



**Generation Interconnection  
Feasibility Study Report  
for  
Queue Project AG1-037  
AHOSKIE 34.5 KV  
3 MW Capacity / 5 MW Energy**

January 2021

## Table of Contents

1	Introduction.....	3
2	Preface.....	3
3	General .....	4
4	Point of Interconnection.....	5
5	Cost Summary .....	5
6	Transmission Owner Scope of Work .....	6
7	Transmission Owner Analysis.....	7
7.1	Power Flow Analysis .....	7
8	Interconnection Customer Requirements.....	7
8.1	System Protection.....	7
8.2	Compliance Issues and Interconnection Customer Requirements .....	8
8.3	Power Factor Requirements.....	8
9	Revenue Metering and SCADA Requirements .....	8
9.1	PJM Requirements .....	8
9.2	Meteorological Data Reporting Requirements .....	9
9.3	Interconnected Transmission Owner Requirements.....	9
10	Summer Peak - Load Flow Analysis .....	10
10.1	Generation Deliverability .....	11
10.2	Multiple Facility Contingency .....	11
10.3	Contribution to Previously Identified Overloads.....	11
10.4	Potential Congestion due to Local Energy Deliverability.....	11
10.5	System Reinforcements - Summer Peak Load Flow - Primary POI.....	13
10.6	Flow Gate Details.....	14
10.6.1	Index 1 .....	15
10.6.2	Index 2 .....	17
10.7	Queue Dependencies .....	18
10.8	Contingency Descriptions.....	19
11	Short Circuit Analysis.....	20
12	Affected Systems .....	21
12.1	TVA.....	21
12.2	Duke Energy Progress.....	21

## 1 Introduction

This Feasibility Study has been prepared in accordance with the PJM Open Access Transmission Tariff, 36.2, as well as the Feasibility Study Agreement between the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Dominion.

## 2 Preface

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. Cost allocation rules for network upgrades can be found in PJM Manual 14A, Attachment B. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Interconnection Customer seeking to interconnect a wind or solar generation facility shall maintain meteorological data facilities as well as provide that meteorological data which is required per Schedule H to the Interconnection Service Agreement and Section 8 of Manual 14D.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

### 3 General

The Interconnection Customer (IC), has proposed a Solar generating facility located in Hertford County, North Carolina. The installed facilities will have a total capability of 5 MW with 3 MW of this output being recognized by PJM as Capacity. The proposed in-service date for this project is December 31, 2021. This study does not imply a TO commitment to this in-service date.

<b>Queue Number</b>	<b>AG1-037</b>
<b>Project Name</b>	AHOSKIE 34.5 KV
<b>State</b>	North Carolina
<b>County</b>	Hertford
<b>Transmission Owner</b>	Dominion
<b>MFO</b>	5
<b>MWE</b>	5
<b>MWC</b>	3
<b>Fuel</b>	Solar/Storage
<b>Basecase Study Year</b>	2024

Any new service customers who can feasibly be commercially operable prior to June 1st of the basecase study year are required to request interim deliverability analysis.

## 4 Point of Interconnection

AG1-037 will interconnect with the Dominion transmission system at the Ahoskie 115 kV substation.

## 5 Cost Summary

The AG1-037 project will be responsible for the following costs:

Description	Total Cost
<b>Total Physical Interconnection Costs</b>	\$ To be provided in the two-party IA with ITO
<b>Total System Network Upgrade Costs</b>	\$ 10,676,000 <sup>1</sup>
<b>Total Costs</b>	\$ 10,676,000

This cost excludes a Federal Income Tax Gross Up charges. This tax may or may not be charged based on whether this project meets the eligibility requirements of IRS Notice 2016-36, 2016-25 I.R.B. (6/20/2016). If at a future date it is determined that the Federal Income Tax Gross charge is required, the Transmission Owner shall be reimbursed by the Interconnection Customer for such taxes.

Cost allocations for any System Upgrades will be provided in the System Impact Study Report.

---

<sup>1</sup> This project currently causes and/or contributes to overloads of the Transmission System (see Summer Peak Load Flow Analysis section below) and therefore has potential to have cost allocation for the system reinforcements listed in the report. This will be re-evaluated in the System Impact phase. The results may vary with queue customers withdrawing from the queue and other generators deactivating over time. If a customer is the first to cause the need for a project (causes loading to exceed 100% of rating), then the customer is responsible. If a customer contributes to a facility that is already overloaded by a prior queue, then they may receive cost allocation.

## 6 Transmission Owner Scope of Work

*Remote Terminal Work:* During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

## 7 Transmission Owner Analysis

Dominion assessed the impact of the proposed AG1-037 for compliance with NERC Reliability Criteria on the Dominion Transmission System. The system was assessed using the summer 2024 AG1 case provided to Dominion by PJM.

When performing a generation analysis, Dominion's main analysis includes load flow study results following a single contingency event for both normal and stressed system conditions. Dominion Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under normal and stressed system conditions. A full listing of Dominion's Planning Criteria and interconnection requirements can be found in the Company's Facility Connection Requirements which are publicly available at: <http://www.dominionenergy.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed generation facility under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically, in Planning Studies, NERC Planning Event 3 and 6 Contingency Conditions (Loss of generator, transmission circuit, transformer, shunt device, or Single Pole of a DC line followed by the loss of a generator, transmission circuit, transformer, shunt device or single pole of a DC line) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For Dominion Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating.

### 7.1 Power Flow Analysis

PJM performed a power flow analysis of the transmission system using a 2024 summer peak load flow model and the results were verified by Dominion. Additionally, Dominion performed an analysis of its transmission system and no further deficiencies were identified.

## 8 Interconnection Customer Requirements

### 8.1 System Protection

The IC must design its Customer Facilities in accordance with all applicable standards, including the standards in Dominion's "Dominion Energy Electric Transmission Generator Interconnection Requirements" documented in Dominion's Facility Interconnection Requirements "Exhibit C" located at: <https://www.dominionenergy.com/company/moving-energy/electric-transmission-access>. Preliminary Protection requirements will be provided as part of the Facilities Study. Detailed Protection Requirements will be provided once the project enters the construction phase.

## 8.2 Compliance Issues and Interconnection Customer Requirements

The proposed Customer Facilities must be designed in accordance with Dominion's "Dominion's Facility Interconnection Requirements" document located at: <https://www.dominionenergy.com/company/moving-energy/electric-transmission-access>. In particular, the IC is responsible for the following:

1. The purchase and installation of a fully rated protection device (circuit breaker, circuit switcher, fuse) to protect the IC's GSU transformer(s).
2. The purchase and installation of the minimum required Dominion generation interconnection relaying and control facilities as described in the System Protection section noted above. This includes over/under voltage protection, over/under frequency protection, and zero sequence voltage protection relays.
3. The purchase and installation of supervisory control and data acquisition ("SCADA") equipment to provide information in a compatible format to the Dominion Transmission System Control Center.
4. Compliance with the Dominion and PJM generator power factor and voltage control requirements.

The GSU(s) associated with the IC queue request shall meet the grounding requirements as noted in Dominion's "Dominion's Facility Interconnection Requirements" document located at: <https://www.dominionenergy.com/company/moving-energy/electric-transmission-access>.

The IC will also be required to meet all PJM, SERC, and NERC reliability criteria and operating procedures for standards compliance. For example, the IC will need to properly locate and report the over and under voltage and over and under frequency system protection elements for its units as well as the submission of the generator model and protection data required to satisfy the PJM and SERC audits. Failure to comply with these requirements may result in a disconnection of service if the violation is found to compromise the reliability of the Dominion system.

## 8.3 Power Factor Requirements

The IC shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading (absorbing VARs) to 0.95 lagging (supplying VARs) measured at the high-side of the facility substation transformer(s) connected to the Dominion transmission system.

# 9 Revenue Metering and SCADA Requirements

## 9.1 PJM Requirements

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Section 8 of Attachment O.



## 9.2 Meteorological Data Reporting Requirements

The solar generation facility shall provide the Transmission Provider with site-specific meteorological data including:

- Back Panel temperature (Fahrenheit) - (Required for plants with Maximum Facility Output of 3 MW or higher)
- Irradiance (Watts/meter<sup>2</sup>) - (Required for plants with Maximum Facility Output of 3 MW or higher)
- Ambient air temperature (Fahrenheit) - (Accepted, not required)
- Wind speed (meters/second) - (Accepted, not required)
- Wind direction (decimal degrees from true north) - (Accepted, not required)

## 9.3 Interconnected Transmission Owner Requirements

The IC will be required to comply with all Interconnected Transmission Owner's revenue metering requirements for generation interconnection customers located at the following link:

<http://www.pjm.com/planning/design-engineering/to-tech-standards/>

## 10 Summer Peak - Load Flow Analysis

The Queue Project AG1-037 was evaluated as a 5.0 MW (Capacity 3.0 MW) injection at the Ahoskie 115 kV substation in the Dominion area. Project AG1-037 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AG1-037 was studied with a commercial probability of 53.0 %. Potential network impacts were as follows:

## 10.1 Generation Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADIN G %	POST PROJECT LOADIN G %	AC D C	MW IMPAC T
168910119	314568	3EARLEY S	115.0	DVP	314569	6EARLEY S	230.0	DVP	1	DVP_P1-3: 6EARLEY S-TX#4	single	202.475997925	99.32	100.09	DC	1.55

## 10.2 Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

## 10.3 Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADIN G %	POST PROJECT LOADIN G %	AC D C	MW IMPAC T
168909987	314551	3AHOSKI E	115.0	DVP	314568	3EARLEY S	115.0	DVP	1	DVP_P1-2: LN 108-A	single	141.0	171.44	173.56	DC	3.0
168909989	314551	3AHOSKI E	115.0	DVP	314568	3EARLEY S	115.0	DVP	1	DVP_P1-2: LN 140	single	141.0	129.05	130.81	DC	2.49
168909990	314551	3AHOSKI E	115.0	DVP	314568	3EARLEY S	115.0	DVP	1	Base Case	single	141.0	103.56	105.23	DC	2.37

## 10.4 Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADIN G %	POST PROJECT LOADIN G %	AC D C	MW IMPAC T
168909985	314551	3AHOSK IE	115.0	DVP	314568	3EARLEYS	115.0	DVP	1	DVP_P1-2: LN 108-A	operation	141.0	251.21	254.76	DC	5.0

ID	FROM BUS#	FROM BUS	kV	FROM BUS AREA	TO BUS#	TO BUS	kV	TO BUS AREA	CK T ID	CONT NAME	Type	Rating MVA	PRE PROJEC T LOADIN G %	POST PROJEC T LOADIN G %	AC D C	MW IMPAC T
1689099 88	31455 1	3AHOSK IE	115. 0	DVP	31456 8	3EARLE YS	115. 0	DVP	1	Base Case	operatio n	141.0	163.93	166.72	DC	3.95
1689100 73	31456 8	3EARLEY S	115. 0	DVP	31456 9	6EARLE YS	230. 0	DVP	2	DVP_P1- 3: 6EARLEY S-TX#3	operatio n	175.7799987 79	163.81	165.28	DC	2.59
1689100 76	31456 8	3EARLEY S	115. 0	DVP	31456 9	6EARLE YS	230. 0	DVP	2	Base Case	operatio n	167.4140014 65	99.37	100.29	DC	1.55
1689101 17	31456 8	3EARLEY S	115. 0	DVP	31456 9	6EARLE YS	230. 0	DVP	1	DVP_P1- 3: 6EARLEY S-TX#4	operatio n	202.4759979 25	142.33	143.61	DC	2.59

## 10.5 System Reinforcements - Summer Peak Load Flow - Primary POI

ID	Idx	Facility	Upgrade Description	Cost
168909987,168909990,168909989	2	3AHOSKIE 115.0 kV - 3EARLEYS 115.0 kV Ckt 1	<u>DVP</u> dom-313 (356) : Reconductor 6.81 miles of 115 kV Line 136 from Earleys to Ahoskie with 768.2 ACSS 250 C. Replace Wave Trap, Relay (CT and Secondary CT) at Earleys terminal. Replace Line Switch and Line Lead at Ahoskie terminal. Project Type : FAC Cost : \$4,676,000 Time Estimate : 30-36 Months	\$4,676,000
168910119	1	3EARLEYS 115.0 kV - 6EARLEYS 230.0 kV Ckt 1	<u>DVP</u> dom-016 (27) : Add additional 230/115 kV transformer at Earleys substation. Project Type : CON Cost : \$6,000,000 Time Estimate : 16-18 Months	\$6,000,000
			<b>TOTAL COST</b>	<b>\$10,676,000</b>

## 10.6 Flow Gate Details

The following indices contain additional information about each facility presented in the body of the report. For each index, a description of the flowgate and its contingency was included for convenience. The intent of the indices is to provide more details on which projects/generators have contributions to the flowgate in question. All New Service Queue Requests, through the end of the Queue under study, that are contributors to a flowgate will be listed in the indices. Please note that there may be contributors that are subsequently queued after the queue under study that are not listed in the indices. Although this information is not used "as is" for cost allocation purposes, it can be used to gage the impact of other projects/generators. It should be noted the project/generator MW contributions presented in the body of the report are Full MW Impact contributions which are also noted in the indices column named "Full MW Impact", whereas the loading percentages reported in the body of the report, take into consideration the PJM Generator Deliverability Test rules such as commercial probability of each project as well as the ramping impact of "Adder" contributions. The MW Impact found and used in the analysis is shown in the indices column named "Gendeliv MW Impact".

---

## 10.6.1 Index 1

ID	FROM BUS#	FROM BUS	FROM BUS AREA	TO BUS#	TO BUS	TO BUS AREA	CKT ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADING %	POST PROJECT LOADING %	AC DC	MW IMPACT
168910119	314568	3EARLEYS	DVP	314569	6EARLEYS	DVP	1	DVP_P1-3: 6EARLEYS-TX#4	single	202.48	99.32	100.09	DC	1.55

Bus #	Bus	Gendeliv MW Impact	Type	Full MW Impact
313506	AB1-173 C OP	2.8389	80/20	2.8389
313719	3CHESTNUT	0.7625	80/20	0.7625
314582	3KELFORD	0.9917	80/20	0.9917
314589	3MURPHYS	0.1592	80/20	0.1592
314623	3WITAKRS	0.0973	80/20	0.0973
315115	1S HAMPT1	1.0924	80/20	1.0924
315126	1ROARAP2	0.8579	80/20	0.8579
315128	1ROARAP4	0.8187	80/20	0.8187
315606	3AA2-053SOLA	1.6734	80/20	1.6734
315607	3AA1-063SOLA	1.1244	80/20	1.1244
315608	3AA2-088SOLA	1.0820	80/20	1.0820
316087	AB2-174 C	0.4142	80/20	0.4142
316103	AB2-015 C	5.8125	80/20	5.8125
316129	AC1-054 C	3.1996	80/20	3.1996
316140	AB2-099 C (Suspended)	1.8134	80/20	1.8134
920591	AA2-165 C	0.1024	80/20	0.1024
923991	AB2-040 C O1	3.0919	80/20	3.0919
926201	AC1-098 C	9.2447	80/20	9.2447
926211	AC1-099 C	3.0980	80/20	3.0980
927145	AC1-208 C	8.4153	80/20	8.4153
932631	AC2-084 C	13.1786	80/20	13.1786
938771	AE1-103 C	1.7869	80/20	1.7869
941541	AE2-151 C (Withdrawn : 01/08/2021)	0.6008	80/20	0.6008
943171	AE2-346 C	4.3522	80/20	4.3522
957521	AF2-046 C	35.0268	80/20	35.0268
961091	AF2-400 C	0.3139	80/20	0.3139
961681	AG1-008 C	35.0970	80/20	35.0970
961931	AG1-036 C	3.5624	80/20	3.5624
961941	AG1-037 C	1.5544	80/20	1.5544
962331	AG1-082 C	6.2174	80/20	6.2174
962341	AG1-083 C	6.2174	80/20	6.2174
962351	AG1-084 C	6.1509	80/20	6.1509
962361	AG1-085 C	6.1509	80/20	6.1509
964501	AG1-313 C O1	8.0195	80/20	8.0195
964801	AG1-343 C	7.3584	80/20	7.3584
965291	AG1-394 C	2.2684	80/20	2.2684
965721	AG1-440 C	2.4129	80/20	2.4129
965731	AG1-441 C	2.4129	80/20	2.4129
965771	AG1-445	1.3941	80/20	1.3941
965781	AG1-446	1.3941	80/20	1.3941

Bus #	Bus	Gendeliv MW Impact	Type	Full MW Impact
966751	AG1-546 C	7.3918	80/20	7.3918
966811	AG1-552 C	1.3622	80/20	1.3622
WEC	WEC	0.0110	Confirmed LTF	0.0110
LGEE	LGEE	0.0239	Confirmed LTF	0.0239
CPL	CPL	0.0969	Confirmed LTF	0.0969
CBM-W2	CBM-W2	0.4928	Confirmed LTF	0.4928
NY	NY	0.0343	Confirmed LTF	0.0343
TVA	TVA	0.0952	Confirmed LTF	0.0952
SIGE	SIGE	0.0114	Confirmed LTF	0.0114
CBM-S2	CBM-S2	1.3676	Confirmed LTF	1.3676
CBM-S1	CBM-S1	0.0239	Confirmed LTF	0.0239
MEC	MEC	0.0667	Confirmed LTF	0.0667
LAGN	LAGN	0.1155	Confirmed LTF	0.1155
CBM-W1	CBM-W1	0.4486	Confirmed LTF	0.4486



## 10.6.2 Index 2

ID	FROM BUS#	FROM BUS	FROM BUS AREA	TO BUS#	TO BUS	TO BUS AREA	CKT ID	CONT NAME	Type	Rating MVA	PRE PROJECT LOADING %	POST PROJECT LOADING %	AC DC	MW IMPACT
168909987	314551	3AHOSKIE	DVP	314568	3EARLEYS	DVP	1	DVP_P1-2: LN 108-A	single	141.0	171.44	173.56	DC	3.0

Bus #	Bus	Gendeliv MW Impact	Type	Full MW Impact
314589	3MURPHYS	0.5096	80/20	0.5096
316140	AB2-099 C (Suspended)	3.4999	80/20	3.4999
943171	AE2-346 C	8.3998	80/20	8.3998
957521	AF2-046 C	99.7980	80/20	99.7980
961681	AG1-008 C	99.9980	80/20	99.9980
961931	AG1-036 C	8.0998	80/20	8.0998
961941	AG1-037 C	2.9999	80/20	2.9999
962331	AG1-082 C	11.9998	80/20	11.9998
962341	AG1-083 C	11.9998	80/20	11.9998
964801	AG1-343 C	34.9993	80/20	34.9993
CALDERWOOD	CALDERWOOD	0.0010	Confirmed LTF	0.0010
NY	NY	0.0011	Confirmed LTF	0.0011
PRAIRIE	PRAIRIE	0.0052	Confirmed LTF	0.0052
CHEOAH	CHEOAH	0.0010	Confirmed LTF	0.0010
COTTONWOOD	COTTONWOOD	0.0042	Confirmed LTF	0.0042
HAMLET	HAMLET	0.0012	Confirmed LTF	0.0012
GIBSON	GIBSON	0.0011	Confirmed LTF	0.0011
BLUEG	BLUEG	0.0035	Confirmed LTF	0.0035
TRIMBLE	TRIMBLE	0.0011	Confirmed LTF	0.0011
CATAWBA	CATAWBA	0.0007	Confirmed LTF	0.0007

## 10.7 Queue Dependencies

The Queue Projects below are listed in one or more indices for the overloads identified in your report. These projects contribute to the loading of the overloaded facilities identified in your report. The percent overload of a facility and cost allocation you may have towards a particular reinforcement could vary depending on the action of these earlier projects. The status of each project at the time of the analysis is presented in the table. This list may change as earlier projects withdraw or modify their requests.

Queue Number	Project Name	Status
AA1-063	Huntsville (Cabin Creek) 69kV	Withdrawn
AA2-053	Carolina-Jackson 115kV	In Service
AA2-088	Boykins-Handsome 115kV	In Service
AA2-165	Hornertown-Whitakers 115kV	In Service
AB1-173	Brink-Trego 115kV	Engineering and Procurement
AB2-015	Franklin 115kV	Engineering and Procurement
AB2-040	Brink 115kV	Engineering and Procurement
AB2-099	Ahoskie 34.5kV	Suspended
AB2-174	Emporia-Trego 115kV	In Service
AC1-054	Kerr Dam–Eatons Ferry 115 kV	Engineering and Procurement
AC1-098	Dawson-South Justice 115kV	Engineering and Procurement
AC1-099	Dawson-South Justice 115kV	Engineering and Procurement
AC1-208	Cox-Whitakers 115kV	Engineering and Procurement
AC2-084	Dawson-South Justice 115kV	Active
AE1-103	Holland-Union Camp 115 kV	Active
AE2-151	Earleys 34.5kV	Withdrawn
AE2-346	Ahoskie 34.5 kV	Active
AF2-046	Tunis-Mapleton 115 kV	Active
AF2-400	Franklin 13.2 kV	Engineering and Procurement
AG1-008	Tunis-Mapleton 115 kV	Active
AG1-036	Tunis 34.5 kV	Active
AG1-037	Ahoskie 34.5 kV	Active
AG1-082	Ahoskie 34.5 kV	Active
AG1-083	Ahoskie 34.5 kV	Active
AG1-084	Earlys 34.5 kV	Active
AG1-085	Earlys 34.5 kV	Active
AG1-313	Jackson DP–Occonechee 115 kV	Active
AG1-343	Boykins-Murphy 115 kV	Active
AG1-394	Boykins 34.5 kV	Active
AG1-440	Palmer Springs 115 kV	Active
AG1-441	Palmer Springs 115 kV	Active
AG1-445	Palmer Spring 115 kV	Active
AG1-446	Palmer Springs 115 kV	Active
AG1-546	Ebony-Elams Road 115 kV	Active
AG1-552	Carolina 13.2 kV	Active

## 10.8 Contingency Descriptions

Contingency Name	Contingency Definition
<b>DVP_P1-2: LN 140</b>	CONTINGENCY 'DVP_P1-2: LN 140' OPEN BRANCH FROM BUS 313720 TO BUS 314526 CKT 1 /* 3NEWSOMS 115.00 - 3HANDSOM 115.00 OPEN BRANCH FROM BUS 314526 TO BUS 314534 CKT 1 /* 3HANDSOM 115.00 - 3S HAMPT 115.00 OPEN BUS 314526 /* ISLAND: 3HANDSOM 115.00 END
<b>DVP_P1-2: LN 108-A</b>	CONTINGENCY 'DVP_P1-2: LN 108-A' OPEN BRANCH FROM BUS 314558 TO BUS 964800 CKT 1 /* 3BOYKINS 115.00 - AG1-343 TAP 115.00 END
<b>DVP_P1-3: 6EARLEYS-TX#3</b>	CONTINGENCY 'DVP_P1-3: 6EARLEYS-TX#3' OPEN BRANCH FROM BUS 314568 TO BUS 314569 CKT 1 /* 3EARLEYS 115.00 - 6EARLEYS 230.00 END
<b>Base Case</b>	
<b>DVP_P1-3: 6EARLEYS-TX#4</b>	CONTINGENCY 'DVP_P1-3: 6EARLEYS-TX#4' OPEN BRANCH FROM BUS 314568 TO BUS 314569 CKT 2 /* 3EARLEYS 115.00 - 6EARLEYS 230.00 END

## 11 Short Circuit Analysis

No upgrades identified.

## **12 Affected Systems**

### **12.1 TVA**

TVA Impacts to be determined during later study phases (as applicable).

### **12.2 Duke Energy Progress**

Duke Energy Progress Impacts to be determined during later study phases (as applicable).