

***Generation Interconnection  
System Impact Study Report***

***For***

***PJM Generation Interconnection Request  
Queue Position AB2-051***

***Chesapeake 230kV  
765.5 MW Capacity / 884.5 MW Energy***

**June / 2017**

## Introduction

This System Impact Study (SIS) has been prepared in accordance with the PJM Open Access Transmission Tariff, Section 205, as well as the System Impact Study Agreement between Gilmerton Energy Center, LLC, the Interconnection Customer (IC) and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

## Preface

The intent of the System Impact Study is to determine a plan, with approximate cost and construction time estimates, to connect the subject generation interconnection project to the PJM network at a location specified by the IC. As a requirement for interconnection, the IC may be responsible for the cost of constructing Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system. All facilities required for interconnection of a generation interconnection project must be designed to meet the technical specifications (on PJM web site) for the appropriate transmission owner.

In some instances an IC may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection or merchant transmission upgrade, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the System Impact Study is performed.

The System Impact Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

## General

The IC has proposed a natural gas combined cycle generating facility located in the City of Chesapeake, VA. The installed facilities will have a total capability of 884.5 MW with 765.5 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is March 31, 2021. **This study does not imply an ITO commitment to this in-service date.**

## Point of Interconnection

AB2-051 will interconnect with the ITO transmission system via a new breaker bay that connects into the Chesapeake 230kV double breaker double bus.

### **Cost Summary**

The AB2-051 interconnection request will be responsible for the following costs:

<b>Description</b>	<b>Total Cost</b>
Attachment Facilities	\$1,800,000
Direct Connection Network Upgrades	\$3,000,000
Non Direct Connection Network Upgrades	\$0
Allocation for New System Upgrades	\$ 678,713.71
Contribution for Previously Identified Upgrades	\$0
<b>Total Costs</b>	<b>\$5,478,713.71</b>

## **Attachment Facilities**

Generation Substation: Install metering and associated Protection Equipment. Estimated Cost \$600,000.

Transmission: Construct approximately one span of 230 kV Attachment line between the generation substation and the existing Chesapeake 230 kV Substation. The estimated cost for this work is \$1,200,000.

The estimated total cost of the Attachment Facilities is \$1,800,000. It is estimated to take 18-24 months to complete this work. These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase. These costs do not include CIAC Tax Gross-up. The single line is shown below in Attachment 1.

## **Direct Connection Cost Estimate**

Substation: To reliably interconnect the proposed generation with the ITO Transmission System, it will be necessary to install two 230kV breakers and associated protection equipment to the existing Chesapeake Substation. The estimated cost of this work is \$3,000,000. This substation may also need to be expanded to accommodate the additional equipment and additional land and permitting may be required. It is estimated to take 24-36 months to complete this work.

## **Non-Direct Connection Cost Estimate**

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

## **New System Reinforcements**

PJM OATT 217.3 outlines cost responsibility for Network Upgrades and as the minimum amount of Network Upgrades required to resolve a single reliability criteria violation will not meet or exceed \$5,000,000 such costs shall be allocated to those Interconnection Requests in the New Services Queue that contribute to the need for such upgrades. Such allocations shall be made in proportion to each Interconnection Request's megawatt contribution to the need for these upgrades subject to the rules for minimum cost allocation thresholds in the PJM Manuals. For the purpose of applying the \$5,000,000 threshold, each reliability criteria violation shall be considered separately.

**Reinforcement: In order to mitigate the Chesterfield - Basin 230 kV line # 259 overload.**

Replace 0.14 miles of 1109 ACAR with a conductor which will increase the current line rating

by a minimum of 15% to approximately 550 MVA. Estimated cost \$250,000 and is estimated to take 15-18 months to Engineer, Permit and Construct.

Queue	MW contribution	Percentage of Cost	Cost(\$25M)	Contingency Name	Contingency Type
AB2-039	7.75	8.72%	\$21,799.05	LN 563'	single
AB2-051	48.08	54.10%	\$135,238.52	LN 563'	single
AB2-100	7.04	7.92%	\$19,801.98	LN 563'	single
AB2-128	6.03	6.78%	\$16,961.07	LN 563'	single
AB2-134	7.99	8.99%	\$22,474.12	LN 563'	single
AB2-190	11.99	13.49%	\$33,725.25	LN 563'	single

**Reinforcement: In order to mitigate the Elmont-Ladysmith 500 kV line overload.** Replace the wave trap to accommodate the proposed generation interconnection project. This work is estimated to take 20-24 months to complete based on typical permitting parameters and is estimated to cost \$700,000.

Queue	MW contribution	Percentage of Cost	Cost(\$0.70M)	Contingency Name	Contingency Type
AB2-051	241.35	34.78%	\$243,475.19	LN 576'	single
AB2-068	416.56	60.03%	\$420,227.99	LN 576'	single
AB2-190	35.98	5.19%	\$36,296.82	LN 576'	single

**Reinforcement: Replace Yadkin 230kV 210512 with 50kA breaker.** It is estimated to take 12 months to complete and it is estimated to cost \$300,000 to resolve this deficiency.

## Interconnection Customer Requirements

ITO's Facility Interconnection Requirements as posted on PJM's website

<http://www.pjm.com/~media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx>

An Interconnection Customer entering the New Services Queue on or after October 1, 2012 with a proposed new Customer Facility that has a Maximum Facility Output equal to or greater than 100 MW shall install and maintain, at its expense, phasor measurement units (PMUs). See Section 8.5.3 of Appendix 2 to the Interconnection Service Agreement as well as section 4.3 of PJM Manual 14D for additional information.

## Revenue Metering and SCADA Requirements

### **PJM Requirements**

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

## **Interconnected Transmission Owner Requirements**

Metering and SCADA/Communication equipment must meet the requirements outlined in section 3.1.6 Metering and Telecommunications of ITO's Facility Connection Requirement NERC Standard FAC-001 which is publically available at [www.dom.com](http://www.dom.com).

## Network Impacts

The Queue Project AB2-051 was evaluated as a 765.5 MW (Capacity 765.5 MW) injection at the Chesapeake 230kV substation in the ITO area. Project AB2-051 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AB2-051 was studied with a commercial probability of 100%. Potential network impacts were as follows:

### Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description
LN 208-259	CONTINGENCY 'LN 208-259' OPEN BRANCH FROM BUS 314286 TO BUS 314309 CKT 1 /* 6CHSTF A 230.00 - 6IRON208 230.00 OPEN BRANCH FROM BUS 314309 TO BUS 314338 CKT 1 /* 6IRON208 230.00 - 6SOUWEST 230.00 OPEN BUS 314309 /* ISLAND OPEN BRANCH FROM BUS 314276 TO BUS 314287 CKT 1 /* 6BASIN 230.00 - 6CHSTF B 230.00 END
LN 563	CONTINGENCY 'LN 563' OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /* 8CARSON 500.00 - 8MDLTHAN 500.00 END
LN 576	CONTINGENCY 'LN 576' OPEN BRANCH FROM BUS 314322 TO BUS 314914 CKT 1 /* 6MDLTHAN 230.00 - 8MDLTHAN 500.00 OPEN BRANCH FROM BUS 314914 TO BUS 314918 CKT 1 /* 8MDLTHAN 500.00 - 8NO ANNA 500.00 END

## Summer Peak Analysis – 2020

### Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
1	N-1	LN 563	DVP - DVP	6CHSTF B-6BASIN 230 kV line	314287	314276	1	AC	91.47	100.62	ER	449	48.08	1
2	N-1	LN 576	DVP - DVP	8ELMONT-8LDYSMTH 500 kV line	314908	314911	1	AC	77.6	85.92	ER	2442	241.35	2

### Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output).

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
3	DCTL	LN 208-259	DVP - DVP	6CHARCTY-6LAKESD 230 kV line	314225	314227	1	AC	97.24	104.29	LD	459	38.45	3

### Short Circuit

(Summary of impacted circuit breakers)

New circuit breakers found to be over-duty:

#	Area	Bus No.	Bus	Breaker	Rating Type	Duty Percent Without AB2-051	Duty Percent With AB2-051	Duty Percent Difference
4	DVP	777	YADKIN 2&4 230.kV	210512	S	95.02	108.95	13.94



Contributions to previously identified circuit breakers found to be over-duty:

None

### **Contribution to Previously Identified Overloads**

*(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)*

#	Contingency		Affected Area	Facility Description	Bus			Power Flow	Loading %		Rating		MW Contribution	Ref
	Type	Name			From	To	Cir.		Initial	Final	Type	MVA		
5	DCTL	LN 208-259	DVP - DVP	6MESSER-6CHARCTY 230 kV line	314228	314225	1	AC	108.36	115.4	LD	459	38.45	4
6	DCTL	LN 208-259	DVP - DVP	6CHSTF B-6MESSER 230 kV line	314287	314228	1	AC	108.39	115.43	LD	459	38.45	5

### **Steady-State Voltage Requirements**

*(Summary of the VAR requirements based upon the results of the steady-state voltage studies)*

None

### **Stability and Reactive Power Requirement for Low Voltage Ride Through**

*(Summary of the VAR requirements based upon the results of the dynamic studies)*

No mitigations required

### **New System Reinforcements**

*(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this interconnection request)*

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost	AB2-051 Allocation
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Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost	AB2-051 Allocation																					
# 1	6CHSTF B-6BASIN 230 kV line	<div>Replace 0.14 miles of 1109 ACAR with a conductor which will increase the current line rating by a minimum of 15% to approximately 550 MVA. Estimated to take 15-18 months to Engineer, Permit and Construct</div> <table><tr><th>Queue</th><th>Impact (MW)</th><th>Cost</th></tr><tr><td>AB2-039</td><td>7.75</td><td>\$21,799.05</td></tr><tr><td>AB2-051</td><td>48.08</td><td>\$135,238.52</td></tr><tr><td>AB2-100</td><td>7.04</td><td>\$19,801.98</td></tr><tr><td>AB2-128</td><td>6.03</td><td>\$16,961.07</td></tr><tr><td>AB2-134</td><td>7.99</td><td>\$22,474.12</td></tr><tr><td>AB2-190</td><td>11.99</td><td>\$33,725.25</td></tr></table>	Queue	Impact (MW)	Cost	AB2-039	7.75	\$21,799.05	AB2-051	48.08	\$135,238.52	AB2-100	7.04	\$19,801.98	AB2-128	6.03	\$16,961.07	AB2-134	7.99	\$22,474.12	AB2-190	11.99	\$33,725.25	Pending	\$250,000	\$135,238.52
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AB2-134	7.99	\$22,474.12																								
AB2-190	11.99	\$33,725.25																								
# 2	8ELMONT-8LDYSMTH 500 kV line	<div>Replace the wave trap to accommodate the proposed generation interconnection project. This work is estimated to take 20-24 months to complete based on typical permitting parameters</div> <table><tr><th>Queue</th><th>Impact (MW)</th><th>Cost</th></tr><tr><td>AB2-051</td><td>241.35</td><td>\$243,475.19</td></tr><tr><td>AB2-068</td><td>416.56</td><td>\$420,227.99</td></tr><tr><td>AB2-190</td><td>35.98</td><td>\$36,296.82</td></tr></table>	Queue	Impact (MW)	Cost	AB2-051	241.35	\$243,475.19	AB2-068	416.56	\$420,227.99	AB2-190	35.98	\$36,296.82	Pending	\$700,000	\$243,475.19									
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AB2-190	35.98	\$36,296.82																								
# 3	6CHARCTY-6LAKESD 230 kV line	Rebuild 21.32 miles of the Chesterfield - Lakeside 230kV transmission line by 6/1/2020	b2745	Not Applicable																						
# 4	Yadkin 230kV breaker 210512	Replace 230kV breaker with a 50kA duty	Pending	\$300,000	\$300,000																					
Total New Network Upgrades					\$678,713.71																					

### **Contribution to Previously Identified System Reinforcements**

*(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which is calculated and reported for in the Impact Study)*

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost	AB2-051 Allocation
# 5	6MESSER-6CHARCTY 230 kV line	Rebuild 21.32 miles of the Chesterfield - Lakeside 230kV transmission line by 6/1/2020	b2745	Not Applicable	
# 6	6CHSTF B-6MESSER 230 kV line				
Total New Network Upgrades					\$0

### **Potential Congestion due to Local Energy Deliverability**

*PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.*

*Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this interconnection request by addressing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.*

Not applicable

### **Light Load Analysis in 2020**

None

### **ITO Analysis**

ITO assessed the impact of the proposed Queue Project #AB2-051 interconnection of 765.5 MW of energy (Capacity 765.5 MW) for compliance with reliability criteria on ITO’s Transmission System. The system was assessed using the summer 2020 RTEP case provided to ITO by PJM. When performing a generation analysis, ITO’s main analysis will be load flow study results under single contingency and multiple facility contingency (both normal and stressed system conditions). ITO Criteria considers a transmission facility overloaded if it exceeds 94% of its emergency rating under normal and stressed system conditions. A full listing of ITO’s Planning Criteria and interconnection requirements can be found in the ITO’s Facility Connection Requirements which are publicly available at: <http://www.dom.com>.

The results of these studies evaluate the system under a limited set of operating conditions and do not guarantee the full delivery of the capacity and associated energy of this proposed interconnection request under all operating conditions. NERC Planning and Operating Reliability Criteria allow for the re-dispatch of generating units to resolve projected and actual deficiencies in real time and planning studies. Specifically NERC Category C Contingency Conditions ( Bus Fault, Tower Line, N-1-1, and Stuck Breaker scenarios) allow for re-dispatch of generating units to resolve potential reliability deficiencies. For ITO Planning Criteria the re-dispatch of generating units for these contingency conditions is allowed as long as the projected loading does not exceed 100% of a facility Load Dump Rating.

As part of its generation impact analysis ITO routinely evaluates the impact that a proposed new generation resource will have under maximum generation conditions, stress system conditions and import/export system conditions (greater than 20 MW). The results of these studies are discussed in more detail below.

Category B Analysis (Single Contingency):

- System Normal – Same as PJM Analysis
- Critical System Condition (No Surry 230 kV Unit) – Same as PJM Analysis.

Category C Analysis: (Multiple Facility Contingency)

- Bus Fault - Same as PJM Analysis
- Line Stuck Breaker - Same as PJM Analysis
- Tower Line – Same as PJM Analysis

As part of its generation impact analysis ITO routinely evaluates the impact that a proposed new generation resource (greater than 20 MW) will have under maximum generation conditions, stress system conditions and import/export system conditions. The results of these studies are discussed in Table A and B below.

Table A: Import Study Results

Import Study Results
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Area	Summer 2020	Summer 2020 with AB2-051	Limiting Element
AEP	2000+	2000+	None
APS	2000+	2000+	None
CPL	2000+	2000+	None
PJM	2000+	2000+	None

Table B: Export Study Results

Export Study Results			
Area	Summer 2020	Summer 2020 with AB2-051	Limiting Element
AEP	2000+	2000+	None
APS	2000+	2000+	None
CPL	2000+	2000+	None
PJM	2000+	2000+	None

ITO's Planning Criteria indicates a need to have approximately 2000 MW of import and export capability. The results of these import and export studies indicate that the proposed AB2-051 (Transfer) will not impact ITO's import or export capability

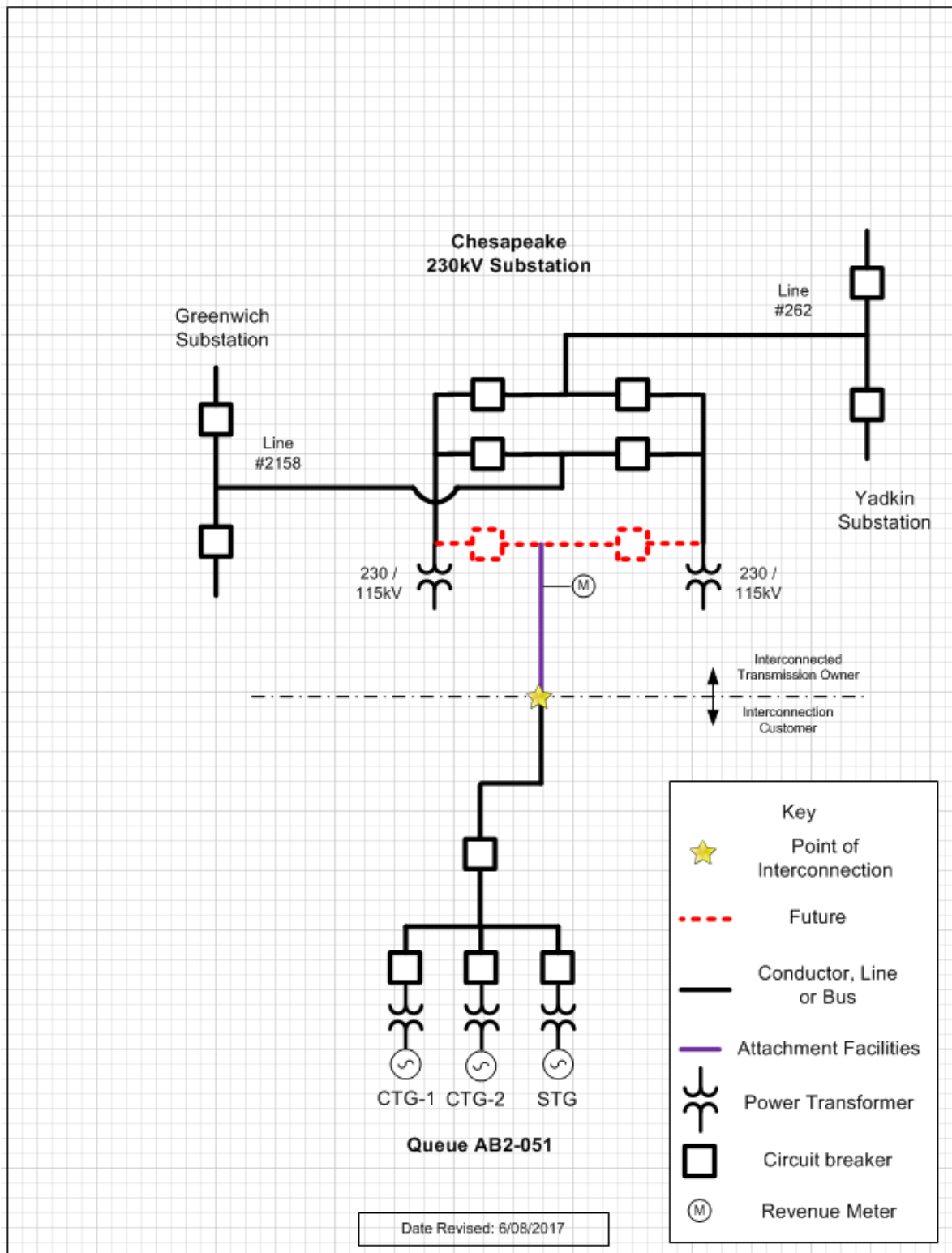
## **Affected System Analysis & Mitigation**

### **Duke Energy:**

Nothing identified

# Attachment 1.

## System Configuration



## **Appendices**

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact.

It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.



## **Appendix 1**

(DVP - DVP) The 6CHSTF B-6BASIN 230 kV line (from bus 314287 to bus 314276 ckt 1) loads from 91.47% to 100.62% (AC power flow) of its emergency rating (449 MVA) for the single line contingency outage of 'LN 563'. This project contributes approximately 48.08 MW to the thermal violation.

CONTINGENCY 'LN 563'

OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 /\* 8CARSON  
500.00 - 8MDLTHAN 500.00  
END

Bus Number	Bus Name	Full Contribution
315065	1CHESTF6	39.53
315139	1GASTONA	1.88
315141	1GASTONB	1.88
315119	1GRAVEL3	1.49
315120	1GRAVEL4	1.5
315121	1GRAVEL5	1.48
315122	1GRAVEL6	1.5
315117	1GRAVELC	0.51
315077	1HOPHCF1	2.13
315078	1HOPHCF2	2.13
315079	1HOPHCF3	2.13
315080	1HOPHCF4	3.23
315076	1HOPPOLC	1.82
315116	1SURRY 1	15.61
314314	3LOCKS	0.98
315074	CIR_AB2-152	0.84
315075	CIR_AB2-152	0.83
902241	W2-022 C OP1	0.61
914231	Y2-077	0.86
921092	AA1-049 C	0.84
921532	AA1-132 C	2.61
921542	AA1-133 C	3.47
921552	AA1-134 C	3.54
921562	AA1-135 C	3.61
921572	AA1-138 C	3.62
921752	AA2-053 C	3.84
921762	AA2-057 C	2.87
921772	AA2-059 C	0.88
921862	AA2-068 C	0.92
921982	AA2-088 C	2.7

922442	AA2-165 C	0.39
922472	AA2-169 C	0.85
922512	AA2-174 C	0.18
922522	AA2-177 C	6.
922532	AA2-178 C	3.61
922602	AB1-013 C	1.09
922722	AB1-053 C	0.51
922922	AB1-081 C OP	3.44
923262	AB1-132 C OP	6.97
923572	AB1-173 C OP	1.14
923582	AB1-173AC OP	1.14
923801	AB2-015 C OP	3.5
923831	AB2-022 C	0.81
923851	AB2-025 C	1.8
923911	AB2-031 C OP	1.13
923941	AB2-035 C	0.13
923981	AB2-039 C OP	7.75
923991	AB2-040 C OP	3.71
924071	AB2-051 C OP	48.08
924151	AB2-059 C	4.05
924381	AB2-087 C	0.23
924391	AB2-088 C	0.17
924491	AB2-098 C	0.21
924501	AB2-099 C	0.24
924511	AB2-100 C	7.04
924761	AB2-128 C	6.03
924811	AB2-134 C OP	7.99
924931	AB2-147 C	1.38
924941	AB2-149 C OP	1.72
924951	AB2-150 C OP	1.38
925051	AB2-160 C OP	3.91
925061	AB2-161 C OP	3.13
925141	AB2-171 C OP	2.01
925171	AB2-174 C OP	3.66
925281	AB2-186 C	0.22
925291	AB2-188 C OP	0.89
925331	AB2-190 C	12.

## **Appendix 2**

(DVP - DVP) The 8ELMONT-8LDYSMTH 500 kV line (from bus 314908 to bus 314911 ckt 1) loads from 77.6% to 85.92% (AC power flow) of its emergency rating (2442 MVA) for the single line contingency outage of 'LN 576'. This project contributes approximately 241.35 MW to the thermal violation.

### CONTINGENCY 'LN 576'

OPEN BRANCH FROM BUS 314322 TO BUS 314914 CKT 1 /\* 6MDLTHAN  
230.00 - 8MDLTHAN 500.00

OPEN BRANCH FROM BUS 314914 TO BUS 314918 CKT 1 /\* 8MDLTHAN  
500.00 - 8NO ANNA 500.00

END

Bus Number	Bus Name	Full Contribution
315058	1CHESTF3	6.7
315059	1CHESTF4	10.85
315060	1CHESTF5	23.01
315061	1CHESTG7	9.02
315063	1CHESTG8	8.94
315062	1CHESTS7	4.1
315064	1CHESTS8	4.58
315067	1DARBY 1	5.88
315068	1DARBY 2	5.88
315069	1DARBY 3	5.96
315070	1DARBY 4	5.96
315233	1SURRY 2	58.46
315091	1YORKTN2	53.69
315092	1YORKTN3	52.8
314309	6IRON208	0.88
314236	6NRTHEST	0.42
314251	6S PUMP	1.79
297087	V2-040	0.28
902241	W2-022 C OP1	2.57
LTF	Z2-067	28.75
921092	AA1-049 C	4.22
LTF	AA1-058	1.25
921172	AA1-064 C	13.27
921532	AA1-132 C	13.04
921542	AA1-133 C	17.45
921552	AA1-134 C	17.02
921562	AA1-135 C	14.68

921572	AA1-138 C	16.68
921752	AA2-053 C	13.8
921762	AA2-057 C	10.83
921772	AA2-059 C	4.03
921862	AA2-068 C	3.44
LTF	AA2-074	8.44
921982	AA2-088 C	10.62
922442	AA2-165 C	1.48
922472	AA2-169 C	3.33
922512	AA2-174 C	0.63
922522	AA2-177 C	17.99
922532	AA2-178 C	16.09
922602	AB1-013 C	4.86
922682	AB1-027 C	4.79
922722	AB1-053 C	1.67
922922	AB1-081 C OP	13.26
923262	AB1-132 C OP	22.23
923272	AB1-135 C OP	4.79
923572	AB1-173 C OP	3.57
923582	AB1-173AC OP	3.57
923801	AB2-015 C OP	14.44
923831	AB2-022 C	3.99
923841	AB2-024 C	4.41
923851	AB2-025 C	4.02
923861	AB2-026 C	3.55
923911	AB2-031 C OP	3.55
923941	AB2-035 C	0.51
923981	AB2-039 C OP	14.69
923991	AB2-040 C OP	11.64
924061	AB2-050	4.83
924071	AB2-051 C OP	241.35
924151	AB2-059 C	15.62
924241	AB2-068 OP	416.56
LTF	AB2-075	4.54
LTF	AB2-076	5.35
924381	AB2-087 C	0.92
924391	AB2-088 C	0.65
924401	AB2-089 C	3.11
924491	AB2-098 C	0.88
924501	AB2-099 C	0.95
924511	AB2-100 C	18.54
924761	AB2-128 C	15.89
924811	AB2-134 C OP	23.09
924931	AB2-147 C	4.05
924941	AB2-149 C OP	5.87

924951	AB2-150 C OP	4.05
925051	AB2-160 C OP	9.59
925061	AB2-161 C OP	5.94
925141	AB2-171 C OP	8.13
925171	AB2-174 C OP	11.16
925281	AB2-186 C	1.03
925291	AB2-188 C OP	3.97
925331	AB2-190 C	35.99

### **Appendix 3**

(DVP - DVP) The 6CHARCTY-6LAKESD 230 kV line (from bus 314225 to bus 314227 ckt 1) loads from 97.24% to 104.29% (AC power flow) of its load dump rating (459 MVA) for the tower line contingency outage of 'LN 208-259'. This project contributes approximately 38.45 MW to the thermal violation.

CONTINGENCY 'LN 208-259'

OPEN BRANCH FROM BUS 314286 TO BUS 314309 CKT 1 /\* 6CHSTF A  
230.00 - 6IRON208 230.00

OPEN BRANCH FROM BUS 314309 TO BUS 314338 CKT 1 /\* 6IRON208  
230.00 - 6SOUWEST 230.00

OPEN BUS 314309 /\* ISLAND

OPEN BRANCH FROM BUS 314276 TO BUS 314287 CKT 1 /\* 6BASIN 230.00 -  
6CHSTF B 230.00

END

Bus Number	Bus Name	Full Contribution
315065	1CHESTF6	39.27
315077	1HOPHCF1	2.28
315078	1HOPHCF2	2.28
315079	1HOPHCF3	2.28
315080	1HOPHCF4	3.46
315076	1HOPPOLC	1.95
315073	1STONECA	5.71
314784	1WEYRHSB	0.64
314539	3UNCAMP	0.81
314541	3WATKINS	0.23
314229	6MT R221	-0.33
315074	CIR_AB2-152	0.89
315075	CIR_AB2-152	0.88
292791	U1-032 E	2.97
900672	V4-068 E	0.1
901082	W1-029E	13.15
902241	W2-022 C OP1	0.49
902242	W2-022 E OP1	3.26
907092	X1-038 E	2.02
914231	Y2-077	0.92
916042	Z1-036 E	13.29
917332	Z2-043 E	0.34
917342	Z2-044 E	0.18
917592	Z2-099 E	0.15

921163	AA1-063AE	1.48
918512	AA1-065 E OP	1.46
918562	AA1-072 E	0.06
921552	AA1-134 C	2.82
921553	AA1-134 E	1.21
921562	AA1-135 C	2.91
921563	AA1-135 E	1.25
921572	AA1-138 C	2.92
921573	AA1-138 E	1.25
921752	AA2-053 C	3.22
921753	AA2-053 E	1.38
921762	AA2-057 C	2.32
921763	AA2-057 E	1.16
921772	AA2-059 C	0.7
921773	AA2-059 E	0.32
921862	AA2-068 C	0.75
921863	AA2-068 E	0.35
920022	AA2-086 E	0.08
921982	AA2-088 C	2.24
921983	AA2-088 E	3.66
922442	AA2-165 C	0.32
922443	AA2-165 E	0.15
922472	AA2-169 C	0.7
922473	AA2-169 E	0.32
922512	AA2-174 C	0.15
922513	AA2-174 E	0.16
922522	AA2-177 C	6.12
922523	AA2-177 E	2.62
922532	AA2-178 C	2.9
922533	AA2-178 E	1.24
922602	AB1-013 C	0.88
922603	AB1-013 E	5.86
922722	AB1-053 C	0.44
922723	AB1-053 E	0.24
923262	AB1-132 C OP	5.95
923263	AB1-132 E OP	2.55
923572	AB1-173 C OP	0.98
923573	AB1-173 E OP	0.46
923582	AB1-173AC OP	0.98
923583	AB1-173AE OP	0.46
923801	AB2-015 C OP	2.9
923802	AB2-015 E OP	2.38
923851	AB2-025 C	1.64
923852	AB2-025 E	0.74
923911	AB2-031 C OP	0.97

923912	AB2-031 E OP	0.48
923981	AB2-039 C OP	7.68
923982	AB2-039 E OP	6.21
923991	AB2-040 C OP	3.2
923992	AB2-040 E OP	2.62
924071	AB2-051 C OP	38.45
924381	AB2-087 C	0.19
924382	AB2-087 E	0.09
924501	AB2-099 C	0.2
924502	AB2-099 E	0.09
924511	AB2-100 C	6.23
924512	AB2-100 E	3.07
924761	AB2-128 C	5.34
924762	AB2-128 E	2.1
924811	AB2-134 C OP	8.22
924812	AB2-134 E OP	8.08
924931	AB2-147 C	1.21
924932	AB2-147 E	1.97
924941	AB2-149 C OP	1.54
924942	AB2-149 E OP	2.51
924951	AB2-150 C OP	1.21
924952	AB2-150 E OP	1.97
925051	AB2-160 C OP	4.25
925052	AB2-160 E OP	6.93
925061	AB2-161 C OP	3.11
925062	AB2-161 E OP	5.07
925122	AB2-169 E	1.77
925141	AB2-171 C OP	1.67
925142	AB2-171E OP	2.72
925171	AB2-174 C OP	3.17
925172	AB2-174 E OP	2.87
925281	AB2-186 C	0.18
925282	AB2-186 E	0.08
925291	AB2-188 C OP	0.72
925292	AB2-188 E OP	0.32
925331	AB2-190 C	12.24
925332	AB2-190 E	5.25



## **Appendix 4**

(DVP - DVP) The 6MESSER-6CHARCTY 230 kV line (from bus 314228 to bus 314225 ckt 1) loads from 108.36% to 115.4% (AC power flow) of its load dump rating (459 MVA) for the tower line contingency outage of 'LN 208-259'. This project contributes approximately 38.45 MW to the thermal violation.

CONTINGENCY 'LN 208-259'

OPEN BRANCH FROM BUS 314286 TO BUS 314309 CKT 1 /\* 6CHSTF A  
230.00 - 6IRON208 230.00

OPEN BRANCH FROM BUS 314309 TO BUS 314338 CKT 1 /\* 6IRON208  
230.00 - 6SOUWEST 230.00

OPEN BUS 314309 /\* ISLAND

OPEN BRANCH FROM BUS 314276 TO BUS 314287 CKT 1 /\* 6BASIN 230.00 -  
6CHSTF B 230.00

END

Bus Number	Bus Name	Full Contribution
315065	1CHESTF6	39.27
315077	1HOPHCF1	2.28
315078	1HOPHCF2	2.28
315079	1HOPHCF3	2.28
315080	1HOPHCF4	3.46
315076	1HOPPOLC	1.95
315073	1STONECA	5.71
314784	1WEYRHSB	0.64
314539	3UNCAMP	0.81
314541	3WATKINS	0.23
314229	6MT R221	-0.33
315074	CIR_AB2-152	0.89
315075	CIR_AB2-152	0.88
292791	U1-032 E	2.97
900672	V4-068 E	0.1
901082	W1-029E	13.15
902241	W2-022 C OP1	0.49
902242	W2-022 E OP1	3.26
907092	X1-038 E	2.02
914231	Y2-077	0.92
916042	Z1-036 E	13.29
917332	Z2-043 E	0.34
917342	Z2-044 E	0.18
917592	Z2-099 E	0.15

921163	AA1-063AE	1.48
918512	AA1-065 E OP	1.46
918562	AA1-072 E	0.06
921552	AA1-134 C	2.82
921553	AA1-134 E	1.21
921562	AA1-135 C	2.91
921563	AA1-135 E	1.25
921572	AA1-138 C	2.92
921573	AA1-138 E	1.25
921752	AA2-053 C	3.22
921753	AA2-053 E	1.38
921762	AA2-057 C	2.32
921763	AA2-057 E	1.16
921772	AA2-059 C	0.7
921773	AA2-059 E	0.32
921862	AA2-068 C	0.75
921863	AA2-068 E	0.35
920022	AA2-086 E	0.08
921982	AA2-088 C	2.24
921983	AA2-088 E	3.66
922442	AA2-165 C	0.32
922443	AA2-165 E	0.15
922472	AA2-169 C	0.7
922473	AA2-169 E	0.32
922512	AA2-174 C	0.15
922513	AA2-174 E	0.16
922522	AA2-177 C	6.12
922523	AA2-177 E	2.62
922532	AA2-178 C	2.9
922533	AA2-178 E	1.24
922602	AB1-013 C	0.88
922603	AB1-013 E	5.86
922722	AB1-053 C	0.44
922723	AB1-053 E	0.24
923262	AB1-132 C OP	5.95
923263	AB1-132 E OP	2.55
923572	AB1-173 C OP	0.98
923573	AB1-173 E OP	0.46
923582	AB1-173AC OP	0.98
923583	AB1-173AE OP	0.46
923801	AB2-015 C OP	2.9
923802	AB2-015 E OP	2.38
923851	AB2-025 C	1.64
923852	AB2-025 E	0.74
923911	AB2-031 C OP	0.97

923912	AB2-031 E OP	0.48
923981	AB2-039 C OP	7.68
923982	AB2-039 E OP	6.21
923991	AB2-040 C OP	3.2
923992	AB2-040 E OP	2.62
924071	AB2-051 C OP	38.45
924381	AB2-087 C	0.19
924382	AB2-087 E	0.09
924501	AB2-099 C	0.2
924502	AB2-099 E	0.09
924511	AB2-100 C	6.23
924512	AB2-100 E	3.07
924761	AB2-128 C	5.34
924762	AB2-128 E	2.1
924811	AB2-134 C OP	8.22
924812	AB2-134 E OP	8.08
924931	AB2-147 C	1.21
924932	AB2-147 E	1.97
924941	AB2-149 C OP	1.54
924942	AB2-149 E OP	2.51
924951	AB2-150 C OP	1.21
924952	AB2-150 E OP	1.97
925051	AB2-160 C OP	4.25
925052	AB2-160 E OP	6.93
925061	AB2-161 C OP	3.11
925062	AB2-161 E OP	5.07
925122	AB2-169 E	1.77
925141	AB2-171 C OP	1.67
925142	AB2-171E OP	2.72
925171	AB2-174 C OP	3.17
925172	AB2-174 E OP	2.87
925281	AB2-186 C	0.18
925282	AB2-186 E	0.08
925291	AB2-188 C OP	0.72
925292	AB2-188 E OP	0.32
925331	AB2-190 C	12.24
925332	AB2-190 E	5.25

## **Appendix 5**

(DVP - DVP) The 6CHSTF B-6MESSER 230 kV line (from bus 314287 to bus 314228 ckt 1) loads from 108.39% to 115.43% (AC power flow) of its load dump rating (459 MVA) for the tower line contingency outage of 'LN 208-259'. This project contributes approximately 38.45 MW to the thermal violation.

CONTINGENCY 'LN 208-259'

OPEN BRANCH FROM BUS 314286 TO BUS 314309 CKT 1 /\* 6CHSTF A  
230.00 - 6IRON208 230.00

OPEN BRANCH FROM BUS 314309 TO BUS 314338 CKT 1 /\* 6IRON208  
230.00 - 6SOUWEST 230.00

OPEN BUS 314309 /\* ISLAND

OPEN BRANCH FROM BUS 314276 TO BUS 314287 CKT 1 /\* 6BASIN 230.00 -  
6CHSTF B 230.00

END

Bus Number	Bus Name	Full Contribution
315065	1CHESTF6	39.27
315077	1HOPHCF1	2.28
315078	1HOPHCF2	2.28
315079	1HOPHCF3	2.28
315080	1HOPHCF4	3.46
315076	1HOPPOLC	1.95
315073	1STONECA	5.71
314784	1WEYRHSB	0.64
314539	3UNCAMP	0.81
314541	3WATKINS	0.23
314229	6MT R221	-0.33
315074	CIR_AB2-152	0.89
315075	CIR_AB2-152	0.88
292791	U1-032 E	2.97
900672	V4-068 E	0.1
901082	W1-029E	13.15
902241	W2-022 C OP1	0.49
902242	W2-022 E OP1	3.26
907092	X1-038 E	2.02
914231	Y2-077	0.92
916042	Z1-036 E	13.29
917332	Z2-043 E	0.34
917342	Z2-044 E	0.18
917592	Z2-099 E	0.15

921163	AA1-063AE	1.48
918512	AA1-065 E OP	1.46
918562	AA1-072 E	0.06
921552	AA1-134 C	2.82
921553	AA1-134 E	1.21
921562	AA1-135 C	2.91
921563	AA1-135 E	1.25
921572	AA1-138 C	2.92
921573	AA1-138 E	1.25
921752	AA2-053 C	3.22
921753	AA2-053 E	1.38
921762	AA2-057 C	2.32
921763	AA2-057 E	1.16
921772	AA2-059 C	0.7
921773	AA2-059 E	0.32
921862	AA2-068 C	0.75
921863	AA2-068 E	0.35
920022	AA2-086 E	0.08
921982	AA2-088 C	2.24
921983	AA2-088 E	3.66
922442	AA2-165 C	0.32
922443	AA2-165 E	0.15
922472	AA2-169 C	0.7
922473	AA2-169 E	0.32
922512	AA2-174 C	0.15
922513	AA2-174 E	0.16
922522	AA2-177 C	6.12
922523	AA2-177 E	2.62
922532	AA2-178 C	2.9
922533	AA2-178 E	1.24
922602	AB1-013 C	0.88
922603	AB1-013 E	5.86
922722	AB1-053 C	0.44
922723	AB1-053 E	0.24
923262	AB1-132 C OP	5.95
923263	AB1-132 E OP	2.55
923572	AB1-173 C OP	0.98
923573	AB1-173 E OP	0.46
923582	AB1-173AC OP	0.98
923583	AB1-173AE OP	0.46
923801	AB2-015 C OP	2.9
923802	AB2-015 E OP	2.38
923851	AB2-025 C	1.64
923852	AB2-025 E	0.74
923911	AB2-031 C OP	0.97

923912	AB2-031 E OP	0.48
923981	AB2-039 C OP	7.68
923982	AB2-039 E OP	6.21
923991	AB2-040 C OP	3.2
923992	AB2-040 E OP	2.62
924071	AB2-051 C OP	38.45
924381	AB2-087 C	0.19
924382	AB2-087 E	0.09
924501	AB2-099 C	0.2
924502	AB2-099 E	0.09
924511	AB2-100 C	6.23
924512	AB2-100 E	3.07
924761	AB2-128 C	5.34
924762	AB2-128 E	2.1
924811	AB2-134 C OP	8.22
924812	AB2-134 E OP	8.08
924931	AB2-147 C	1.21
924932	AB2-147 E	1.97
924941	AB2-149 C OP	1.54
924942	AB2-149 E OP	2.51
924951	AB2-150 C OP	1.21
924952	AB2-150 E OP	1.97
925051	AB2-160 C OP	4.25
925052	AB2-160 E OP	6.93
925061	AB2-161 C OP	3.11
925062	AB2-161 E OP	5.07
925122	AB2-169 E	1.77
925141	AB2-171 C OP	1.67
925142	AB2-171E OP	2.72
925171	AB2-174 C OP	3.17
925172	AB2-174 E OP	2.87
925281	AB2-186 C	0.18
925282	AB2-186 E	0.08
925291	AB2-188 C OP	0.72
925292	AB2-188 E OP	0.32
925331	AB2-190 C	12.24
925332	AB2-190 E	5.25