# Generation Interconnection Feasibility Study Report

## For

# PJM Generation Interconnection Request Queue Position Z2-009

East Hazelton-Harwood 69kV

### **Preface**

The intent of the feasibility study is to determine a plan, with ballpark cost and construction time estimates, to connect the subject generation to the PJM network at a location specified by the Interconnection Customer. The Interconnection Customer may request the interconnection of generation as a capacity resource or as an energy-only resource. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: (1) Direct Connections, which are new facilities and/or facilities upgrades needed to connect the generator to the PJM network, and (2) Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system.

In some instances a generator interconnection may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the feasibility study, but the actual allocation will be deferred until the impact study is performed.

The Feasibility Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

The conduct of light load analysis as required under the PJM planning process is not performed during the Generation Interconnection Feasibility Study phase of the PJM study process. Additional reinforcement requirements for this Interconnection Request may be defined during the conduct of the light load analysis which shall be performed following execution of the System Impact Study agreement.

#### General

The Interconnection Customer (IC), has proposed a wind generating facility located Freeland, PA. The installed facilities will have a total capability of 67.5 MW with 8.78 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is December 31, 2016. This study does not imply a PPL Electric Utilities (PPL EU) commitment to this in-service date.

### **Point of Interconnection**

Z2-009 will interconnect with the PPL EU transmission system at one of two options. Option 1 is to connect to the Harwood-East Hazelton #2 69kV line. Option 2 is to connect to the Harwood Jenkins #1 69kV line.

### **Cost Summary**

The Z2-009 project will be responsible for the following costs:

Description	<b>Total Cost</b>
Attachment Facilities	\$ 4,250,000
Direct Connection Network Upgrades	\$ 0
Non Direct Connection Network Upgrades	\$ 150,000
Total Costs	\$ 4,400,000

The 69 kV connection estimate is based on the assumptions stated in the following Transmission Attachment Facilities, Direct Connection, and Substation Non- Direct Connection Work sections. This estimate may vary depending upon the Queue Z2-009 substation location and orientation.

<u>Note:</u> Before the Impact Study stage, the exact location of the Interconnection Substation must be identified by the Z2-009 IC in order to refine the cost estimate.

In addition, the Z2-009 project may be responsible for a contribution to the following costs:

Description	<b>Total Cost</b>
New System Upgrades	\$ 9,690,000
Previously Identified Upgrades	\$ 0
Total Costs	\$ 9,690,000

Cost allocations for these upgrades will be provided in the System Impact Study Report.

The transmission and substation costs given above exclude any applicable state or federal taxes. If at a future date Federal CIAC (cost in aid of construction) taxes are deemed necessary by the IRS for this project, both PJM and PPL EU shall be reimbursed by the Interconnection Customer for such taxes.

### Overview

The Z2-009 project can be connected to PPL EU's 69 kV transmission system by tapping the Harwood – East Hazelton #2 69 kV line near White Haven Substation and extending approximately 0.5 mile of single circuit transmission line to the Interconnection Customer's (IC's) Substation. The Point of Interconnection (POI) will be where the PPL EU transmission line lands on the customer's dead-end structure inside the IC's yard. Please see Figure 1 for a one-line diagram of the POI.

#### **Attachment Facilities**

### **Transmission Line Work**

The Z2-009 Project will require siting to identify a suitable route for the 100'-wide right of way needed to construct the approximately 0.5 mile 69 kV single circuit transmission line using 556 Kcmil ACSR conductors with optical ground wire (OPGW) to the dead end structure inside the customer's substation (POI). The tap line will be a 138 kV single circuit steel pole design, initially operated at single circuit 69 kV

- The tap will be designed to 138kv 845BIL standards by utilizing 556.5 ACSR power conductors and 2 0.567" OPGW fiber optic cables in the shield wire position
- The tap will begin from structure number 52975N30214; the existing line currently has 3-556.6 ACSR power conductors and 1 3/8" OHGW
- The total distance of the tap will be less than one mile from this structure
- Structure 52975N30214 will be replaced by a custom high tap pole with foundation
- Reframe structures 53008N30221 and 52929N30206 from suspension to tension
- Average ruling span of 500' will be assumed
- This will result in the use of 5 tangent LD8 steel poles
- There will be 2 splice boxes needed for this project (1 at the high tap pole and 1 at the dead-end structure)

The transmission network upgrade work includes installation of two MOLBAB (Motor Operated Load Break Air Break) switch on the PPL EU Harwood-East Hazleton #2 69 kV line on either side of the tap point to Z2-009. The switches would be installed on a custom designed steel pole with concrete foundations. See Figure 1 for the connection schematic.

PA PUC Certification of the proposed 69 kV transmission line route will be required as it will be designed for future 138 kV operation. The certification would be through the abbreviated "Letter of Notification" (LON) process since the tap is expected to be less than 2 miles long. The lead time required to prepare, file and obtain PA PUC approval and obtain property rights will be approximately 12-15 months and assumes that no litigation or condemnation is required.

### **Substation Work for Mini Yard**

At the tapping point, a mini yard with a motor-operated switch and 69 kV breaker will be installed. A small control house will contain the circuit breaker relays and communication devices. Refer to Figure 1 for clarity.

### **Cost**

The total preliminary cost estimate for the Attachment work is given in the table below. These costs do not include CIAC Tax Gross-up.

Description	,	Total Cost
Transmission line work	\$	3,500,000
Substation work	\$	750,000
<b>Total Attachment Facilities</b>	\$	4,250,000

### **Direct Connection Cost Estimate**

There are no Direct Connection facilities required by PPL EU.

### **Non-Direct Connection Cost Estimate**

The protection system at the source end of the 69 kV line will be modified to support this interconnection. To accommodate Z2-009, the following upgrades are required at PPL EU's Harwood 230-69kV Substation:

- Update relay to Microprocessor based on East Hazleton #2 69kV line at Harwood
- Install 1 Relay (DTT) Cabinets at Harwood
- Install new phone based line protection equipment at Harwood
- Install Potential Transformer (PT) at Harwood necessary for sync check of East Hazleton #2 69kV transmission line
- Modify the controls of the East Hazleton #2 69kV circuit breaker at Harwood for trip and close
- Modify SCADA for new alarms
- Modify AMS (Alarm Management System)
- Perform system checks and test equipment before placing in service

The total preliminary cost estimate for the Non-Direct Connection work is given in the table below. These costs do not include CIAC Tax Gross-up.

Description	<b>Total Cost</b>				
Harwood substation work	\$	150,000			
<b>Total Non-Direct Connection Facility Costs</b>	\$	150,000			

#### **Alternate Outlet**

The IC has not requested an alternate outlet for their generation. When the Harwood-East Hazleton #2 69 kV line needs to come off line for any line maintenance or repair activities, the generator will be asked to come off line.

### **Preliminary Schedule**

The estimated PPL EU elapsed time to complete the 69 kV Attachment Facilities, Direct Connection, and Non-Direct connection substation work is approximately 24 months after the receipt of a fully executed ISA/CSA.

The schedule for the 69 kV substation work to accommodate Z2-009 would depend on the project's start date. The work to accommodate Z2-009 will require substation facility outages.

PPL EU's outage windows for construction are typically available in the spring and fall of the year. Missing an outage window could result in project delays.

The transmission and substation work can be completed concurrently. PPL EU will commence siting, engineering design, material purchase and construction of the facilities identified in this study after receiving written authorization by PJM to begin work. This time frame is contingent upon the acquisition of all rights of way in the stated time frame before the start of construction and detailed design.

### **Transmission Owner Assumptions in Developing the Cost Estimates**

- For the custom-designed steel transmission poles, the lead-time is approximately 32 to 42 weeks. It is estimated that approximately custom designed steel poles will be needed for this project.
- During construction, if extreme weather conditions or other system safety concerns arise, field construction may need to be rescheduled, which could possibly delay the schedule.
- This magnitude estimate has been prepared without extensive research or field review.
- For the new 69 kV double circuit tap from Z2-009 to the Harwood-East Hazleton #2 69 kV line, it is as assumed that a new ROW and siting study would be required and the tap would be owned by PPL EU.
- No environmental, real estate, or permitting issues were reviewed for the estimate of this
  project.
- This estimate assumes that suitable facility outages can be schedule as required to install the new circuit breaker. Failure to meet a scheduled facility outage may result in project delays.
- Excepting any operational, governmental, and/or environmental regulatory delays, the use of
  additional resources, such as overtime, premiums for expedited material, and/or contractor
  labor, may enable PPL EU to decrease this construction period but no guarantees can be
  made. It is also assumed that all rights-of-way and easements are secured by the anticipated
  construction start dates.
- PPL EU recommends that an Interim ISA be completed during the Facilities Study stage to address critical path items, such as long lead-time purchases and any other compressed project schedule issues.
- The ISA/CSA or an Interim Interconnection Service Agreement (IISA) must be signed by the Z2-009 Interconnection Customer, PJM, and PPL EU before any PPL EU design and construction activities may commence.

### **Interconnection Customer Requirements**

### **Z2-009 Generator, GSU, and Line Modeling**

The turbines will be modeled as one unit and will inject 67.5 MW into PPL EU's system.

Per the Z2-009 supplied data the following was used in modeling the generator and the GSU:

### **Z2-009** Generator (Alstom ECO 122):

• Number of Turbines: 25

• Size: 2.7 MW per turbine

MVA Base: 3.27 MVA

• 0.90 lead to 0.90 lag power factor at the Harwood 69 kV bus

#### **Transformers:**

• GSU (Generator Step Up Transformer):

• Number of machines per GSU: 25

• MVA Base: 45 MVA

• Voltage Level: 34.5/69 kV

• Impedance: 8.0%

• GSU (Wind Turbine Unit):

MVA Base: 3.2 kV

• Voltage Level: 34.5/0.69 kV

#### **Transmission Line:**

Voltage Level: 69 kV

• MVA Base: 100 MVA

• Length: 0.25 miles

• Positive sequence impedance: 0.00460+j0.01580

• Negative sequence impedance: 0.01380+j0.04740

### **Telephone Circuit Requirements (At the IPP)**

PPL EU will require a communication path for SCADA, DTT, and voice circuits. PPL EU anticipates that telephone circuits will be required to establish these paths. The Interconnection Customer will be responsible to procure the following:

- 1. A 4-wire dedicated FDDA-type phone line for SCADA
- 2. A normal dialup telephone line for voice communication
- 3. A protective relay-grade telephone circuit for the DTT communication requirements, type PRDA. This phone line needs to communicate between the Interconnection Customer's control house and PPL EU's Harwood Substation.

Phone lines tend to be long lead-time items and must be in place and operational for equipment testing. The Interconnection Customer should investigate with the local phone company the possibility of obtaining this type of service at their facility.

All installation, maintenance, and monthly lease or billing charges for communications facilities are the responsibility of the Interconnection Customer.

### **Intertie and PC Protective Relaying Equipment**

The Interconnection Customer will need to install suitable protection and control equipment at its facilities based on PPL EU parallel generation requirements. This includes both Intertie Protective Relaying (IPR) and Point of Contact (POC) relaying. Please refer to the PPL EU web site for the IPR and POC requirements. The website addresses are shown below:

#### **IPR Requirements:**

 $\frac{https://www.pplelectric.com/at-your-service/electric-rates-and-rules/customer-owned-generation.aspx}{}$ 

#### **POC Requirements:**

https://www.pplelectric.com/at-your-service/electric-rates-and-rules/point-of-contact-requirements-for-high-voltage-facilities.aspx

### **Isolation Breaker Requirement at the Interconnection Customer's Substation**

Per the customer's preliminary sketches, the customer is planning to provide a high side circuit breaker at 69 kV with a manually operated 69 kV disconnect switch on the PPL EU line side of this breaker. Unless otherwise indicated, it is assumed that this be will be the "Isolation Circuit Breaker" and will be operated by the IPR relay and the DTT signal. It is requested that the customer confirm this or provide alternate isolation breaker.

### **Z2-009 Generator Harmonic and Flicker Requirements**

On the PPL EU 69 kV system, the total harmonic distortion to the fundamental voltage wave from a single customer is limited to 1.5% of nominal. In addition, no individual harmonic component can exceed 1.0% of the fundamental system voltage.

If PPL EU discovers that objectionable harmonics in excess of the stated limits are being injected into the system from Z2-009's equipment, the Queue Z2-009 Interconnection Customer will be responsible for taking corrective measures to mitigate harmonic currents.

Concerning voltage flicker, the Interconnection Customer must limit the severity of their voltage variation to within a level which will not cause objectionable flickers to other customers. A voltage drop greater than 5% at the point of interconnection is generally not acceptable. The frequency and severity of the voltage variation will be considered when determining whether a

customer's equipment is violating PPL EU flicker guidelines. PPL EU uses the General Electric flicker-irritation curves as a guideline to determine if the system is operating within acceptable limits. PPL EU will require corrective actions by the Interconnection Customer if their operation causes flickers that exceed PPL EU guidelines. One such correction could be the installation of static var compensators (SVC) to hold a constant voltage.

### **Z2-009** Generator Regulation or Reactive Support Requirements

As specified in Part IV, Subpart E at 54.7 of the PJM OATT, the Project Z2-009 generator shall design its "Facility" to maintain a composite power factor delivery at continuous rated power output at the generators terminals at a power factor of at least 0.95 leading (absorbing vars) to 0.95 lagging (supplying vars).

"For all new wind-powered and other non-synchronous generation facilities, if determined in the system Feasibility study to be required for the safety or reliability of the Transmission System, the Generation Interconnection Customer shall design its Customer Facility with the ability to maintain a composite power delivery at continuous rated power output at a power factor of at least 0.95 leading to 0.95 lagging."

The PPL EU preliminary load flow studies have indicated that the Z2-009 generator will maintain the required voltage regulation within the required ranges. A voltage schedule will be developed at the time of the Facilities Study.

### **Revenue Metering and SCADA Requirements**

### **PJM Requirements**

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

### **PPL EU Requirements**

### **SCADA Equipment Requirements**

PPL EU will require installation of PPL EU approved SCADA equipment that will connect to its existing SCADA system to provide real time values of KW, KVAR, and kV metering data at the POC. SCADA equipment will also provide capability to trip and the status monitoring of the POC isolating circuit breaker. In addition to that, monitoring of other abnormal conditions at developer's plant will be provided where deemed necessary. This connection will be a 4-wire dedicated FDDA-type phone line. PPL EU will provide detailed specifications and design drawings for this equipment.

#### **Revenue Metering Equipment Installation at the Point of Interconnection**

Installation of revenue grade Bi-directional Metering Equipment will be required at the Queue Z2-009 Point of Interconnection (POI) to measure KWh and KVARh. PPL EU will design and

supply the required metering equipment but all the installation cost would be borne by the developer including CT/PTs. All metering equipment must meet applicable PPL EU tariff requirements as well as being compliant with all applicable requirements of the PJM agreements. The equipment must provide bi-directional revenue metering (KWH and KVARH) and real-time data (KW, KVAR, circuit breaker status, and generator bus voltages) for the developer's generating resource. The equipment should be housed in a control cabinet or similar enclosure and must be accessible to PPL EU metering personnel.

### **Other Issues Impacting the Interconnection Customer**

### **Distribution Service Requirements**

The Interconnection Customer must submit a request for electric service through PPL EU's Industrial and Commercial Services (ICS) group if the queue Z2-009 requires back-up electric service at a voltage less than 69 kV. The ICS Help Desk can be reached at 1-888-220-9991. Cost for distribution electric service is NOT included in the PPL scope of work transmission or substation estimates.

### Future Conversion of line to 138 kV from 69 kV

PPL EU presently has no plans to convert this line to 138 kV in the next 15-20 years. If the transmission system in this area is converted to 138 kV in the future, the Interconnection Customer would be responsible for conversion of its substation to 138 kV at that time.

### PA PUC Certification & Environmental Issues

All required land and right of way will be made available to PPL EU at no cost from the Interconnection Customer developer. It is assumed here that the transmission tap would be owned by PPL EU.

PA PUC certification will be required as the tap will be designed for future 138 kV but will initially operate at 69 kV.

### **Intertie 69-34.5 kV Transformer Turns Ratio**

PPL EU typically procures the transformers with the following high side (69 kV) taps:

70.6 kV, 68.8 kV, 67.0 kV, 65.2 kV, 63.4 kV with nominal midpoint voltage is 67 kV, this provides a range of 5% above (in two 2.5% steps) and 5% below (in two 2.5% steps) to the midpoint range of 67 kV.

### **Network Impacts**

### Option 1

The Queue Project Z2-009 was studied as a 67.5 MW (Capacity 8.5 MW) injection as a tap of the Harwood – East Hazelton #2 69 kV line in the PPL area. Project Z2-009 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project Z2-009 was studied with a commercial probability of 53%. A Summer 2018 case was used for this analysis.

Potential network impacts were as follows:

### **Contingency Descriptions**

The following contingencies resulted in overloads:

<b>Contingency Name</b>	Description
PJM69	CONTINGENCY 'PJM69' DISCONNECT BRANCH FROM BUS 200021 TO BUS 200009 CKT 1 /* SUNBURY JUNIATA 500 500 DISCONNECT BRANCH FROM BUS 200021 TO BUS 200022 CKT 2 /* SUNBURY SUSQHANA 500 500 / CKT 1 -> 2 DISCONNECT BRANCH FROM BUS 200021 TO BUS 208109 CKT 24 /* SUNBURY SUNBURY 500 230 END

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(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None.

#### **Multiple Facility Contingency**

(Double Circuit Tower Line contingencies were studied for the full energy output. The contingencies of Line with Failed Breaker and Bus Fault will be performed for the Impact Study.)

None.

#### **Contribution to Previously Identified Overloads**

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

None.

#### **Short Circuit**

(Summary of impacted circuit breakers)

None.

### Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

	Cor	ontingency Affected			В	us		Power	Load	ing %	Rat	ting	MW
#	Type	Name	Area	<b>Facility Description</b>	From	To	Circuit	Flow	Initial	Final	Type	MVA	Contribution
1	N-1	PJM69	PPL	SUSQHANA 500/230kV transformer	208116	200022	21	DC	113.54	114.36	ER	1165	21.49

### **Transmission Owner Network Analysis**

PPL has identified the following overloads:

	Contingency			Affected		Load	ing %	Rating		
#	Case	Type	Name	Area	<b>Facility Description</b>	Initial	Final	Type	MVA	
2	2017 Light Load	Non	Non	PPL	EHAZ 2 – WEAT TP section of HARW-EHAZ 2 69kV line	28	121	SN	46	
3	2017 Light Load	Non	Non	PPL	WEAT TP - WHHA TP section of HARW-EHAZ 2 69kV line	25	124	SN	46	
4	2017 Summer Peak	Non	Non	PPL	EHAZ 2 – WEAT TP section of HARW-EHAZ 2 69kV line	50	98	SN	46	
5	2017 Summer Peak	Non	Non	PPL	WEAT TP - WHHA TP section of HARW-EHAZ 2 69kV line	43	104	SN	46	

### **New System Reinforcements**

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Up	grade Cost	
2, 4	EHAZ 2 – WEAT TP section of HARW- EHAZ 2 69kV line	In order to accommodate the full output of this generator, approximately 3.23 miles of existing 4/0 ACSR along with existing East Hazelton-Freeland tie off the Harwood-East Hazleton #2 69 kV line will need to be rebuilt using 556 ACSR conductor.	Pending	\$	9,690,000	
3, 5	WEAT TP – WHHA TP section of HARW- EHAZ 2 69kV line					
Total New Network Upgrades						

### **Contribution to Previously Identified System Reinforcements**

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

None.

### Option 2

The Queue Project Z2-009 was studied as a 67.5 MW (Capacity 8.5 MW) injection as a tap of the Harwood – Jenkins #1 69 kV line in the PPL area. Project Z2-009 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project Z2-009 was studied with a commercial probability of 100%. A Summer 2018 case was used for this analysis.

Potential network impacts were as follows:

#### **Contingency Descriptions**

The following contingencies resulted in overloads:

<b>Contingency Name</b>	Description
PJM69	CONTINGENCY 'PJM69' DISCONNECT BRANCH FROM BUS 200021 TO BUS 200009 CKT 1 /* SUNBURY JUNIATA 500 500 DISCONNECT BRANCH FROM BUS 200021 TO BUS 200022 CKT 2 /* SUNBURY SUSQHANA 500 500 / CKT 1 -> 2 DISCONNECT BRANCH FROM BUS 200021 TO BUS 208109 CKT 24 /* SUNBURY SUNBURY 500 230 END

Generator Delive	erability
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(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None.

#### **Multiple Facility Contingency**

(Double Circuit Tower Line contingencies were studied for the full energy output. The contingencies of Line with Failed Breaker and Bus Fault will be performed for the Impact Study.)

None.

#### **Contribution to Previously Identified Overloads**

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

None.

#### **Short Circuit**

(Summary of impacted circuit breakers)

None.

### Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

	Cor	ntingency	Affected	Bus		Power	Loading %		Rating		MW		
#	Type	Name	Area	<b>Facility Description</b>	From	To	Circuit	Flow	Initial	Final	Type	MVA	Contribution
1	N-1	PJM69	PPL	SUSQHANA 500/230kV transformer	208116	200022	21	DC	108.38	109.21	ER	1165	21.43
2	Non	Non	PPL	Z2-009 TAP-SAJO 69kV line	917060	211824	1	DC	0.0	229.59%	NR	29	67.5

### **New System Reinforcements**

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

None.

#### **Contribution to Previously Identified System Reinforcements**

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

None.

## **Attachment 1. Single Line Diagram**