revenue metering will also be required.

Protection and Relay Work and Cost:

Install line protection and controls at the Axton Substation 138 kV Yard.

It is understood that The Interconnection Customer is responsible for all costs associated with this interconnection. The costs above are reimbursable to AEP. The cost of IC's generating plant and the costs for the line connecting the generating plant to IC's switching station are not included in this report; these are assumed to be IC's responsibility.

The Generation Interconnection Agreement does not in or by itself establish a requirement for American Electric Power to provide power for consumption at the developer's facilities. A separate agreement may be reached with the local utility that provides service in the area to ensure that infrastructure is in place to meet this demand and proper metering equipment is installed. It is the responsibility of the developer to contact the local service provider to determine if a local service agreement is required.

Local and Network Impacts for the Primary Point of Interconnection

The impact of the proposed generating facility on the AEP System was assessed for adherence with applicable reliability criteria. AEP planning criteria require that the transmission system meet performance parameters prescribed in the AEP FERC Form 715¹ and Connection Requirements for AEP Transmission System². Therefore, these criteria were used to assess the impact of the proposed facility on the AEP System. The Queue Project AB2-145 was evaluated as a 572.0 MW (Capacity 572.0 MW) injection at the Axton 765kV substation in the AEP area. Project AB2-145 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AB2-145 was studied with a commercial probability of 53%.

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Potential network impacts were as follows:

Summer Peak Analysis – 2020 for Primary Point of Interconnection

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

1. (AEP - AEP) The 05MOUNTN-05BELMON 765 kV line (from bus 242516 to bus 242920 ckt 1) loads from 102.7% to 103.83% (**DC power flow**) of its normal rating (4047 MVA) for the single line contingency outage of '707_B2_TOR8315_B'. This project contributes approximately 101.48 MW to the thermal violation.

CONTINGENCY '707_B2_TOR8315_B'

OPEN BRANCH FROM BUS 924330 TO BUS 242928 CKT 1 / 924330

AB2-080 TAP 242928 05MARYSV 765 1

END

■ The Mountaineer 765 kV Wavetrap is limiting this line.

Please refer to Appendix 1 for a table containing the generators having contribution to this flowgate.

Short Circuit

(Summary of impacted circuit breakers)

None

Stability Analysis

To be determined in the System Impact Study

Voltage Variations

None

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

None

Local and Network Impacts for the Secondary Point of Interconnection

The impact of the proposed generating facility on the AEP System was assessed for adherence with applicable reliability criteria. AEP planning criteria require that the transmission system meet performance parameters prescribed in the AEP FERC Form 715³ and Connection Requirements for AEP Transmission System⁴. Therefore, these criteria were used to assess the impact of the proposed facility on the AEP System. The Queue Project AB2-145 was evaluated as a 572.0 MW (Capacity 572.0 MW) injection at the Axton 138 kV substation in the AEP area. Project AB2-145 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AB2-145 was studied with a commercial probability of 53%.

Potential network impacts were as follows:

<u>Summer Peak Analysis – 2020 for Secondary Point of Interconnection</u>

Generator Deliverability (Single or N-1 contingencies for the Capacity portion only of the interconnection) None

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Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Oueue)

None

Short Circuit

(Summary of impacted circuit breakers)

None

Stability Analysis

To be determined in the System Impact Study

Voltage Variations

None

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Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

None

Additional Limitations of Concern

None

Local/Network Upgrades

- 1. Replace the Mountaineer 765 kV Wavetrap.
 - Estimated Cost to replace the Mountaineer 765 kV Wavetrap: \$582,945

Schedule

It is anticipated that the time between receipt of executed agreements and Commercial Operation may range from 12 to 18 months if no line work is required. If line work is required, construction time would be between 24 to 36 months after signing an interconnection agreement.

Conclusion

Based upon the results of this Feasibility Study, the construction of the 572.0 MW (572.0 MW Capacity) 1x1 combined cycle natural gas generating facility of The Interconnection Customer (PJM Project #AB2-145) will require the following additional interconnection charges. This plan of service will interconnect the proposed natural gas generating facility in a manner that will provide operational reliability and flexibility to both the AEP system and the Interconnection Customer's natural gas generating facility.

Cost Breakdown for the Primary Point of Interconnection (Axton Substation 765 kV Yard):

Estimated Cost to connect to the Axton Substation 765 kV Yard: \$12,000,000

Estimated Protection and Relay Cost: \$1,000,000 Estimated Local/Network Upgrades Cost: \$582,945

Total Estimated Cost for Project AB2-085: \$13,582,945

The estimates are preliminary in nature, as they were determined without the benefit of detailed engineering studies. Final estimates will require an on-site review and coordination to determine final construction requirements.

Additional Interconnection Customer Responsibilities:

- 1. An Interconnection Customer entering the New Services Queue on or after October 1, 2012 with a proposed new Customer Facility that has a Maximum Facility Output equal to or greater than 100 MW shall install and maintain, at its expense, phasor measurement units (PMUs). See Section 8.5.3 of Appendix 2 to the Interconnection Service Agreement as well as section 4.3 of PJM Manual 14D for additional information.
- 2. The Interconnection Customer may be required to install and/or pay for metering as necessary to properly track real time output of the facility as well as installing metering which shall be used for billing purposes. See Section 8 of Appendix 2 to the Interconnection Service Agreement as well as Section 4 of PJM Manual 14D for additional information.
- 3. The Interconnection Customer seeking to interconnect a wind generation facility shall maintain meteorological data facilities as well as provide that meteorological data which is required per item 5.iv. of Schedule H to the Interconnection Service Agreement.

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(AEP - AEP) The 05MOUNTN-05BELMON 765 kV line (from bus 242516 to bus 242920 ckt 1) loads from 102.7% to 103.83% (**DC power flow**) of its normal rating (4047 MVA) for the single line contingency outage of '707_B2_TOR8315_B'. This project contributes approximately 101.48 MW to the thermal violation.

Note to TOs: AEP Rate A should be applied to this overload

CONTINGENCY '707_B2_TOR8315_B'
OPEN BRANCH FROM BUS 924330 TO BUS 242928 CKT 1
AB2-080 TAP 242928 05MARYSV 765 1
END

/ 924330

Bus Number	Bus Name	Full Contribution
242891	05AMG1	44.7
242892	05AMG2	40.21
242893	05AMG3	72.64
246859	05CER G2	3.54
246861	05CER G3	3.54
246862	05CER G4	3.54
246864	05CER G5	3.54
246865	05CER G6	3.54
247216	05FLATG1	11.14
247217	05FLATG2	11.15
247218	05FLATG3	11.14
247219	05FLATG4	11.14
247220	05FLATG5	11.16
247224	05FTHLG1	8.29
247225	05FTHLG2	8.29
243186	05GVG1	88.02
243187	05GVG2	90.42
247245	05HRKG1A	8.38
247246	05HRKG1B	8.38
247247	05HRKG1S	12.43
247248	05HRKG2A	8.38
247249	05HRKG2B	8.38
247250	05HRKG2S	12.43
242894	05MTG1	91.97
247230	05RIVRG1	8.18
247231	05RIVRG2	8.18
247232	05RIVRG3	8.18
244873	05WINFIELD	0.87
242903	CIR_Y3-38_39	7.4
247609	W3-128	137.55
247615	Y1-006 C	1.71

LTF	Y2-006	29.25
920422	Y2-045	0.29
247623	Y3-036	2.4
247624	Y3-037	2.01
LTF	Z1-046	31.4
920742	Z2-042 C	3.3
LTF	Z2-067	17.05
LTF	AA1-001	8.71
LTF	AA1-004	27.77
920902	AA1-013	2.4
922272	AA2-137	10.81
922282	AA2-138	10.81
LTF	AB1-023	14.62
922772	AB1-058	3.74
923112	AB1-109	12.8
923632	AB1-180 C	0.46
LTF	AB2-005	18.62
923761	AB2-010 C	0.48
923771	AB2-011 C	0.48
LTF	AB2-075	5.74
LTF	AB2-076	7.04
924331	AB2-080 OP	409.13
924911	AB2-145 OP	101.48
924921	AB2-146 OP	60.33