Generation Interconnection Feasibility Study Report

For

PJM Generation Interconnection Request Queue Position AC2-080 Olive – Reynolds (NIPSCO) 345 kV

Preface

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

General

The Interconnection Customer (IC) proposes to install PJM Project #AC2-080, a 200.0 MW (26.0 MW Capacity) wind generating facility in Pulaski County, Indiana (see Figure 2). The generating facility will consist of 58 Vestas V136 machines. The primary point of interconnection will be to AEP's Olive – Reynolds (NIPSCO) 345 kV circuit #1 (see Figure 1). The secondary point of interconnection will be to AEP's Reynolds (NIPSCO) – Meadow Lake 345 kV circuit #1 (see Figure 3).

The requested in service date is December 31, 2019.

The objective of this Feasibility Study is to determine budgetary cost estimates and approximate construction timelines for identified transmission facilities required to connect the proposed generating facilities to the AEP transmission system. These reinforcements include the Attachment Facilities, Local Upgrades, and Network Upgrades required maintaining the reliability of the AEP transmission system. Stability analysis is not included as part of this study.

Attachment Facilities

Primary Point of Interconnection (Olive – Reynolds (NIPSCO) 345 kV Circuit #1)

To accommodate the interconnection on the Olive – Reynolds (NIPSCO) 345 kV circuit #1, a new three (3) circuit breaker 345 kV switching station physically configured in a breaker and half bus arrangement but operated as a ring-bus will be constructed (see Figure 1). Installation of associated protection and control equipment, 345 kV line risers, SCADA, and 345 kV revenue metering will also be required. AEP reserves the right to specify the final acceptable configuration considering design practices, future expansion, and compliance requirements.

New Line Tap/Switching Station Work and Cost:

- Construct a new three (3) circuit breaker 345 kV switching station physically configured in a breaker and half bus arrangement but operated as a ring-bus. Installation of associated protection and control equipment, 345 kV line risers, SCADA, and 345 kV revenue metering will also be required (see Figure 1).
 - Estimated Station Cost: \$8,000,000

Direct Connection Cost Estimate

The total preliminary cost estimate for Direct Connection work is given in the following tables below.

For AEP building Direct Connection cost estimates:

Description	Total Cost
Olive – Reynolds (NIPSCO) 345 kV T-Line Cut In	\$2,000,000
Total	\$2,000,000

Table 1

Non-Direct Connection Cost Estimate

The total preliminary cost estimate for Non-Direct Connection work is given in the following table below:

For AEP building Non-Direct Connection cost estimates:

Description	Estimated Cost
345 kV Revenue Metering	\$250,000
Upgrade line protection and controls at the Olive 345 kV substation.	\$300,000
Upgrade line protection and control settings at the Reynolds (NIPSCO) 345 kV substation.	NIPSCO to provide cost estimate
Total	\$550,000

Table 2

Secondary Point of Interconnection (Reynolds (NIPSCO) – Meadow Lake 345 kV Circuit #1)

To accommodate the interconnection on the Reynolds (NIPSCO) – Meadow Lake 345 kV circuit #1, a new three (3) circuit breaker 345 kV switching station physically configured in a breaker and half bus arrangement but operated as a ring-bus will be constructed (see Figure 3). Installation of associated protection and control equipment, 345 kV line risers, SCADA, and 345 kV revenue metering will also be required. AEP reserves the right to specify the final acceptable configuration considering design practices, future expansion, and compliance requirements.

It is understood that IC is responsible for all costs associated with this interconnection. The cost of IC's generating plant and the costs for the line connecting the generating plant to the point of interconnection are not included in this report; these are assumed to be IC's responsibility.

The Generation Interconnection Agreement does not in or by itself establish a requirement for American Electric Power to provide power for consumption at the developer's facilities. A separate agreement may be reached with the local utility that provides service in the area to ensure that infrastructure is in place to meet this demand and proper metering equipment is installed. It is the responsibility of the developer to contact the local service provider to determine if a local service agreement is required.

Interconnection Customer Requirements

Requirement from the PJM Open Access Transmission Tariff:

- 1. An Interconnection Customer entering the New Services Queue on or after October 1, 2012 with a proposed new Customer Facility that has a Maximum Facility Output equal to or greater than 100 MW shall install and maintain, at its expense, phasor measurement units (PMUs). See Section 8.5.3 of Appendix 2 to the Interconnection Service Agreement as well as section 4.3 of PJM Manual 14D for additional information.
- 2. The Interconnection Customer may be required to install and/or pay for metering as necessary to properly track real time output of the facility as well as installing metering which shall be used for billing purposes. See Section 8 of Appendix 2 to the Interconnection Service Agreement as well as Section 4 of PJM Manual 14D for additional information.

Revenue Metering and SCADA Requirements

PJM Requirements

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

AEP Requirements

The Interconnection Customer will be required to comply with all AEP Revenue Metering Requirements for Generation Interconnection Customers. The Revenue Metering Requirements may be found within the "Requirements for Connection of New Facilities or Changes to Existing Facilities Connected to the AEP Transmission System" document located at the following link:

http://www.pjm.com/~/media/planning/plan-standards/private-aep/aep-interconnection-requirements.ashx

Option 1

Network Impacts

The Queue Project AC2-080 was evaluated as a 200.0 MW (Capacity 26.0 MW) injection tapping the Olive – Reynolds 345 kV line in the AEP area. Project AC2-080 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AC2-080 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Base Case Used

Summer Peak Analysis – 2020 Case

Contingency Descriptions

The following contingencies resulted in overloads:

Description	
CONTINGENCY '2978_C2_05DUMONT 765-B_A'	
OPEN BRANCH FROM BUS 243206 TO BUS 920251 CKT 1	/ 243206
05DUMONT 765 920251 X1-020 TAP 765 1	
OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1	/ 243206
05DUMONT 765 270644 WILTON ; 765 1	
END	
	/ WILTO; 765
	/ WILTO;4M 345
	/ WILTO;4M 345
,	/ Y Y TO 12 5 1 5
	/ WILTO;4M 345
· · · · · · · · · · · · · · · · · · ·	
<u> </u>	
	/ WILL TO . 765
	/ WILTO; 765
	/ WILL TO 2M 245
	/ WILTO;3M 345
	/ WILTO;3M 345
	/ WILTO,3WI 343
· · · · · · · · · · · · · · · · · · ·	/ WILTO;3M 345
	/ WILTO,5W 543
	/ 242924 05HANG
	, _ ;_; _ ; , , , , , , , , , , , , , ,
END	
CONTINGENCY '695 B2'	
OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1	/ 243206
05DUMONT 765 270644 WILTO; 765 1	
END	
	OPEN BRANCH FROM BUS 243206 TO BUS 920251 CKT 1 05DUMONT 765 920251 X1-020 TAP 765 1 OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 05DUMONT 765 270644 WILTON; 765 1 END CONTINGENCY '112-65-BT4-5' TRIP BRANCH FROM BUS 270644 TO BUS 243206 CKT 1 05DUMONT 765 TRIP BRANCH FROM BUS 275233 TO BUS 270644 CKT 1 WILTO; 765 TRIP BRANCH FROM BUS 275233 TO BUS 270927 CKT 1 WILTO; R 345 TRIP BRANCH FROM BUS 275233 TO BUS 270927 CKT 1 WILTO; 4C 33 END CONTINGENCY '112-65-BT3-4' TRIP BRANCH FROM BUS 275232 TO BUS 243206 CKT 1 05DUMONT 765 TRIP BRANCH FROM BUS 275232 TO BUS 270644 CKT 1 WILTO; 765 TRIP BRANCH FROM BUS 275232 TO BUS 270926 CKT 1 WILTO; B 345 TRIP BRANCH FROM BUS 275232 TO BUS 270926 CKT 1 WILTO; B 345 TRIP BRANCH FROM BUS 275232 TO BUS 275332 CKT 1 WILTO; 3C 33 END CONTINGENCY '8649_B2_TOR546' OPEN BRANCH FROM BUS 242924 TO BUS 243208 CKT 1 R 765 243208 05JEFRSO 765 1 END CONTINGENCY '695_B2' OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 05DUMONT 765 270644 WILTO; 765 1

Table 3

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

			AC2	2-080 Contribution	n to Previ	ously Iden	tified Over	loads				
	Contingency				Bus		Loading		Rating			
			Affected	Facility					Ty		MW	\mathbf{FG}
#	Type	Name	Area	Description	From	To	Initial	Final	pe	MVA	Con.	App.
		2978_C2_05DU		X2-052 TAP-								
		MONT 765-	AEP -	05DUMONT								
1	LFFB	B_A	AEP	345 kV line	247610	243219	115.32	117.35	ER	1409	42.87	
				X2-052 TAP-								
		112-65-BT4-	AEP -	05DUMONT								
2	LFFB	5	AEP	345 kV line	247610	243219	107.7	109.59	ER	1409	41.90	
				X2-052 TAP-								
		112-65-BT3-	AEP -	05DUMONT								
3	LFFB	4	AEP	345 kV line	247610	243219	107.7	109.58	ER	1409	41.90	

Table 4

Steady-State Voltage Requirements

None

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Affected System Analysis & Mitigation

LGEE Impacts:

LGEE Impacts to be determined during later study phases (as applicable).

MISO Impacts:

MISO Impacts to be determined during later study phases (as applicable).

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

OVEC Impacts:

OVEC Impacts to be determined during later study phases (as applicable).

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request. Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

	AC2-080 Delivery of Energy Portion of Interconnection Request													
	Contingency		A 66 () T		Bus		Loading		Rating		N // N // N	FG		
#	Туре	Name	Area		Affected Area	Facility Description	From	To	Initial	Final	Туре	MVA	MW Con.	App ·
				05SORENS-										
		8649_B2_TOR5	AEP -	AC1-225 TAP										
1	N-1	46	AEP	765 kV line	246999	927280	101.04	101.06	NR	4249	52.83			
				X2-052 TAP-										
			AEP -	05DUMONT										
2	N-1	695_B2	AEP	345 kV line	247610	243219	107.61	109.5	NR	1409	41.90			
		0.640 D2 TO		AC1-225 TAP-										
		8649_B2_TO	AEP -	05MARYSV										
3	N-1	R546	AEP	765 kV line	927280	242928	103.56	103.58	NR	4249	52.83			

Table 5

Previous System Reinforcements

	Overloaded Facility	Upgrade Description	Schedule	Estimated Cost
#1	X2-052 TAP- 05DUMONT 345 kV line	The following work determined during the sag study will be required to resolve the X2-052 Tap – Dumont 345 kV line overload: Replace tower 20 with a custom steel pole and the removal of swing angle brackets on 2 structures (PJM Network Upgrade N4512). New SE rating to be 1868 MVA. This overload is caused by the AB1 Queue.	The standard time required for construction differs from state to state. An approximate construction time would be 24 to 36 months after signing an interconnection agreement.	\$1.0775 Million
			Total New Network Upgrades	\$1.0775 Million

Table 6

Schedule

It is anticipated that the time between receipt of executed agreements and Commercial Operation may range from 12 to 18 months if no line work is required. If line work is required, construction time would be between 24 to 36 months after signing an interconnection agreement.

Note: The time provided between anticipated normal completion of System Impact, Facilities Studies, subsequent execution of ISA and ICSA documents, and the proposed Backfeed Date is shorter than usual and may be difficult to achieve.

Conclusion

Based upon the results of this Feasibility Study, the construction of the 200.0 MW (26.0 MW Capacity) wind generating facility of IC(PJM Project #AC2-080) will require the following additional interconnection charges. This plan of service will interconnect the proposed wind generating facility in a manner that will provide operational reliability and flexibility to both the AEP system and the IC's generating facility.

Cost Breakdown	for Primary Point of Interconnection (Olive – Reynolds (N	IPSCO) 345 kV)
Attachment Cost	New 345 kV Switching Station	\$8,000,000
	345 kV Revenue Metering	\$250,000
	Upgrade line protection and controls at the Olive 345 kV substation.	\$350,000
Non-Direct Connection	Upgrade line protection and control settings at the Reynolds (NIPSCO) 345 kV substation.	NIPSCO to provide cost estimate
Cost Estimate	The following work determined during the sag study will be required to resolve the X2-052 Tap – Dumont 345 kV line overload:	
	Replace tower 20 with a custom steel pole and the removal of swing angle brackets on 2 structures (PJM Network Upgrade N4512). New SE rating to be 1868 MVA. This overload is caused by the AB1 Queue.	\$1,077,500
	Total Estimated Cost for Project AC2-080	\$9,677,500

Table 7

The estimates are preliminary in nature, as they were determined without the benefit of detailed engineering studies. Final estimates will require an on-site review and coordination to determine final construction requirements.

Option 2

Network Impacts

The Queue Project AC2-080 was evaluated as a 200.0 MW (Capacity 26.0 MW) injection tapping the Olive – Meadow 345 kV line in the AEP area. Project AC2-080 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AC2-080 was studied with a commercial probability of 53%. Potential network impacts were as follows:

Base Case Used

Summer Peak Analysis – 2020 Case

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description	
2978_C2_05DUMONT 765-	CONTINGENCY '2978_C2_05DUMONT 765-B_A' OPEN BRANCH FROM BUS 243206 TO BUS 920251 CKT 1 05DUMONT 765 920251 X1-020 TAP 765 1	/ 243206
B_A	OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 05DUMONT 765 270644 WILTON; 765 1 END	/ 243206
	CONTINGENCY '8648_C2_05JEFRSO 765-B1' OPEN BRANCH FROM BUS 243208 TO BUS 243209 CKT 1 05JEFRSO 765 243209 05ROCKPT 765 1	/ 243208
8648_C2_05JEFRSO 765-B1	OPEN BRANCH FROM BUS 243208 TO BUS 242865 CKT 2 05JEFRSO 765 242865 05JEFRSO 345 2	/ 243208
	OPEN BRANCH FROM BUS 242865 TO BUS 248000 CKT Z1 05JEFRSO 345 248000 06CLIFTY 345 Z1 END	/ 242865
	CONTINGENCY '112-65-BT4-5' TRIP BRANCH FROM BUS 270644 TO BUS 243206 CKT 1 05DUMONT 765	/ WILTO; 765
112-65-BT4-5	TRIP BRANCH FROM BUS 275233 TO BUS 270644 CKT 1 WILTO; 765	/ WILTO;4M 345
112-03-B14-3	TRIP BRANCH FROM BUS 275233 TO BUS 270927 CKT 1 WILTO; R 345	/ WILTO;4M 345
	TRIP BRANCH FROM BUS 275233 TO BUS 275333 CKT 1 WILTO;4C 33 END	/ WILTO;4M 345
	CONTINGENCY '112-65-BT3-4' TRIP BRANCH FROM BUS 270644 TO BUS 243206 CKT 1	/ WILTO; 765
	05DUMONT 765	•
112-65-BT3-4	TRIP BRANCH FROM BUS 275232 TO BUS 270644 CKT 1 WILTO; 765	/ WILTO;3M 345
112-03- D 13-4	TRIP BRANCH FROM BUS 275232 TO BUS 270926 CKT 1 WILTO; B 345	/ WILTO;3M 345
	TRIP BRANCH FROM BUS 275232 TO BUS 275332 CKT 1 WILTO;3C 33 END	/ WILTO;3M 345
8649_B2_TOR546	CONTINGENCY '8649_B2_TOR546' OPEN BRANCH FROM BUS 242924 TO BUS 243208 CKT 1 R 765 243208 05JEFRSO 765 1 END	/ 242924 05HANG

Contingency Name	Description	
695_B2	CONTINGENCY '695_B2' OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 05DUMONT 765 270644 WILTO; 765 1 END	/ 243206
8807_B2	CONTINGENCY '8807_B2' OPEN BRANCH FROM BUS 243878 TO BUS 255205 CKT 1 05MEADOW 345 255205 17REYNOLDS 345 1 END	/ 243878
363_B2_TOR1682	CONTINGENCY '363_B2_TOR1682' OPEN BRANCH FROM BUS 243208 TO BUS 243209 CKT 1 05JEFRSO 765 243209 05ROCKPT 765 1 END	/ 243208

Table 8

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

			AC	2-080 Contribution	n to Previ	ously Iden	tified Over	loads				
	Contingency				Bus		Load	ing	Rating			\mathbf{FG}
			Affected	Facility							\mathbf{MW}	Ap
#	Type	Name	Area	Description	From	To	Initial	Final	Type	MVA	Con.	p.
			AEP -	05MEADOW-								
		8648_C2_05JE	MISO	17REYNOLDS								
1	LFFB	FRSO 765-B1	NIPS	345 kV line	243878	255205	101.52	103.56	ER	2938	60.01	
		2978_C2_05DU		X2-052 TAP-								
		MONT 765-	AEP -	05DUMONT								
2	LFFB	B_A	AEP	345 kV line	247610	243219	115.34	117.41	ER	1409	43.49	
				X2-052 TAP-								
		112-65-BT4-	AEP -	05DUMONT								
3	LFFB	5	AEP	345 kV line	247610	243219	107.71	109.68	ER	1409	42.92	
		· · · · · · · · · · · · · · · · · · ·		X2-052 TAP-			·					
		112-65-BT3-	AEP -	05DUMONT								
4	LFFB	4	AEP	345 kV line	247610	243219	107.71	109.67	ER	1409	42.92	

Table 9

Steady-State Voltage Requirements

Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

None

Affected System Analysis & Mitigation

LGEE Impacts:

LGEE Impacts to be determined during later study phases (as applicable).

MISO Impacts:

MISO Impacts to be determined during later study phases (as applicable).

Duke, Progress & TVA Impacts:

Duke Carolina, Progress, & TVA Impacts to be determined during later study phases (as applicable).

OVEC Impacts:

OVEC Impacts to be determined during later study phases (as applicable).

Delivery of Energy Portion of Interconnection Request

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request. Only the most severely overloaded conditions are listed. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed, which will study all overload conditions associated with the overloaded element(s) identified.

AC2-080 Delivery of Energy Portion of Interconnection Request													
	Contingency		A 604- J	TF9194	Bus		Loading		Rating		N #XX7	FG	
	#	Туре	Name	Affected Area	Facility Description	From	To	Initial	Final	Туре	MVA	MW Con.	App
Г				AEP -	05MEADOW-								
			363_B2_TOR16	MISO	17REYNOLDS								
	1	N-1	82	NIPS	345 kV line	243878	255205	134.36	137.24	NR	2114	60.92	
Г					05SORENS-								
			363_B2_TOR16	AEP -	AC1-225 TAP								
L	2	N-1	82'	AEP	765 kV line	246999	927280	101.05	101.07	NR	4249	52.38	

AC2-080 Delivery of Energy Portion of Interconnection Request												
	Contingency				В	Bus Lo		oading I		ting		\mathbf{FG}
#	Туре	Name	Affected Area	Facility Description	From	To	Initial	Final	Туре	MVA	MW Con.	App
				X2-052 TAP-								
			AEP -	05DUMONT								
3	N-1	695_B2	AEP	345 kV line	247610	243219	107.62	109.59	NR	1409	42.92	
		0.640 D2 T0		AC1-225 TAP-								
		8649_B2_TO	AEP -	05MARYSV								
4	N-1	R546	AEP	765 kV line	927280	242928	103.31	116.09	NR	4249	52.38	
				AC2-080 TAP-								
			AEP -	050LIVE 345								
5	N-1	8807_B2	AEP	kV line	931600	243229	103.31	116.09	NR	971	124.07	

Table 10

Figure 1: Primary Point of Interconnection (Olive – Reynolds (NIPSCO) 345 kV Circuit #1)

Single-Line Diagram

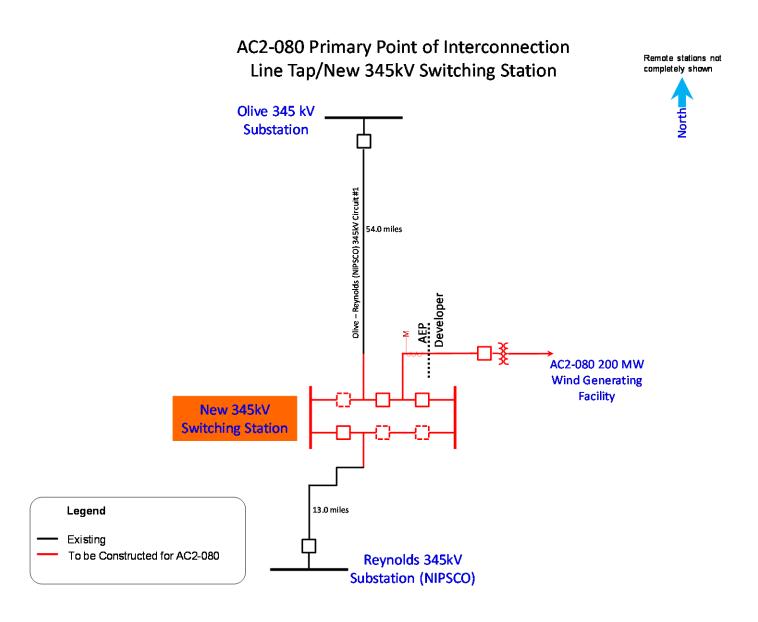
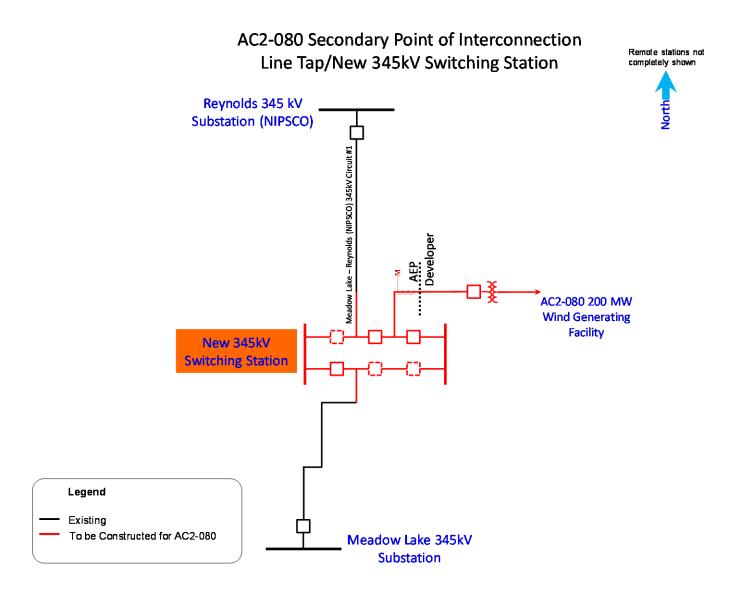


Figure 3: Secondary Point of Interconnection (Reynolds (NIPSCO) – Meadow Lake 345 kV Circuit #1)

Single-Line Diagram



Appendices – Option 1

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(AEP - AEP) The X2-052 TAP-05DUMONT 345 kV line (from bus 247610 to bus 243219 ckt 2) loads from 115.32% to 117.35% (**DC power flow**) of its emergency rating (1409 MVA) for the line fault with failed breaker contingency outage of '2978_C2_05DUMONT 765-B_A'. This project contributes approximately 42.87 MW to the thermal violation.

CONTINGENCY '2978_C2_05DUMONT 765-B_A'

OPEN BRANCH FROM BUS 243206 TO BUS 920251 CKT 1 / 243206
05DUMONT 765 920251 X1-020 TAP 765 1

OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 / 243206
05DUMONT 765 270644 WILTON ; 765 1
END

Bus Number	Bus Name	Full Contribution
247900	05FR-11G E	6.99
247901	05FR-12G E	6.88
247902	05FR-21G E	7.35
247903	05FR-22G E	7.04
247904	05FR-3G E	14.26
247905	05FR-4G E	10.72
246909	05MDL-1G C	0.71
247906	05MDL-1G E	16.04
246910	05MDL-2G C	0.35
247907	05MDL-2G E	7.96
246976	05MDL-3G C	0.35
247912	05MDL-3G E	8.32
246979	05MDL-4G C	0.71
247913	05MDL-4G E	7.94
931011	AC2-007 C	0.49
931012	AC2-007 E	0.92
931601	AC2-080 C OP	5.57
931602	AC2-080 E OP	37.3
290051	GSG-6; E	6.12
275149	KEMPTON ;1E	10.51
290108	LEEDK;1U E	14.15
274850	MENDOTA H;RU	3.52
275148	MILKS GRV;1E	10.51
293061	N-015 E	9.04
293644	O22 E1	5.88
293645	O22 E2	11.42
290021	O50 E	11.38
294392	P-010 E	11.48
274830	PWR VTREC;1U	3.56
274831	PWR VTREC;2U	3.56
274722	S-055 E	6.51

884780	S-058 C	28.93
884781	S-058 E	86.78
295111	SUBLETTE E	1.59
247556	T-127 C	2.04
247943	T-127 E	8.14
291984	U4-033	0.72
274814	UNIV PK N;0U	0.56
274805	UNIV PK N;1U	0.56
274806	UNIV PK N;2U	0.56
274807	UNIV PK N;3U	0.56
274808	UNIV PK N;4U	0.56
274809	UNIV PK N;5U	0.56
274810	UNIV PK N;6U	0.56
274811	UNIV PK N;7U	0.56
274812	UNIV PK N;8U	0.56
274813	UNIV PK N;9U	0.56
274815	UNIV PK N;XU	0.56
274816	UNIV PK N;YU	0.56
295109	WESTBROOK E	3.28
274687	WILL CNTY;4U	37.81
247611	X2-052	66.29
920462	Y2-103	26.02
920472	Y3-013 1	2.17
920482	Y3-013 2	2.17
920492	Y3-013 3	2.17
LTF	Z1-043	17.53
247634	Z1-051 E	-1.73
916502	Z1-106 E1	0.73
916504	Z1-106 E2	0.73
916512	Z1-107 E	1.51
916522	Z1-108 E	1.44
LTF	Z1-112	6.09
916651	Z1-127 1	0.96
916652	Z1-127 2	0.57
920782	Z2-081	0.96
920882	Z2-114 C	0.39
920883	Z2-114 E	0.39
920932	AA1-018 C	1.46
920933	AA1-018 E	9.77
921012	AA1-040 1	0.74
921022	AA1-040 2	0.74
LTF	AA1-071	4.06
921222	AA1-078	2.26
918972	AA1-116 E	1.5
918982	AA1-117 E	1.5

921692	AA2-035	74.56
922053	AA2-107 E	1.43
922183	AA2-123 E	1.42
922592	AB1-006 C	2.61
922593	AB1-006 E	17.48
922912	AB1-080	22.33
923002	AB1-089 C	39.07
923012	AB1-090 C	39.07
923012	AB1-091 C OP	41.02
930751	AB1-121	60.7
930752	AB1-121 E	57.57
930761	AB1-121 E	42.43
930762	AB1-122 2	41.54
923562	AB1-172	0.47
LTF	AB2-013	9.9
924471	AB2-096 AB2-191 C	24.72
925301		0.74
925302	AB2-191 E	0.66
926311	AC1-109	1.1
926321	AC1-109 2	1.1
926331	AC1-110	1.09
926341	AC1-110 2	1.09
926351	AC1-111	0.44
926361	AC1-111 2	0.44
926371	AC1-111 3	0.44
926381	AC1-111 4	0.44
926391	AC1-111 5	0.44
926401	AC1-111 6	0.44
926421	AC1-113 1	0.7
926422	AC1-113 2	0.7
926431	AC1-114	1.4
926601	AC1-142A	2.41
926602	AC1-142A 2	2.41
926701	AC1-153 C	45.15
926711	AC1-153 C2	46.12
926702	AC1-153 E	1.81
926712	AC1-153 E2	1.85
926821	AC1-168 C OP	0.72
926822	AC1-168 E OP	4.82
927091	AC1-204	41.63
927092	AC1-204 2	41.65

Appendices – Option 2

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

Appendix 1

(AEP - MISO NIPS) The 05MEADOW-17REYNOLDS 345 kV line (from bus 243878 to bus 255205 ckt 1) loads from 101.52% to 103.56% (**DC power flow**) of its emergency rating (2938 MVA) for the line fault with failed breaker contingency outage of '8648_C2_05JEFRSO 765-B1'. This project contributes approximately 60.01 MW to the thermal violation.

CONTINGENCY '8648_C2_05JEFRSO 765-B1'

OPEN BRANCH FROM BUS 243208 TO BUS 243209 CKT 1 / 243208 05JEFRSO

765 243209 05ROCKPT 765 1

OPEN BRANCH FROM BUS 243208 TO BUS 242865 CKT 2 / 243208 05JEFRSO

765 242865 05JEFRSO 345 2

OPEN BRANCH FROM BUS 242865 TO BUS 248000 CKT Z1 / 242865

05JEFRSO 345 248000 06CLIFTY 345 Z1

END

Bus Number	Bus Name	Full Contribution
243859	05FR-11G C	1.76
247900	05FR-11G E	39.87
243862	05FR-12G C	1.73
247901	05FR-12G E	39.2
243864	05FR-21G C	1.85
247902	05FR-21G E	41.9
243866	05FR-22G C	1.76
247903	05FR-22G E	40.12
243870	05FR-3G C	3.57
247904	05FR-3G E	81.26
243873	05FR-4G C	2.77
247905	05FR-4G E	61.1
246909	05MDL-1G C	4.24
247906	05MDL-1G E	96.29
246910	05MDL-2G C	2.12
247907	05MDL-2G E	47.75
246976	05MDL-3G C	2.12
247912	05MDL-3G E	49.93
246979	05MDL-4G C	4.24
247913	05MDL-4G E	47.63
243442	05RKG1	27.98
243443	05RKG2	27.55
931601	AC2-080 C OP	7.8
931602	AC2-080 E OP	52.21
998111	J468	2.83
998112	J468 E	16.05
998120	J515	55.03
247556	T-127 C	12.22
247943	T-127 E	48.86

900404	X3-028 C	228.5
900405	X3-028 E	304.66
247629	Y3-038	4.34
701171	Y4-018 C	0.95
701172	Y4-018 E	3.8
701461	Y4-047	14.76
701471	Y4-048	17.16
701842	Y4-085 E	1.11
LTF	AA1-001	5.37
922592	AB1-006 C	15.68
922593	AB1-006 E	104.92
922982	AB1-087 C OP	83.78
922992	AB1-088 C OP	83.78
LTF	AC1-002	37.08
927331	AC1-040 C	6.3
927332	AC1-040 E	10.28

Appendix 2

(AEP - AEP) The X2-052 TAP-05DUMONT 345 kV line (from bus 247610 to bus 243219 ckt 2) loads from 115.34% to 117.41% (**DC power flow**) of its emergency rating (1409 MVA) for the line fault with failed breaker contingency outage of '2978_C2_05DUMONT 765-B_A'. This project contributes approximately 43.49 MW to the thermal violation.

CONTINGENCY '2978_C2_05DUMONT 765-B_A'

OPEN BRANCH FROM BUS 243206 TO BUS 920251 CKT 1 / 243206
05DUMONT 765 920251 X1-020 TAP 765 1

OPEN BRANCH FROM BUS 243206 TO BUS 270644 CKT 1 / 243206
05DUMONT 765 270644 WILTON ; 765 1
END

Bus Number	Bus Name	Full Contribution
247900	05FR-11G E	6.99
247901	05FR-12G E	6.88
247902	05FR-21G E	7.35
247903	05FR-22G E	7.04
247904	05FR-3G E	14.26
247905	05FR-4G E	10.72
246909	05MDL-1G C	0.71
247906	05MDL-1G E	16.04
246910	05MDL-2G C	0.35
247907	05MDL-2G E	7.96
246976	05MDL-3G C	0.35
247912	05MDL-3G E	8.32
246979	05MDL-4G C	0.71
247913	05MDL-4G E	7.94
931011	AC2-007 C	0.49
931012	AC2-007 E	0.92
931601	AC2-080 C OP	5.65
931602	AC2-080 E OP	37.84
290051	GSG-6; E	6.12
275149	KEMPTON ;1E	10.51
290108	LEEDK;1U E	14.15
274850	MENDOTA H;RU	3.52
275148	MILKS GRV;1E	10.51
293061	N-015 E	9.04
293644	O22 E1	5.88
293645	O22 E2	11.42
290021	O50 E	11.38
294392	P-010 E	11.48
274830	PWR VTREC;1U	3.56
274831	PWR VTREC;2U	3.56
274722	S-055 E	6.51

004700		
884780	S-058 C	28.93
884781	S-058 E	86.78
295111	SUBLETTE E	1.59
247556	T-127 C	2.04
247943	T-127 E	8.14
291984	U4-033	0.72
274814	UNIV PK N;0U	0.56
274805	UNIV PK N;1U	0.56
274806	UNIV PK N;2U	0.56
274807	UNIV PK N;3U	0.56
274808	UNIV PK N;4U	0.56
274809	UNIV PK N;5U	0.56
274810	UNIV PK N;6U	0.56
274811	UNIV PK N;7U	0.56
274812	UNIV PK N;8U	0.56
274813	UNIV PK N;9U	0.56
274815	UNIV PK N;XU	0.56
274816	UNIV PK N;YU	0.56
295109	WESTBROOK E	3.28
274687	WILL CNTY;4U	37.81
247611	X2-052	66.29
920462	Y2-103	26.02
920472	Y3-013 1	2.17
920482	Y3-013 2	2.17
920492	Y3-013 3	2.17
LTF	Z1-043	17.53
247634	Z1-051 E	-1.73
916502	Z1-106 E1	0.73
916504	Z1-106 E2	0.73
916512	Z1-107 E	1.51
916522	Z1-108 E	1.44
LTF	Z1-112	6.09
916651	Z1-127 1	0.96
916652	Z1-127 2	0.57
920782	Z2-081	0.96
920882	Z2-114 C	0.39
920883	Z2-114 E	0.39
920932	AA1-018 C	1.46
920933	AA1-018 E	9.77
921012	AA1-040 1	0.74
921022	AA1-040 2	0.74
LTF	AA1-071	4.06
921222	AA1-078	2.26
918972	AA1-116 E	1.5
918982	AA1-117 E	1.5

921692	AA2-035	74.56
922053	AA2-107 E	1.43
922183	AA2-123 E	1.42
922592	AB1-006 C	2.61
922593	AB1-006 E	17.48
922912	AB1-080	22.33
923002	AB1-089 C	39.07
923012	AB1-090 C	39.07
923012	AB1-091 C OP	41.01
930751	AB1-121	60.69
930752	AB1-121 E	57.56
930752	AB1-121 E AB1-122 1	42.43
930762	AB1-122 2	41.54
923562	AB1-172	0.47
25502 LTF	AB1-1/2 AB2-013	9.9
924471	AB2-013 AB2-096	24.72
925301	AB2-191 C	0.74
925301	AB2-191 E	0.66
925302	AC1-109	1.1
926321	AC1-109 AC1-109 2	1.1
926331	AC1-109 2 AC1-110	1.19
926341	AC1-110 2	1.09
926351	AC1-110 2 AC1-111	0.44
926361	AC1-111 2	0.44
	AC1-111 2 AC1-111 3	0.44
926371		
926381	ACI-111 4	0.44
926391	AC1-111 5	
926401	ACI-111 6	0.44
926421	ACI-113 1	0.7
926422	AC1-113 2	0.7
926431	ACI-114	1.4
926601	AC1-142A	2.41
926602	AC1-142A 2	2.41
926701	AC1-153 C	45.15
926711	ACI-153 C2	46.12
926702	AC1-153 E	1.81
926712	AC1-153 E2	1.85
926821	AC1-168 C OP	0.72
926822	AC1-168 E OP	4.82
927091	ACI-204	41.63
927092	AC1-204 2	41.64