

***Generation Interconnection
Feasibility Study Report***

For

***PJM Generation Interconnection Request
Queue Position AC1-034***

***Anaconda – Vaugh 115kV
42.75 MW Capacity / 75 MW Energy***

Revised May / 2017

Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

Preface

The intent of the Feasibility Study is to determine a plan, with high level estimated cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the IC. The IC may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the IC may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the Impact Study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by ITO, the costs may be included in the study.

General

The IC has proposed a solar generating facility located in Edgecombe County, NC. The installed facilities will have a total capability of 75 MW with 42.75 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is 12/31/2018. **This study does not imply an ITO commitment to this in-service date.**

Point of Interconnection

AC1-034 will interconnect with the ITO transmission system at one of the following points of interconnection:

Option 1 will connect via a new three breaker ring bus switching station that connects at the Anaconda – Vaugh 115kV line #55.

Option 2 will connect via a new three breaker ring bus switching station that connects at the Edgecombe NUG – Tarboro 230kV line.

Cost Summary

The AC1-034 project will be responsible for the following costs:

Description	Total Cost
Attachment Facilities	\$1,200,000
Direct Connection Network Upgrades	\$5,500,000
Non Direct Connection Network Upgrades	\$ 900,000
Total Costs	\$7,600,000

In addition, the AC1-034 project may be responsible for a contribution to the following costs:

Description	Total Cost
New System Upgrades	\$17,000,000
Previously Identified Upgrades	\$ 15,000
Total Costs	\$17,015,000

Cost allocations for these upgrades will be provided in the System Impact Study Report.

Note: PJM Open Access Transmission Tariff (OATT) section 217.3A outline cost allocation rules. The rules are further clarified in PJM Manual 14A Attachment B. For New System Upgrades, the cost allocation rule differ depending on whether the minimum amount of upgrades to resolve a single reliability criteria violation will cost less than \$5,000,000. For upgrades estimated to cost less than \$5,000,000 the allocation of costs will not occur outside of the Queue in which the need for the Network Upgrade was identified. Cost allocation within the Queue will be contingent each Queue projects Distribution Factor on the overloaded facility. For upgrades estimated to cost \$5,000,000 or greater the allocation of costs will start with the first Queue project to cause the need for the upgrade. Later queue projects will receive cost allocation contingent on their contribution to the violation and are allocated to the queues that have not closed less than 5 years following the execution of the first Interconnection Service Agreement which identifies the need for this upgrade.

Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost \$600,000.

Transmission: Construct approximately one span of 115 kV Attachment line between the generation substation and the proposed AC1-034 site. The estimated cost for this work is \$1,200,000.

The estimated total cost of the Attachment Facilities is \$1,800,000. It is estimated to take 18-24 months to complete. These costs do not include CIAC Tax Gross-up. The single line is shown below in Attachment 1.

Direct Connection Cost Estimate

Substation: Build a new three breaker 115 kV Switching Station and associated facilities on Line #55 between Anaconda and Tar River Substation. The estimated cost of this work scope is \$5,500,000. It is estimated to take 24-36 months to complete this work.

Non-Direct Connection Cost Estimate

Transmission: Re-arrange Line #55 to interconnect with the new 115 kV AC1-034 Switching Station. The estimated cost of this work is \$900,000 dollars.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

New System Reinforcement

Reinforcement: Uprate / Rebuild Line #2141 Carolina – Lakeview 230 kV. Uprate/rebuild approximately 1.4 miles of 230 kV Line to increase the line rating by 15% to 360 MVA. It is estimated to take 18-20 months timeframe to permit and construct and it is estimated to cost \$3,500,000 to resolve this deficiency.

Reinforcement: Rebuild the AB2-100 TAP-Clubhouse 230kV line. Rebuild the AB2-100 TAP-Clubhouse 230kV line to increase its line rating to a minimum of 460 MVA. It is estimated to take 24-28 months to permit and construct a Virginia CPCN will most likely be required for this rebuild and it is estimated to cost \$13,500,000 to resolve this deficiency.

Contribution to Previously Identified Overloads

Reinforcement: Battleboro – Rocky Mt 115kV: Replace Battleboro substation terminal equipment. Estimated cost is \$15,000.

Note: Duke/Progress Energy portion of this line will need to be studied under Duke's FERC tariff process.

Interconnection Customer Requirements

ITO's Facility Connection Requirements as posted on PJM's website

<http://www.pjm.com/~media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx>

Voltage Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for voltages and times as specified for the Eastern Interconnection in Attachment 1 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low voltage conditions, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Frequency Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for frequencies and times as specified in Attachment 2 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low frequency condition, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Reactive Power - The Generation Interconnection Customer shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading to 0.95 lagging measured at the generator's terminals.

Revenue Metering and SCADA Requirements

PJM Requirements

The IC will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

Option One

Network Impacts

The Queue Project AC1-034 was evaluated as a 75.0 MW (Capacity 42.8 MW) injection tapping the Anaconda-Tarboro 115kV line in the ITO area. Project AC1-034 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AC1-034 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
246T2034_A	CONTINGENCY '246T2034_A' /* EARLEYS OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1 /* 246 AA1-138 TAP OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1 /* 2034 OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1 /* 2034 OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1 /* TROWBRIDGE TX #1&2 END
LN 2012	CONTINGENCY 'LN 2012' OPEN BRANCH FROM BUS 314266 TO BUS 314569 CKT 1 /* 6NORTHAMPTON230.00 - 6EARLEYS 230.00 OPEN BRANCH FROM BUS 314266 TO BUS 314599 CKT 1 /* 6NORTHAMPTON230.00 - 6ROA VAL 230.00 OPEN BUS 314266 /* ISLAND END
LN 2058-2181	CONTINGENCY 'LN 2058-2181' OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00 OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA- RMOUNT#4230.00 - 6NASH 230.00 OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY 230.00 - 6NASH 230.00 OPEN BUS 314591 /* ISLAND: 6NASH 230.00 OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /* 6ROCKYMT230T230.00 - 6HATHAWAY 230.00 END

Contingency Name	Description
LN 2131A	CONTINGENCY 'LN 2131A' OPEN BRANCH FROM BUS 314662 TO BUS 916040 CKT 1 /* 6S HERTFORD 230.00 - Z1-036 TAP 230.00 OPEN BRANCH FROM BUS 314651 TO BUS 314662 CKT 1 /* 6WINFALL 230.00 - 6S HERTFORD 230.00 OPEN BUS 314662 /* ISLAND END
LN 238	CONTINGENCY 'LN 238' OPEN BRANCH FROM BUS 314282 TO BUS 314435 CKT 1 /* 6CARSON 230.00 - 6SAPONY 230.00 OPEN BRANCH FROM BUS 314435 TO BUS 314563 CKT 1 /* 6SAPONY 230.00 - 6CLUBHSE 230.00 OPEN BRANCH FROM BUS 314562 TO BUS 314563 CKT 1 /* 3CLUBHSE 115.00 - 6CLUBHSE 230.00 OPEN BUS 314435 /* ISLAND END
LN 254_A	CONTINGENCY 'LN 254_A' OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1 /* 6CLUBHSE 230.00 - AB2-100 TAP 230.00 END
LN 563	CONTINGENCY 'LN 563' OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /* 8CARSON 500.00 - 8MDLTHAN 500.00 END

Summer Peak Analysis - 2020

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

Contingency			Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
#	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
1	N-1	LN 254_A	DVP - DVP	6LAKEVIEW-6CAROLNA 230 kV line	314583	314561	1	DC	95.34	96.79	ER	375	5.43	1
2	N-1	LN 238	DVP - DVP	6LAKEVIEW-6CAROLNA 230 kV line	314583	314561	1	DC	94.53	95.91	ER	375	5.16	
3	N-1	LN 2012	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	96.97	98.56	ER	375	5.94	

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

Contingency			Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
#	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
4	LFFB	246T2034_A	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	98.14	101.14	LD	459	13.79	2

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

Contingency			Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
#	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
5	DCTL	LN 2058-2181	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	133.51	141.55	ER	164	13.19	3

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study.

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study.

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
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Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
# 1 – 2	6LAKEVEW-6CAROLNA 230 kV line	Uprate/rebuild approximately 1.4 miles of 230 kV Line to increase the line rating by 15% to 360 MVA. Time: 18 - 20 months	Pending	\$3,500,000
# 3 – 4	AB2-100 TAP-6CLUBHSE 230 kV line	Rebuild the AB2-100 TAP-Clubhouse 230kV line. Time: 44 - 48 months.	Pending	\$13,500,000
Total New Network Upgrades				\$17,000,000

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost
# 5	3BTLEBRO-3ROCKYMT115T 115 kV line	Upgrade Battleboro terminal equipment	Pending	\$15,000
Total New Network Upgrades				

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
	Type	Name			From	To	Circuit		Initial	Final	Type	MVA	
6	N-1	LN 563	DVP - DVP	6CHSTF B-6BASIN 230 kV line	314287	314276	1	DC	140.68	141.14	ER	449	4.64
7	N-1	LN 2131A	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	314569	314575	1	DC	99.55	102.02	ER	572	14.1
8	N-1	LN 2131A	DVP - DVP	6NUCO TP-AA1-138 TAP 230 kV line	314575	921571	1	DC	92.74	95.21	ER	572	14.1
9	N-1	LN 238	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	111.96	114.38	ER	375	9.06
10	N-1	LN 2131A	DVP - DVP	AA1-138 TAP-6SUFFOLK 230 kV line	921571	314537	1	DC	102.76	105.23	ER	572	14.1
11	N-1	LN 2012	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	113.98	116.76	ER	375	10.43
12	Non	Non	DVP - DVP	AC1-034 TAP-3TARRTP 115 kV line	925590	314548	1	DC	4.76	114.32	NR	63	75

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

ITO Analysis

ITO assessed the impact of the proposed Queue Project #AC1-034 interconnection of a 75 MW Energy (42.75 MW Capacity) injection into the ITO's Transmission System, for compliance with NERC Reliability Criteria on ITO's Transmission System. The system was assessed using the summer 2020 RTEP case provided to ITO by PJM. When performing a generation analysis, ITO's main analysis will be load flow study results under single contingency (both normal and stressed system conditions). ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under normal and stressed system conditions. A full listing of ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C Contingency Conditions (Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO's Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating.

As part of its generation impact analysis, the ITO routinely evaluates the impact that a proposed new generation resource will have under maximum generation conditions, stress system conditions and import/export system conditions (greater than 20 MW). The results of these studies are discussed in more detail below.

Category B Analysis (Single Contingency):

1. System Normal – No deficiencies identified
2. Critical System Condition (No Surry 230 kV Unit) – No deficiencies identified.

Category C Analysis: (Multiple Facility Analysis)

1. Bus Fault - No deficiencies identified
2. Line Stuck Breaker - No deficiencies identified
3. Tower Line – No deficiencies identified

Import/Export Analysis (Single Contingency) are tabulated in Table A and B below.

Table A: Import Study Results

Import Study Results			
Area	Summer 2020	Summer 2020 with AC1-034	Limiting Element
AEP	2000+	2000+	None
APS	2000+	2000+	None

CPL	2000+	2000+	None
PJM	2000+	2000+	None

Table B: Export Study Results

Export Study Results			
Area	Summer 2020	Summer 2020 with AC1-034	Limiting Element
AEP	2000+	2000+	None
APS	2000+	2000+	None
CPL	2000+	2000+	None
PJM	2000+	2000+	None

ITO's Planning Criteria indicates a need to have approximately 2000 MW of import and export capability. ITO will evaluate the impact of AC1-034 on transfer capability as part of the System Impact Study.

Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

Option Two

Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost \$600,000.

Transmission: Construct approximately one mile of 230 kV Attachment line between the generation substation and the proposed AC1-034 site. The estimated cost for this work is \$1,500,000.

The estimated total cost of the Attachment Facilities is \$2,100,000. It is estimated to take 22-26 months to complete this work.

Network Upgrades

Substation: Build a new three breaker 230 kV Switching Station and associated facilities on Line #229 between Hathaway and Edgecombe Substation. The estimated cost of this work scope is \$6,500,000.

Transmission: Re-arrange Line #229 to interconnect with the new 115 kV AC1-034 Switching Station. The estimated cost of this work is \$1,100,000 dollars.

The total estimated cost to complete the Direct Connection Network Facilities is \$7,600,000. It is estimated to take 30-40 months to complete this work.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

Note: System Reinforcements to resolved criteria violations are not developed for secondary points of interconnection.

Network Impacts

The Queue Project AC1-034 was evaluated as a 75.0 MW (Capacity 42.8 MW) injection at the Hathaway 230kV substation in the DVP area. Project AC1-034 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AC1-034 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
246T2034_A	CONTINGENCY '246T2034_A' /* EARLEYS OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1 /* 246 OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1 /* 246 AA1-138 TAP OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1 /* 246 - NUCOR OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1 /* 2034 OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1 /* 2034 OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1 /* TROWBRIDGE TX #1&2 END
DVP_P7-1: LN 229-2058	CONTINGENCY 'DVP_P7-1: LN 229-2058' OPEN BRANCH FROM BUS 314564 TO BUS 314610 CKT 1 /* 6EDGECOM 230.00 - 6TOTDP4 230.00 OPEN BRANCH FROM BUS 314608 TO BUS 314609 CKT 1 /* 3TARBORO 115.00 - 6TARBORO 230.00 OPEN BRANCH FROM BUS 314609 TO BUS 314610 CKT 1 /* 6TARBORO 230.00 - 6TOTDP4 230.00 OPEN BUS 314610 /* ISLAND: 6TOTDP4 230.00 OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /* 6ROCKYMT230T230.00 - 6HATHAWAY 230.00 END
LN 2012	CONTINGENCY 'LN 2012' OPEN BRANCH FROM BUS 314266 TO BUS 314569 CKT 1 /* 6NORTHAMPTON230.00 - 6EARLEYS 230.00 OPEN BRANCH FROM BUS 314266 TO BUS 314599 CKT 1 /* 6NORTHAMPTON230.00 - 6ROA VAL 230.00 OPEN BUS 314266 /* ISLAND END

Contingency Name	Description
LN 2058-2181	CONTINGENCY 'LN 2058-2181' OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00 OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA- RMOUNT#4230.00 - 6NASH 230.00 OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY 230.00 - 6NASH 230.00 OPEN BUS 314591 /* ISLAND: 6NASH 230.00 OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /* 6ROCKYMT230T230.00 - 6HATHAWAY 230.00 END
LN 2131A	CONTINGENCY 'LN 2131A' OPEN BRANCH FROM BUS 314662 TO BUS 916040 CKT 1 /* 6S HERTFORD 230.00 - Z1-036 TAP 230.00 OPEN BRANCH FROM BUS 314651 TO BUS 314662 CKT 1 /* 6WINFALL 230.00 - 6S HERTFORD 230.00 OPEN BUS 314662 /* ISLAND END
LN 2141	CONTINGENCY 'LN 2141' OPEN BRANCH FROM BUS 314561 TO BUS 314583 CKT 1 /* 6CAROLNA 230.00 - 6LAKEVIEW 230.00 END
LN 238	CONTINGENCY 'LN 238' OPEN BRANCH FROM BUS 314282 TO BUS 314435 CKT 1 /* 6CARSON 230.00 - 6SAPONY 230.00 OPEN BRANCH FROM BUS 314435 TO BUS 314563 CKT 1 /* 6SAPONY 230.00 - 6CLUBHSE 230.00 OPEN BRANCH FROM BUS 314562 TO BUS 314563 CKT 1 /* 3CLUBHSE 115.00 - 6CLUBHSE 230.00 OPEN BUS 314435 /* ISLAND END
LN 254_A	CONTINGENCY 'LN 254_A' OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1 /* 6CLUBHSE 230.00 - AB2-100 TAP 230.00 END

Contingency Name	Description
LN 54-2012_B	<p>CONTINGENCY 'LN 54-2012_B'</p> <p>OPEN BRANCH FROM BUS 921751 TO BUS 314581 CKT 1 /* AA2-053</p> <p>TAP 115.00 - 3JACKSON 115.00</p> <p>OPEN BRANCH FROM BUS 314568 TO BUS 314625 CKT 1 /* 3EARLEYS</p> <p>115.00 - 3AULANDR 115.00</p> <p>OPEN BRANCH FROM BUS 314581 TO BUS 314626 CKT 1 /* 3JACKSON</p> <p>115.00 - 3WOODLND 115.00</p> <p>OPEN BRANCH FROM BUS 314625 TO BUS 314626 CKT 1 /* 3AULANDR</p> <p>115.00 - 3WOODLND 115.00</p> <p>OPEN BUS 314581 /* ISLAND</p> <p>OPEN BUS 314625 /* ISLAND</p> <p>OPEN BUS 314626 /* ISLAND</p> <p>OPEN BRANCH FROM BUS 314266 TO BUS 314569 CKT 1 /*</p> <p>6NORTHAMPTON230.00 - 6EARLEYS 230.00</p> <p>OPEN BRANCH FROM BUS 314266 TO BUS 314599 CKT 1 /*</p> <p>6NORTHAMPTON230.00 - 6ROA VAL 230.00</p> <p>OPEN BUS 314266 /* ISLAND</p> <p>END</p>
LN 56-2012_A	<p>CONTINGENCY 'LN 56-2012_A'</p> <p>OPEN BRANCH FROM BUS 314259 TO BUS 314559 CKT Z1 /* 3CAR56_1</p> <p>115.00 - 3CAROLNA 115.00</p> <p>OPEN BRANCH FROM BUS 314259 TO BUS 921161 CKT 1 /* 3CAR56_1</p> <p>115.00 - AA1-063A TAP 115.00</p> <p>OPEN BRANCH FROM BUS 314558 TO BUS 314587 CKT 1 /* 3BOYKINS</p> <p>115.00 - 3MARGTSV 115.00</p> <p>OPEN BRANCH FROM BUS 314587 TO BUS 314604 CKT 1 /* 3MARGTSV</p> <p>115.00 - 3SEABORD 115.00</p> <p>OPEN BUS 314259 /* ISLAND</p> <p>OPEN BUS 314587 /* ISLAND</p> <p>OPEN BUS 314604 /* ISLAND</p> <p>OPEN BRANCH FROM BUS 314266 TO BUS 314569 CKT 1 /*</p> <p>6NORTHAMPTON230.00 - 6EARLEYS 230.00</p> <p>OPEN BRANCH FROM BUS 314266 TO BUS 314599 CKT 1 /*</p> <p>6NORTHAMPTON230.00 - 6ROA VAL 230.00</p> <p>OPEN BUS 314266 /* ISLAND</p> <p>END</p>
LN 563	<p>CONTINGENCY 'LN 563'</p> <p>OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /* 8CARSON</p> <p>500.00 - 8MDLTHAN 500.00</p> <p>END</p>

Summer Peak Analysis - 2020

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
1	N-1	LN 254_A	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	95.49	97.62	ER	375	7.97	4
2	N-1	LN 238	DVP - DVP	6LAKEVEW-6CAROLNA 230 kV line	314583	314561	1	DC	94.65	96.7	ER	375	7.69	
3	N-1	LN 2012	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	78.62	80.53	ER	375	7.15	
4	N-1	LN 2012	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	97.08	98.99	ER	375	7.15	
5	N-1	LN 2141	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	86.4	88.64	ER	375	8.39	

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
6	LFFB	246T2034_A	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	89.99	92.29	LD	637	14.68	5
7	DCTL	LN 54-2012_B	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	88.97	90.99	LD	637	12.82	

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
8	DCTL	LN 56-2012_A	DVP - DVP	6CLUBHSE-6SAPONY 230 kV line	314563	314435	1	DC	87.61	89.68	LD	637	13.21	
9	LFFB	246T2034_A	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	77.64	80.73	LD	459	14.19	6
10	DCTL	LN 54-2012_B	DVP - DVP	6LAKEVEW-AB2-100 TAP 230 kV line	314583	924510	1	DC	74.98	77.72	LD	459	12.61	
11	DCTL	DVP_P7-1: LN 229-2058	DVP - CPLE	6NASH-6PA-RMOUNT#4 230 kV line	314591	304226	1	DC	75.48	84.54	ER	470	42.55	7
12	LFFB	246T2034_A	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	98.23	101.32	LD	459	14.19	8
13	DCTL	LN 54-2012_B	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	96.39	99.13	LD	459	12.61	
14	DCTL	LN 56-2012_A	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	93.57	96.36	LD	459	12.85	

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Contributions to previously identified circuit breakers found to be over-duty:

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

Contingency			Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
#	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
15	DCTL	LN 2058-2181	DVP - CPLE	3BTLEBRO-3ROCKYMT115T 115 kV line	314554	304223	1	DC	133.28	143.9	ER	164	17.43	9

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies)

To be determined during Impact Study.

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

To be determined during Impact Study.

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

Contingency			Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution
#	Type	Name			From	To	Circuit		Initial	Final	Type	MVA	

Contingency			Affected Area	Facility Description	Bus		Circuit	Power Flow	Loading %		Rating		MW Contribution
#	Type	Name			From	To			Initial	Final	Type	MVA	
16	N-1	LN 563	DVP - DVP	6CHSTF B-6BASIN 230 kV line	314287	314276	1	DC	139.81	140.27	ER	449	4.65
17	N-1	LN 2131A	DVP - DVP	6EARLEYS-6NUCO TP 230 kV line	314569	314575	1	DC	99.84	100.75	ER	572	11.52
18	N-1	LN 2131A	DVP - DVP	6NUCO TP-AA1-138 TAP 230 kV line	314575	921571	1	DC	93.03	93.94	ER	572	11.52
19	N-1	LN 254_A	DVP - DVP	6LAKEVIEW-6CAROLNA 230 kV line	314583	314561	1	DC	113.29	117.02	ER	375	13.99
20	N-1	LN 2131A	DVP - DVP	AA1-138 TAP-6SUFFOLK 230 kV line	921571	314537	1	DC	103.07	103.98	ER	572	11.52
21	N-1	LN 2012	DVP - DVP	AB2-100 TAP-6CLUBHSE 230 kV line	924510	314563	1	DC	114.46	117.81	ER	375	12.55

Light Load Analysis

Light Load Studies to be conducted during later study phases (as required by PJM Manual 14B).

ITO Analysis

ITO assessed the impact of the proposed Queue Project #AC1-034 interconnection of a 75 MW Energy (42.8 MW Capacity) injection into the ITO's Transmission System at the new Hathaway 230 kV Substation, for compliance with NERC Reliability Criteria on ITO's Transmission System. The system was assessed using the summer 2019 RTEP case provided to ITO by PJM. When performing a generation analysis, ITO's main analysis will be load flow study results under single contingency (both normal and stressed system conditions). ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under normal and stressed system conditions. A full listing of ITO's Planning Criteria and interconnection requirements can be found in the ITO's Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C

Contingency Conditions (Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO's Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating.

As part of its generation impact analysis, the ITO routinely evaluates the impact that a proposed new generation resource will have under maximum generation conditions, stress system conditions and import/export system conditions (greater than 20 MW). The results of these studies are discussed in more detail below.

Category B Analysis (Single Contingency):

System Normal – See PJM Study Results

Critical System Condition (No Surry 230 kV Unit) – No deficiencies identified.

Category C Analysis: (Multiple Facility Analysis)

Bus Fault - No deficiencies identified

Line Stuck Breaker - No deficiencies identified

Tower Line – See PJM Study Results

Import/Export Analysis (Single Contingency)

ITO's Planning Criteria indicates a need to have approximately 2000 MW of import and export capability. ITO will evaluate the impact of AC1-034 on transfer capability as part of the System Impact Study.

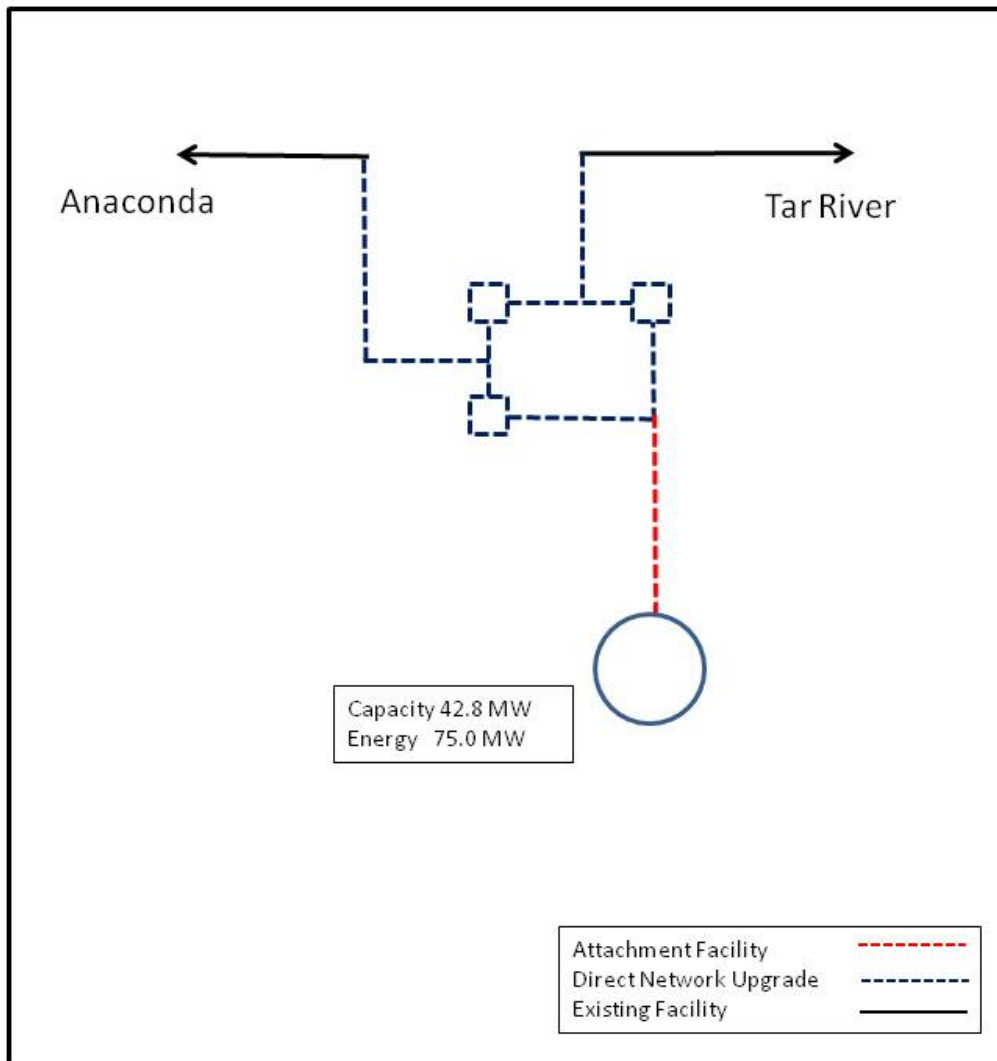
Affected System Analysis & Mitigation

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

Attachment 1
System Configuration

AC1 - 034



Flowgate Appendices

Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gauge other generators impact. When a flowgate is identified in multiple analysis the appendix is presented for only the analysis with the greatest overload.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(DVP - DVP) The 6LAKEVEW-6CAROLNA 230 kV line (from bus 314583 to bus 314561 ckt 1) loads from 95.34% to 96.79% (**DC power flow**) of its emergency rating (375 MVA) for the single line contingency outage of 'LN 254_A'. This project contributes approximately 5.43 MW to the thermal violation.

CONTINGENCY 'LN 254_A'

OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1 /* 6CLUBHSE

230.00 - AB2-100 TAP 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.04
315132	1EDGECEMB	2.04
315139	1GASTONA	12.93
315141	1GASTONB	12.93
315136	1ROSEMG1	8.46
315138	1ROSEMG2	3.96
315137	1ROSEMS1	5.25
917341	Z2-044 C	0.14
917511	Z2-088 C OP1	0.41
918411	AA1-050	0.34
922722	AB1-053 C	3.63
922922	AB1-081 C OP	8.07
923262	AB1-132 C OP	52.26
923941	AB2-035 C	0.27
924151	AB2-059 C OP	9.51
924391	AB2-088 C	0.34
924511	AB2-100 C	41.68
924761	AB2-128 C	35.71
925591	AC1-034 C OP	5.43
926071	AC1-086 C	76.96
927141	AC1-208 C	20.86

Appendix 2

(DVP - DVP) The AB2-100 TAP-6CLUBHSE 230 kV line (from bus 924510 to bus 314563 ckt 1) loads from 98.14% to 101.14% (**DC power flow**) of its load dump rating (459 MVA) for the line fault with failed breaker contingency outage of '246T2034_A'. This project contributes approximately 13.79 MW to the thermal violation.

CONTINGENCY '246T2034_A'

/* EARLEYS

OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1

/* 246

OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1

/* 246 AA1-138

TAP

OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1

/* 246 - NUCOR

OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1

/* TROWBRIDGE

TX #1&2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.07
315132	1EDGECEMB	2.07
315139	1GASTONA	7.99
315141	1GASTONB	7.99
315126	1ROARAP2	1.71
315128	1ROARAP4	1.64
315134	1ROAVALA	11.09
315135	1ROAVALB	2.96
315136	1ROSEMG1	5.36
315138	1ROSEMG2	2.51
315137	1ROSEMS1	3.33
900671	V4-068 C	0.1
900672	V4-068 E	0.28
917331	Z2-043 C	0.56
917332	Z2-043 E	1.27
917341	Z2-044 C	0.29
917342	Z2-044 E	0.65
917511	Z2-088 C OP1	1.03
917512	Z2-088 E OP1	8.87
917591	Z2-099 C	0.14
917592	Z2-099 E	0.33

918411	AA1-050	0.87
LTF	AA1-058	0.53
921162	AA1-063AC	8.21
921163	AA1-063AE	3.87
918511	AA1-065 C OP	2.47
918512	AA1-065 E OP	6.44
921182	AA1-067 C	1.83
921183	AA1-067 E	0.78
918561	AA1-072 C	0.08
918562	AA1-072 E	0.21
921562	AA1-135 C	11.7
921563	AA1-135 E	5.01
921752	AA2-053 C	10.03
921753	AA2-053 E	4.31
921762	AA2-057 C	8.1
921763	AA2-057 E	4.05
921862	AA2-068 C	2.57
921863	AA2-068 E	1.18
LTF	AA2-074	2.29
920021	AA2-086 C	0.08
920022	AA2-086 E	0.18
921982	AA2-088 C	4.76
921983	AA2-088 E	7.76
922442	AA2-165 C	1.1
922443	AA2-165 E	0.53
922472	AA2-169 C	1.51
922473	AA2-169 E	0.69
922512	AA2-174 C	0.46
922513	AA2-174 E	0.5
922722	AB1-053 C	2.3
922723	AB1-053 E	1.29
922732	AB1-054 C	5.17
922733	AB1-054 E	2.54
922922	AB1-081 C OP	10.09
922923	AB1-081 E OP	4.32
923262	AB1-132 C OP	32.27
923263	AB1-132 E OP	13.83
923941	AB2-035 C	0.39
923942	AB2-035 E	0.17

924151	AB2-059 C OP	11.89
924152	AB2-059 E OP	6.12
924381	AB2-087 C	0.76
924382	AB2-087 E	0.36
924391	AB2-088 C	0.5
924392	AB2-088 E	0.24
924491	AB2-098 C	0.61
924492	AB2-098 E	0.26
924501	AB2-099 C	0.72
924502	AB2-099 E	0.31
924511	AB2-100 C	35.63
924512	AB2-100 E	17.55
924761	AB2-128 C	30.53
924762	AB2-128 E	12.02
925121	AB2-169 C OP	4.42
925122	AB2-169 E OP	3.96
925141	AB2-171 C OP	2.77
925142	AB2-171 E OP	4.52
925591	AC1-034 C OP	7.86
925592	AC1-034 E OP	5.93
926071	AC1-086 C	47.52
926072	AC1-086 E	21.63
926201	AC1-098 C	7.29
926202	AC1-098 E	4.35
926211	AC1-099 C	2.44
926212	AC1-099 E	1.44
926771	AC1-163 C	2.6
926772	AC1-163 E	1.22
927021	AC1-189 C	9.42
927022	AC1-189 E	4.69
927051	AC1-193 C	2.03
927052	AC1-193 E	3.32
927141	AC1-208 C	15.19
927142	AC1-208 E	6.75

Appendix 3

(DVP - CPLE) The 3BTLEBRO-3ROCKYMT115T 115 kV line (from bus 314554 to bus 304223 ckt 1) loads from 133.51% to 141.55% (**DC power flow**) of its emergency rating (164 MVA) for the tower line contingency outage of 'LN 2058-2181'. This project contributes approximately 13.19 MW to the thermal violation.

CONTINGENCY 'LN 2058-2181'

OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00

OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-
RMOUNT#4230.00 - 6NASH 230.00

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY
230.00 - 6NASH 230.00

OPEN BUS 314591 /* ISLAND: 6NASH 230.00

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*
6ROCKYMT230T230.00 - 6HATHAWAY 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.54
315132	1EDGECEMB	2.54
315139	1GASTONA	2.41
315141	1GASTONB	2.41
315126	1ROARAP2	1.
315128	1ROARAP4	0.96
315134	1ROAVALA	3.42
315135	1ROAVALB	0.91
315136	1ROSEMG1	1.96
315138	1ROSEMG2	0.92
315137	1ROSEMS1	1.21
900672	V4-068 E	0.15
917331	Z2-043 C	0.36
917332	Z2-043 E	0.83
917341	Z2-044 C	0.55
917342	Z2-044 E	1.25
917511	Z2-088 C OP1	0.71
917512	Z2-088 E OP1	6.1
917592	Z2-099 E	0.2
918411	AA1-050	0.59
LTF	AA1-055	9.47

921162	AA1-063AC	4.88
921163	AA1-063AE	2.3
918512	AA1-065 E OP	1.96
921182	AA1-067 C	0.73
921183	AA1-067 E	0.31
918561	AA1-072 C	0.05
918562	AA1-072 E	0.14
921562	AA1-135 C	4.03
921563	AA1-135 E	1.73
921752	AA2-053 C	5.42
921753	AA2-053 E	2.33
921762	AA2-057 C	12.88
921763	AA2-057 E	6.44
921862	AA2-068 C	3.3
921863	AA2-068 E	1.52
920022	AA2-086 E	0.11
921982	AA2-088 C	2.94
921983	AA2-088 E	4.8
922442	AA2-165 C	1.76
922443	AA2-165 E	0.85
922512	AA2-174 C	0.25
922513	AA2-174 E	0.27
922722	AB1-053 C	0.84
922723	AB1-053 E	0.47
922732	AB1-054 C	3.16
922733	AB1-054 E	1.55
922922	AB1-081 C OP	20.07
922923	AB1-081 E OP	8.6
923262	AB1-132 C OP	9.76
923263	AB1-132 E OP	4.18
923572	AB1-173 C OP	1.21
923573	AB1-173 E OP	0.57
923582	AB1-173AC OP	1.21
923583	AB1-173AE OP	0.57
923911	AB2-031 C OP	1.2
923912	AB2-031 E OP	0.59
923941	AB2-035 C	0.37
923942	AB2-035 E	0.16
923991	AB2-040 C OP	3.95

923992	<i>AB2-040 E OP</i>	3.23
924151	<i>AB2-059 C OP</i>	23.66
924152	<i>AB2-059 E OP</i>	12.19
924381	<i>AB2-087 C</i>	0.31
924382	<i>AB2-087 E</i>	0.15
924391	<i>AB2-088 C</i>	0.47
924392	<i>AB2-088 E</i>	0.23
924491	<i>AB2-098 C</i>	0.24
924492	<i>AB2-098 E</i>	0.1
924501	<i>AB2-099 C</i>	0.32
924502	<i>AB2-099 E</i>	0.14
924511	<i>AB2-100 C</i>	6.41
924512	<i>AB2-100 E</i>	3.16
924761	<i>AB2-128 C</i>	5.49
924762	<i>AB2-128 E</i>	2.16
924931	<i>AB2-147 C</i>	1.14
924932	<i>AB2-147 E</i>	1.86
924951	<i>AB2-150 C OP</i>	1.14
924952	<i>AB2-150 E OP</i>	1.86
925141	<i>AB2-171 C OP</i>	1.93
925142	<i>AB2-171 E OP</i>	3.14
925171	<i>AB2-174 C OP</i>	3.57
925172	<i>AB2-174 E OP</i>	3.23
925591	<i>AC1-034 C OP</i>	7.52
925592	<i>AC1-034 E OP</i>	5.67
926071	<i>AC1-086 C</i>	14.37
926072	<i>AC1-086 E</i>	6.54
926201	<i>AC1-098 C</i>	8.
926202	<i>AC1-098 E</i>	4.76
926211	<i>AC1-099 C</i>	2.68
926212	<i>AC1-099 E</i>	1.57
926771	<i>AC1-163 C</i>	1.14
926772	<i>AC1-163 E</i>	0.53
927021	<i>AC1-189 C</i>	5.15
927022	<i>AC1-189 E</i>	2.56
927051	<i>AC1-193 C</i>	1.41
927052	<i>AC1-193 E</i>	2.31
927111	<i>AC1-206 C OP</i>	5.11
927112	<i>AC1-206 E OP</i>	2.42

<i>927141</i>	<i>ACI-208 C</i>	<i>10.06</i>
<i>927142</i>	<i>ACI-208 E</i>	<i>4.47</i>

Appendix 4

(DVP - DVP) The 6LAKEVEW-6CAROLNA 230 kV line (from bus 314583 to bus 314561 ckt 1) loads from 95.49% to 97.62% (**DC power flow**) of its emergency rating (375 MVA) for the single line contingency outage of 'LN 254_A'. This project contributes approximately 7.97 MW to the thermal violation.

CONTINGENCY 'LN 254_A'

OPEN BRANCH FROM BUS 314563 TO BUS 924510 CKT 1 /* 6CLUBHSE
230.00 - AB2-100 TAP 230.00
END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.07
315132	1EDGECEMB	2.07
315139	1GASTONA	13.11
315141	1GASTONB	13.11
315136	1ROSEMG1	8.58
315138	1ROSEMG2	4.02
315137	1ROSEMS1	5.32
917341	Z2-044 C	0.14
917511	Z2-088 C OP1	0.41
918411	AA1-050	0.35
922722	AB1-053 C	3.63
922922	AB1-081 C OP	8.07
923262	AB1-132 C OP	52.26
923941	AB2-035 C	0.27
924151	AB2-059 C OP	9.51
924391	AB2-088 C	0.34
924511	AB2-100 C	41.68
924761	AB2-128 C	35.71
925591	AC1-034 C OP	7.97
926071	AC1-086 C	76.96
927141	AC1-208 C	3.51

Appendix 5

(DVP - DVP) The 6CLUBHSE-6SAPONY 230 kV line (from bus 314563 to bus 314435 ckt 1) loads from 89.99% to 92.29% (**DC power flow**) of its load dump rating (637 MVA) for the line fault with failed breaker contingency outage of '246T2034_A'. This project contributes approximately 14.68 MW to the thermal violation.

CONTINGENCY '246T2034_A'

/* EARLEYS

OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1

/* 246

OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1

/* 246 AA1-138

TAP

OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1

/* 246 - NUCOR

OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1

/* TROWBRIDGE

TX #1&2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315132	1EDGECEMB	2.17
315139	1GASTONA	7.78
315141	1GASTONB	7.78
315126	1ROARAP2	2.81
315128	1ROARAP4	2.71
315134	1ROAVALA	11.06
315135	1ROAVALB	2.95
315136	1ROSEMG1	5.25
315138	1ROSEMG2	2.46
315137	1ROSEMS1	3.26
314704	3LAWRENC	0.82
314541	3WATKINS	0.52
900671	V4-068 C	0.13
900672	V4-068 E	0.36
917331	Z2-043 C	0.66
917332	Z2-043 E	1.49
917341	Z2-044 C	0.33
917342	Z2-044 E	0.74
917512	Z2-088 E OPI	9.27
917592	Z2-099 E	0.48
LTF	AA1-058	0.57
921162	AA1-063AC	12.86
921163	AA1-063AE	6.07

918511	AA1-065 C OP	2.64
918512	AA1-065 E OP	6.78
921182	AA1-067 C	1.92
921183	AA1-067 E	0.82
918561	AA1-072 C	0.1
918562	AA1-072 E	0.25
921562	AA1-135 C	12.3
921563	AA1-135 E	5.27
921752	AA2-053 C	14.95
921753	AA2-053 E	6.42
921762	AA2-057 C	9.81
921763	AA2-057 E	4.91
921862	AA2-068 C	3.27
921863	AA2-068 E	1.5
LTF	AA2-074	2.64
920022	AA2-086 E	0.26
921982	AA2-088 C	6.85
921983	AA2-088 E	11.18
922442	AA2-165 C	1.34
922443	AA2-165 E	0.65
922472	AA2-169 C	2.96
922473	AA2-169 E	1.36
922512	AA2-174 C	0.68
922513	AA2-174 E	0.74
922722	AB1-053 C	2.22
922723	AB1-053 E	1.25
922732	AB1-054 C	7.44
922733	AB1-054 E	3.66
922922	AB1-081 C OP	10.86
922923	AB1-081 E OP	4.65
923262	AB1-132 C OP	31.01
923263	AB1-132 E OP	13.29
923572	AB1-173 C OP	5.12
923573	AB1-173 E OP	2.39
923582	AB1-173AC OP	5.12
923583	AB1-173AE OP	2.39
923911	AB2-031 C OP	5.09
923912	AB2-031 E OP	2.51
923941	AB2-035 C	0.4
923942	AB2-035 E	0.17
923991	AB2-040 C OP	16.7
923992	AB2-040 E OP	13.66
924021	AB2-043 C OP	2.78
924022	AB2-043 E OP	4.57
924151	AB2-059 C OP	12.79

924152	AB2-059 E OP	6.59
924301	AB2-077 C OP	1.74
924302	AB2-077 E OP	1.16
924311	AB2-078 C OP	1.74
924312	AB2-078 E OP	1.16
924321	AB2-079 C OP	1.74
924322	AB2-079 E OP	1.16
924381	AB2-087 C	0.86
924382	AB2-087 E	0.4
924391	AB2-088 C	0.52
924392	AB2-088 E	0.25
924401	AB2-089 C	2.43
924402	AB2-089 E	1.25
924411	AB2-090 C	3.51
924412	AB2-090 E	1.8
924491	AB2-098 C	0.64
924492	AB2-098 E	0.27
924501	AB2-099 C	0.84
924502	AB2-099 E	0.36
924511	AB2-100 C	31.41
924512	AB2-100 E	15.47
924761	AB2-128 C	26.91
924762	AB2-128 E	10.59
924931	AB2-147 C	6.65
924932	AB2-147 E	10.85
924951	AB2-150 C OP	6.65
924952	AB2-150 E OP	10.85
925141	AB2-171 C OP	4.01
925142	AB2-171 E OP	6.54
925171	AB2-174 C OP	16.93
925172	AB2-174 E OP	15.32
925221	AB2-176 C	1.44
925222	AB2-176 E	0.62
925591	AC1-034 C OP	8.37
925592	AC1-034 E OP	6.31
925781	AC1-054 C OP	8.89
925782	AC1-054 E OP	4.1
926071	AC1-086 C	45.67
926072	AC1-086 E	20.78
926201	AC1-098 C	9.07
926202	AC1-098 E	5.4
926211	AC1-099 C	3.04
926212	AC1-099 E	1.78
926281	AC1-106	2.31
926771	AC1-163 C	3.03

926772	<i>ACI-163 E</i>	<i>1.42</i>
927021	<i>ACI-189 C</i>	<i>9.86</i>
927022	<i>ACI-189 E</i>	<i>4.91</i>
927051	<i>ACI-193 C</i>	<i>2.94</i>
927052	<i>ACI-193 E</i>	<i>4.79</i>
927111	<i>ACI-206 C OP</i>	<i>30.25</i>
927112	<i>ACI-206 E OP</i>	<i>14.3</i>
927141	<i>ACI-208 C</i>	<i>11.9</i>
927142	<i>ACI-208 E</i>	<i>5.29</i>
927211	<i>ACI-215 C</i>	<i>9.17</i>
927212	<i>ACI-215 E</i>	<i>4.16</i>

Appendix 6

(DVP - DVP) The 6LAKEVIEW-AB2-100 TAP 230 kV line (from bus 314583 to bus 924510 ckt 1) loads from 77.64% to 80.73% (**DC power flow**) of its load dump rating (459 MVA) for the line fault with failed breaker contingency outage of '246T2034_A'. This project contributes approximately 14.19 MW to the thermal violation.

CONTINGENCY '246T2034_A'

/* EARLEYS

OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1

/* 246

OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1

/* 246 AA1-138

TAP

OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1

/* 246 - NUCOR

OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1

/* TROWBRIDGE

TX #1&2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.1
315132	1EDGECEMB	2.1
315139	1GASTONA	8.1
315141	1GASTONB	8.1
315126	1ROARAP2	1.73
315128	1ROARAP4	1.67
315134	1ROAVALA	11.25
315135	1ROAVALB	3.
315136	1ROSEMG1	5.44
315138	1ROSEMG2	2.55
315137	1ROSEMS1	3.37
314784	1WEYRHSB	1.17
900671	V4-068 C	0.1
900672	V4-068 E	0.28
917331	Z2-043 C	0.57
917332	Z2-043 E	1.27
917341	Z2-044 C	0.29
917342	Z2-044 E	0.65
917511	Z2-088 C OP1	1.04
917512	Z2-088 E OP1	8.87
917591	Z2-099 C	0.15
917592	Z2-099 E	0.33
918411	AA1-050	0.88

<i>LTF</i>	<i>AA1-058</i>	<i>0.53</i>
<i>921162</i>	<i>AA1-063AC</i>	<i>8.21</i>
<i>921163</i>	<i>AA1-063AE</i>	<i>3.87</i>
<i>918511</i>	<i>AA1-065 C OP</i>	<i>2.5</i>
<i>918512</i>	<i>AA1-065 E OP</i>	<i>6.44</i>
<i>921182</i>	<i>AA1-067 C</i>	<i>1.83</i>
<i>921183</i>	<i>AA1-067 E</i>	<i>0.78</i>
<i>918561</i>	<i>AA1-072 C</i>	<i>0.09</i>
<i>918562</i>	<i>AA1-072 E</i>	<i>0.21</i>
<i>921562</i>	<i>AA1-135 C</i>	<i>11.69</i>
<i>921563</i>	<i>AA1-135 E</i>	<i>5.01</i>
<i>921752</i>	<i>AA2-053 C</i>	<i>10.03</i>
<i>921753</i>	<i>AA2-053 E</i>	<i>4.31</i>
<i>921762</i>	<i>AA2-057 C</i>	<i>8.1</i>
<i>921763</i>	<i>AA2-057 E</i>	<i>4.05</i>
<i>921862</i>	<i>AA2-068 C</i>	<i>2.57</i>
<i>921863</i>	<i>AA2-068 E</i>	<i>1.18</i>
<i>LTF</i>	<i>AA2-074</i>	<i>2.29</i>
<i>920021</i>	<i>AA2-086 C</i>	<i>0.08</i>
<i>920022</i>	<i>AA2-086 E</i>	<i>0.18</i>
<i>921982</i>	<i>AA2-088 C</i>	<i>4.76</i>
<i>921983</i>	<i>AA2-088 E</i>	<i>7.76</i>
<i>922442</i>	<i>AA2-165 C</i>	<i>1.1</i>
<i>922443</i>	<i>AA2-165 E</i>	<i>0.53</i>
<i>922472</i>	<i>AA2-169 C</i>	<i>1.51</i>
<i>922473</i>	<i>AA2-169 E</i>	<i>0.69</i>
<i>922512</i>	<i>AA2-174 C</i>	<i>0.46</i>
<i>922513</i>	<i>AA2-174 E</i>	<i>0.5</i>
<i>922722</i>	<i>AB1-053 C</i>	<i>2.3</i>
<i>922723</i>	<i>AB1-053 E</i>	<i>1.29</i>
<i>922732</i>	<i>AB1-054 C</i>	<i>5.16</i>
<i>922733</i>	<i>AB1-054 E</i>	<i>2.54</i>
<i>922922</i>	<i>AB1-081 C OP</i>	<i>10.09</i>
<i>922923</i>	<i>AB1-081 E OP</i>	<i>4.32</i>
<i>923262</i>	<i>AB1-132 C OP</i>	<i>32.27</i>
<i>923263</i>	<i>AB1-132 E OP</i>	<i>13.83</i>
<i>923941</i>	<i>AB2-035 C</i>	<i>0.39</i>
<i>923942</i>	<i>AB2-035 E</i>	<i>0.17</i>
<i>924151</i>	<i>AB2-059 C OP</i>	<i>11.89</i>
<i>924152</i>	<i>AB2-059 E OP</i>	<i>6.12</i>
<i>924381</i>	<i>AB2-087 C</i>	<i>0.76</i>
<i>924382</i>	<i>AB2-087 E</i>	<i>0.36</i>
<i>924391</i>	<i>AB2-088 C</i>	<i>0.5</i>
<i>924392</i>	<i>AB2-088 E</i>	<i>0.24</i>
<i>924491</i>	<i>AB2-098 C</i>	<i>0.61</i>

924492	<i>AB2-098 E</i>	<i>0.26</i>
924501	<i>AB2-099 C</i>	<i>0.72</i>
924502	<i>AB2-099 E</i>	<i>0.31</i>
925121	<i>AB2-169 C OP</i>	<i>4.41</i>
925122	<i>AB2-169 E OP</i>	<i>3.96</i>
925141	<i>AB2-171 C OP</i>	<i>2.77</i>
925142	<i>AB2-171 E OP</i>	<i>4.52</i>
925591	<i>AC1-034 C OP</i>	<i>8.09</i>
925592	<i>AC1-034 E OP</i>	<i>6.1</i>
925781	<i>AC1-054 C OP</i>	<i>4.25</i>
925782	<i>AC1-054 E OP</i>	<i>1.96</i>
926071	<i>AC1-086 C</i>	<i>47.52</i>
926072	<i>AC1-086 E</i>	<i>21.63</i>
926201	<i>AC1-098 C</i>	<i>7.29</i>
926202	<i>AC1-098 E</i>	<i>4.34</i>
926211	<i>AC1-099 C</i>	<i>2.44</i>
926212	<i>AC1-099 E</i>	<i>1.44</i>
926771	<i>AC1-163 C</i>	<i>2.6</i>
926772	<i>AC1-163 E</i>	<i>1.22</i>
927021	<i>AC1-189 C</i>	<i>9.42</i>
927022	<i>AC1-189 E</i>	<i>4.69</i>
927051	<i>AC1-193 C</i>	<i>2.03</i>
927052	<i>AC1-193 E</i>	<i>3.32</i>
927141	<i>AC1-208 C</i>	<i>10.1</i>
927142	<i>AC1-208 E</i>	<i>4.48</i>

Appendix 7

(DVP - CPLE) The 6NASH-6PA-RMOUNT#4 230 kV line (from bus 314591 to bus 304226 ckt 1) loads from 75.48% to 84.54% (**DC power flow**) of its emergency rating (470 MVA) for the tower line contingency outage of 'DVP_P7-1: LN 229-2058'. This project contributes approximately 42.55 MW to the thermal violation.

CONTINGENCY 'DVP_P7-1: LN 229-2058'

OPEN BRANCH FROM BUS 314564 TO BUS 314610 CKT 1 /* 6EDGECOM
230.00 - 6TOTDP4 230.00

OPEN BRANCH FROM BUS 314608 TO BUS 314609 CKT 1 /* 3TARBORO
115.00 - 6TARBORO 230.00

OPEN BRANCH FROM BUS 314609 TO BUS 314610 CKT 1 /* 6TARBORO
230.00 - 6TOTDP4 230.00

OPEN BUS 314610 /* ISLAND: 6TOTDP4 230.00

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*
6ROCKYMT230T230.00 - 6HATHAWAY 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	6.3
315132	1EDGECEMB	6.3
315139	1GASTONA	4.77
315141	1GASTONB	4.77
315126	1ROARAP2	1.5
315128	1ROARAP4	1.44
315134	1ROAVALA	6.4
315135	1ROAVALB	1.71
315136	1ROSEMG1	4.09
315138	1ROSEMG2	1.91
315137	1ROSEMS1	2.53
314541	3WATKINS	0.35
900672	V4-068 E	0.19
917331	Z2-043 C	0.37
917332	Z2-043 E	0.83
917341	Z2-044 C	0.45
917342	Z2-044 E	1.
917591	Z2-099 C	0.12
917592	Z2-099 E	0.28
921162	AA1-063AC	7.
921163	AA1-063AE	3.3
918561	AA1-072 C	0.06

918562	AA1-072 E	0.14
921752	AA2-053 C	7.58
921753	AA2-053 E	3.26
921762	AA2-057 C	10.9
921763	AA2-057 E	5.45
921862	AA2-068 C	2.98
921863	AA2-068 E	1.37
920021	AA2-086 C	0.06
920022	AA2-086 E	0.15
921982	AA2-088 C	3.97
921983	AA2-088 E	6.48
922442	AA2-165 C	1.49
922443	AA2-165 E	0.72
922472	AA2-169 C	1.29
922473	AA2-169 E	0.59
922512	AA2-174 C	0.35
922513	AA2-174 E	0.38
922722	AB1-053 C	1.73
922723	AB1-053 E	0.97
922732	AB1-054 C	4.27
922733	AB1-054 E	2.1
922922	AB1-081 C OP	20.11
922923	AB1-081 E OP	8.62
923262	AB1-132 C OP	19.03
923263	AB1-132 E OP	8.15
923572	AB1-173 C OP	1.93
923573	AB1-173 E OP	0.9
923582	AB1-173AC OP	1.93
923583	AB1-173AE OP	0.9
923911	AB2-031 C OP	1.91
923912	AB2-031 E OP	0.94
923991	AB2-040 C OP	6.29
923992	AB2-040 E OP	5.14
924151	AB2-059 C OP	23.7
924152	AB2-059 E OP	12.21
924381	AB2-087 C	0.35
924382	AB2-087 E	0.17
924501	AB2-099 C	0.36
924502	AB2-099 E	0.16
924511	AB2-100 C	12.29
924512	AB2-100 E	6.05
924761	AB2-128 C	10.53
924762	AB2-128 E	4.14
924931	AB2-147 C	1.96
924932	AB2-147 E	3.21

924951	AB2-150 C OP	1.96
924952	AB2-150 E OP	3.21
925141	AB2-171 C OP	2.59
925142	AB2-171 E OP	4.23
925171	AB2-174 C OP	5.83
925172	AB2-174 E OP	5.28
925591	AC1-034 C OP	24.25
925592	AC1-034 E OP	18.3
926071	AC1-086 C	28.02
926072	AC1-086 E	12.75
926201	AC1-098 C	7.37
926202	AC1-098 E	4.39
926211	AC1-099 C	2.47
926212	AC1-099 E	1.45
926771	AC1-163 C	1.31
926772	AC1-163 E	0.61
927051	AC1-193 C	1.9
927052	AC1-193 E	3.1
927111	AC1-206 C OP	8.94
927112	AC1-206 E OP	4.22
927141	AC1-208 C	14.58
927142	AC1-208 E	6.47

Appendix 8

(DVP - DVP) The AB2-100 TAP-6CLUBHSE 230 kV line (from bus 924510 to bus 314563 ckt 1) loads from 98.23% to 101.32% (**DC power flow**) of its load dump rating (459 MVA) for the line fault with failed breaker contingency outage of '246T2034_A'. This project contributes approximately 14.19 MW to the thermal violation.

CONTINGENCY '246T2034_A'

/* EARLEYS

OPEN BRANCH FROM BUS 314569 TO BUS 314575 CKT 1

/* 246

OPEN BRANCH FROM BUS 314575 TO BUS 921571 CKT 1

/* 246 AA1-138

TAP

OPEN BRANCH FROM BUS 314575 TO BUS 314590 CKT 1

/* 246 - NUCOR

OPEN BRANCH FROM BUS 314569 TO BUS 314620 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314620 TO BUS 314616 CKT 1

/* 2034

OPEN BRANCH FROM BUS 314616 TO BUS 314613 CKT 1

/* TROWBRIDGE

TX #1&2

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.1
315132	1EDGECEMB	2.1
315139	1GASTONA	8.1
315141	1GASTONB	8.1
315126	1ROARAP2	1.73
315128	1ROARAP4	1.67
315134	1ROAVALA	11.25
315135	1ROAVALB	3.
315136	1ROSEMG1	5.44
315138	1ROSEMG2	2.55
315137	1ROSEMS1	3.37
900671	V4-068 C	0.1
900672	V4-068 E	0.28
917331	Z2-043 C	0.57
917332	Z2-043 E	1.27
917341	Z2-044 C	0.29
917342	Z2-044 E	0.65
917511	Z2-088 C OPI	1.04
917512	Z2-088 E OPI	8.87
917591	Z2-099 C	0.15
917592	Z2-099 E	0.33
918411	AA1-050	0.88
LTF	AA1-058	0.53

921162	AA1-063AC	8.21
921163	AA1-063AE	3.87
918511	AA1-065 C OP	2.5
918512	AA1-065 E OP	6.44
921182	AA1-067 C	1.83
921183	AA1-067 E	0.78
918561	AA1-072 C	0.09
918562	AA1-072 E	0.21
921562	AA1-135 C	11.69
921563	AA1-135 E	5.01
921752	AA2-053 C	10.03
921753	AA2-053 E	4.31
921762	AA2-057 C	8.1
921763	AA2-057 E	4.05
921862	AA2-068 C	2.57
921863	AA2-068 E	1.18
LTF	AA2-074	2.29
920021	AA2-086 C	0.08
920022	AA2-086 E	0.18
921982	AA2-088 C	4.76
921983	AA2-088 E	7.76
922442	AA2-165 C	1.1
922443	AA2-165 E	0.53
922472	AA2-169 C	1.51
922473	AA2-169 E	0.69
922512	AA2-174 C	0.46
922513	AA2-174 E	0.5
922722	AB1-053 C	2.3
922723	AB1-053 E	1.29
922732	AB1-054 C	5.16
922733	AB1-054 E	2.54
922922	AB1-081 C OP	10.09
922923	AB1-081 E OP	4.32
923262	AB1-132 C OP	32.27
923263	AB1-132 E OP	13.83
923941	AB2-035 C	0.39
923942	AB2-035 E	0.17
924151	AB2-059 C OP	11.89
924152	AB2-059 E OP	6.12
924381	AB2-087 C	0.76
924382	AB2-087 E	0.36
924391	AB2-088 C	0.5
924392	AB2-088 E	0.24
924491	AB2-098 C	0.61
924492	AB2-098 E	0.26

924501	AB2-099 C	0.72
924502	AB2-099 E	0.31
924511	AB2-100 C	35.63
924512	AB2-100 E	17.55
924761	AB2-128 C	30.53
924762	AB2-128 E	12.02
925121	AB2-169 C OP	4.41
925122	AB2-169 E OP	3.96
925141	AB2-171 C OP	2.77
925142	AB2-171 E OP	4.52
925591	AC1-034 C OP	8.09
925592	AC1-034 E OP	6.1
925781	AC1-054 C OP	4.25
925782	AC1-054 E OP	1.96
926071	AC1-086 C	47.52
926072	AC1-086 E	21.63
926201	AC1-098 C	7.29
926202	AC1-098 E	4.34
926211	AC1-099 C	2.44
926212	AC1-099 E	1.44
926771	AC1-163 C	2.6
926772	AC1-163 E	1.22
927021	AC1-189 C	9.42
927022	AC1-189 E	4.69
927051	AC1-193 C	2.03
927052	AC1-193 E	3.32
927141	AC1-208 C	10.1
927142	AC1-208 E	4.48

Appendix 9

(DVP - CPLE) The 3BTLEBRO-3ROCKYMT115T 115 kV line (from bus 314554 to bus 304223 ckt 1) loads from 133.28% to 143.9% (**DC power flow**) of its emergency rating (164 MVA) for the tower line contingency outage of 'LN 2058-2181'. This project contributes approximately 17.43 MW to the thermal violation.

CONTINGENCY 'LN 2058-2181'

OPEN BUS 304226 /* ISLAND: 6PA-RMOUNT#4115.00

OPEN BRANCH FROM BUS 304226 TO BUS 314591 CKT 1 /* 6PA-
RMOUNT#4230.00 - 6NASH 230.00

OPEN BRANCH FROM BUS 313845 TO BUS 314591 CKT 1 /* 6HATHAWAY
230.00 - 6NASH 230.00

OPEN BUS 314591 /* ISLAND: 6NASH 230.00

OPEN BRANCH FROM BUS 304222 TO BUS 313845 CKT 1 /*
6ROCKYMT230T230.00 - 6HATHAWAY 230.00

END

<i>Bus Number</i>	<i>Bus Name</i>	<i>Full Contribution</i>
315131	1EDGECEMA	2.58
315132	1EDGECEMB	2.58
315139	1GASTONA	2.45
315141	1GASTONB	2.45
315126	1ROARAP2	1.02
315128	1ROARAP4	0.98
315134	1ROAVALA	3.46
315135	1ROAVALB	0.92
315136	1ROSEMG1	1.98
315138	1ROSEMG2	0.93
315137	1ROSEMS1	1.23
900672	V4-068 E	0.15
917331	Z2-043 C	0.37
917332	Z2-043 E	0.83
917341	Z2-044 C	0.56
917342	Z2-044 E	1.25
917511	Z2-088 C OP1	0.72
917512	Z2-088 E OP1	6.1
917592	Z2-099 E	0.2
918411	AA1-050	0.6
LTF	AA1-055	9.46
921162	AA1-063AC	4.88
921163	AA1-063AE	2.3

918512	AA1-065 E OP	1.96
921182	AA1-067 C	0.73
921183	AA1-067 E	0.31
918561	AA1-072 C	0.06
918562	AA1-072 E	0.14
921562	AA1-135 C	4.03
921563	AA1-135 E	1.73
921752	AA2-053 C	5.42
921753	AA2-053 E	2.33
921762	AA2-057 C	12.88
921763	AA2-057 E	6.44
921862	AA2-068 C	3.3
921863	AA2-068 E	1.52
920022	AA2-086 E	0.11
921982	AA2-088 C	2.94
921983	AA2-088 E	4.8
922442	AA2-165 C	1.76
922443	AA2-165 E	0.85
922512	AA2-174 C	0.25
922513	AA2-174 E	0.27
922722	AB1-053 C	0.84
922723	AB1-053 E	0.47
922732	AB1-054 C	3.16
922733	AB1-054 E	1.55
922922	AB1-081 C OP	20.07
922923	AB1-081 E OP	8.6
923262	AB1-132 C OP	9.76
923263	AB1-132 E OP	4.18
923572	AB1-173 C OP	1.21
923573	AB1-173 E OP	0.57
923582	AB1-173AC OP	1.21
923583	AB1-173AE OP	0.57
923911	AB2-031 C OP	1.2
923912	AB2-031 E OP	0.59
923941	AB2-035 C	0.37
923942	AB2-035 E	0.16
923991	AB2-040 C OP	3.95
923992	AB2-040 E OP	3.23
924151	AB2-059 C OP	23.66
924152	AB2-059 E OP	12.19
924381	AB2-087 C	0.31
924382	AB2-087 E	0.15
924391	AB2-088 C	0.47
924392	AB2-088 E	0.23
924491	AB2-098 C	0.24

924492	AB2-098 E	0.1
924501	AB2-099 C	0.32
924502	AB2-099 E	0.14
924511	AB2-100 C	6.41
924512	AB2-100 E	3.16
924761	AB2-128 C	5.49
924762	AB2-128 E	2.16
924931	AB2-147 C	1.14
924932	AB2-147 E	1.86
924951	AB2-150 C OP	1.14
924952	AB2-150 E OP	1.86
925141	AB2-171 C OP	1.93
925142	AB2-171 E OP	3.14
925171	AB2-174 C OP	3.57
925172	AB2-174 E OP	3.23
925591	AC1-034 C OP	9.93
925592	AC1-034 E OP	7.49
926071	AC1-086 C	14.37
926072	AC1-086 E	6.54
926201	AC1-098 C	8.
926202	AC1-098 E	4.76
926211	AC1-099 C	2.68
926212	AC1-099 E	1.57
926771	AC1-163 C	1.14
926772	AC1-163 E	0.53
927021	AC1-189 C	5.15
927022	AC1-189 E	2.57
927051	AC1-193 C	1.41
927052	AC1-193 E	2.31
927111	AC1-206 C OP	5.19
927112	AC1-206 E OP	2.46
927141	AC1-208 C	17.73
927142	AC1-208 E	7.87