Generation Interconnection System Impact Study Report

For

PJM Generation Interconnection Request Queue Position AD1-151

Hopewell-Surry 230kV 90 MW Capacity / 150 MW Energy

> Revision 6/ October 2022 Revision 5/ September 2022 Revision 4/ May 2022 Revision 3 / April 2022 Revision 2 / January 2022 Revision 1 / November 2021 March 2019

Introduction

This System Impact Study (SIS) has been prepared in accordance with the PJM Open Access Transmission Tariff, Section 205, as well as the System Impact Study Agreement between Loblolly Solar, LLC, the Interconnection Customer (IC) and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

Preface

The intent of the System Impact Study is to determine a plan, with approximate cost and construction time estimates, to connect the subject generation interconnection project to the PJM network at a location specified by the IC. As a requirement for interconnection, the IC may be responsible for the cost of constructing Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system. All facilities required for interconnection of a generation interconnection project must be designed to meet the technical specifications (on PJM web site) for the appropriate transmission owner. In some instances an IC may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection or merchant transmission upgrade, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the System Impact Study is performed.

The System Impact Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The IC is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

Revision 1 (November 2021) Summary

This revision is being issued to incorporate results of a re-tool performed in November of 2021.

Revision 2 (January 2022) Summary

This revision is being issued to incorporate results of a re-tool performed in January of 2022. This retool was needed to account for the withdrawal of AC1-107.

Revision 3 (April 2022) Summary

This revision is being issued to incorporate results of short circuit impacts of the Prince George – Poe 230 kV line reinforcement.

Revision 4 (May 2022) Summary

This revision is being issued to incorporate results of a re-tool performed in May of 2022. This retool was needed to account for the withdrawal of AD1-023.

Revision 5 (September 2022) Summary

This revision is being issued to reflect costs changes included in the Facilities Study for the project.

Revision 6 (October 2022) Summary

This revision is being issued to reflect updated analysis driven by model corrections.

General

The IC has proposed a solar generating facility located in Surry County, Virginia. The installed AD1-151 facilities will have a total capability of 150 MW with 90 MW of this output being recognized by PJM as capacity. The proposed in-service date for this project is December 31, 2020. **This study does not imply an ITO commitment to this in-service date.**

Point of Interconnection

AD1-151 will interconnect with the ITO transmission system via a new three breaker ring bus switching station that connects the Hopewell-Surry 230kV line.

Cost Summary

The AD1-151 interconnection request will be responsible for the following costs:

Description	Total Cost
Attachment Facilities	\$ 641,535
Direct Connection Network Upgrades	\$ 6,334,455
Non Direct Connection Network Upgrades	\$ 1,473,092
Allocation for New System Upgrades	\$ 0
Contribution for Previously Identified	\$ 0
Upgrades	
Total Costs	\$ 8,449,082

Attachment Facilities

<u>Generation Substation:</u> Install metering and associated protection equipment. Estimated Cost \$641,535.

The estimated total cost of the Attachment Facilities is \$1,800,000. It is estimated to take 18-24 months to complete this work upon execution of an Interconnection Construction Service Agreement (ICSA). These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase.

Direct Connection Cost Estimate

<u>Substation:</u> Establish the new 230 kV AD1-151 Switching Substation (interconnection substation). The estimated cost of this work scope is \$6,334,455. It is estimated to take 24-36 months to complete this work upon execution of an Interconnection Construction Service Agreement.

Non-Direct Network Upgrades:

<u>Transmission</u>: Install transmission structure in-line with transmission line to allow the proposed interconnection switching station to be interconnected with the transmission system. Estimated cost is \$1,361,288 and is estimated to take 24-30 months to complete.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

Note: Cost of remote changes at Colonial Trail and Hopewell substations as will be included in the facilities study report is \$111,804.

Incremental Capacity Transfer Rights

The network upgrades outlined in this report do not increase the CETL in the 2021/22 BRA case.

Interconnection Customer Requirements

ITO's Facility Interconnection Requirements as posted on PJM's website http://www.pjm.com/~/media/planning/plan-standards/private-dominion/facility-connection-requirements1.ashx

An Interconnection Customer entering the New Services Queue on or after October 1, 2012 with a proposed new Customer Facility that has a Maximum Facility Output equal to or greater than

100 MW shall install and maintain, at its expense, phasor measurement units (PMUs). See Section 8.5.3 of Appendix 2 to the Interconnection Service Agreement as well as section 4.3 of PJM Manual 14D for additional information.

Voltage Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for voltages and times as specified for the Eastern Interconnection in Attachment 1 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low voltage conditions, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Frequency Ride Through Requirements - The Customer Facility shall be designed to remain in service (not trip) for frequencies and times as specified in Attachment 2 of NERC Reliability Standard PRC-024-1, and successor Reliability Standards, for both high and low frequency condition, irrespective of generator size, subject to the permissive trip exceptions established in PRC-024-1 (and successor Reliability Standards).

Reactive Power - The Generation Interconnection Customer shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading to 0.95 lagging measured at the generator's terminals.

Meteorological Data Reporting Requirement - The solar generation facility shall, at a minimum, be required to provide the Transmission Provider with site-specific meteorological data including:

- Temperature (degrees Fahrenheit)
- Atmospheric pressure (hectopascals)
- Irradiance
- Forced outage data

Revenue Metering and SCADA Requirements

PJM Requirements

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Sections 24.1 and 24.2.

Interconnected Transmission Owner Requirements

Metering and SCADA/Communication equipment must meet the requirements outlined in section 3.1.6 Metering and Telecommunications of ITO's Facility Connection Requirement NERC Standard FAC-001 which is publically available at www.dom.com.

Summer Peak Analysis – 2021

The Queue Project AD1-151 was evaluated as a 150.0 MW (Capacity 90.0 MW) injection into Hopewell-Surry 230kV in the ITO area. Project AD1-151 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AD1-151 was studied with a commercial probability of 100%. Potential network impacts were as follows:

Contingency Descriptions

The following contingencies resulted in overloads:

Contingency Name	Description	
DVP_P1-2: LN 211	CONTINGENCY 'DVP_P1-2: LN 211' OPEN BRANCH FROM BUS 314287 TO BUS 314303 CKT 1 230.00 - 6HOPEWLL 230.00	/* 6CHSTF B
DVP_P1-2: LN 217	END CONTINGENCY 'DVP_P1-2: LN 217' OPEN BRANCH FROM BUS 314225 TO BUS 314227 CKT 1 230.00 - 6LAKESD 230.00 OPEN BRANCH FROM BUS 314225 TO BUS 314287 CKT 1 230.00 - 6CHSTF B 230.00 OPEN BUS 314225 /* ISLAND END	
DVP_P1-2: LN 228	CONTINGENCY 'DVP_P1-2: LN 228' OPEN BRANCH FROM BUS 314278 TO BUS 314286 CKT 1 6BERMUDA 230.00 - 6CHSTF A 230.00 OPEN BRANCH FROM BUS 314278 TO BUS 314303 CKT 1 6BERMUDA 230.00 - 6HOPEWLL 230.00 OPEN BUS 314278 /* ISLAND END	/* /*

	CONTINGENCY 'DVP_P1-2: LN 563'		
DVP_P1-2: LN 563	OPEN BRANCH FROM BUS 314902 TO BUS 314914 CKT 1 500.00 - 8MDLTHAN 500.00		/* 8CARSON
	END		
	CONTINGENCY 'DVP_P1-2: LN 574'		
DVP_P1-2: LN 574	OPEN BRANCH FROM BUS 314908 TO BUS 314911 CKT 1 500.00 - 8LDYSMTH 500.00		/* 8ELMONT
	END		
	CONTINGENCY 'DVP_P1-2: LN 575'		
DVP_P1-2: LN 575	OPEN BRANCH FROM BUS 314911 TO BUS 314918 CKT 1 500.00 - 8NO ANNA 500.00		/* 8LDYSMTH
	END		
	CONTINGENCY 'DVP_P1-2: LN 576'		
DVP_P1-2: LN 576	OPEN BRANCH FROM BUS 314914 TO BUS 314918 CKT 1 500.00 - 8NO ANNA 500.00		/* 8MDLTHAN
	END		
	CONTINGENCY 'DVP_P1-2: LN 594'		
DVP_P1-2: LN 594	OPEN BRANCH FROM BUS 314916 TO BUS 314934 CKT 1 8MORRSVL 500.00 - 8SPOTSYL 500.00		/*
	END		
	CONTINGENCY 'DVP_P4-2: 211T2124'	/*_ HOPE	WELL
DVP_P4-2:	OPEN BRANCH FROM BUS 314303 TO BUS 314287 CKT 1 HOPEWELL CHESTERFIELD		/*L211
211T2124	OPEN BRANCH FROM BUS 314303 TO BUS 314269 CKT 1		/*L2124
	END		

	CONTINGENCY 'DVP_P4-2: 562T563'	/*CARSO	N
DVP_P4-2:	OPEN BRANCH FROM BUS 314902 TO BUS 314923 CKT TO MIDLOTHIAN	1	/*CARSON
562T563	OPEN BRANCH FROM BUS 314914 TO BUS 314902 CKT 500.00 - 8SEPTA 500.00	1	/*CARSON
	END		
	CONTINGENCY 'DVP_P7-1: LN 211-228'		
	OPEN BRANCH FROM BUS 314287 TO BUS 314303 CKT 230.00 - 6HOPEWLL 230.00	1	/* 6CHSTF B
DVP_P7-1: LN 211-228	OPEN BRANCH FROM BUS 314278 TO BUS 314286 CKT 6BERMUDA 230.00 - 6CHSTF A 230.00	1	/*
LIN 211-220	OPEN BRANCH FROM BUS 314278 TO BUS 314303 CKT 6BERMUDA 230.00 - 6HOPEWLL 230.00	1	/*
	OPEN BUS 314278 /* ISLAN	D	
	END		
	CONTINGENCY 'DVP_P7-1: LN 212-240_D'		
DVP_P7-1: LN 212-	OPEN BRANCH FROM BUS 925330 TO BUS 314538 CKT TAP 230.00 - 6SURRY 230.00	2	/* AB2-190
240_D	OPEN BRANCH FROM BUS 924810 TO BUS 314538 CKT TAP 230.00 - 6SURRY 230.00	1	/* AB2-134
	END		

Generator Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output).

Overload		Contingency	Affected		В	us		Power	Load	ling %	Rat	ing	MW	Flowgate
Number	Type	Name	Area	Facility Description	From	То	Circuit	Flow	Initial	Final	Type	MVA	Contribution	Appendix
		DVP_P4-2:	DVP -	6BERMUDA-6CHESTF A 230										
1	LFFB	211T2124	DVP	kV line	314278	314286	1	AC	99	110.49		549	63.99	1
		DVP_P7-1: LN 212-	DVP -	6BERMUDA-6CHESTF A 230										
2	DCTL	240_D	DVP	kV line	314278	314286	1	AC	89.46	101.47		549	67.25	
		DVP_P4-2:	DVP -	6HOPEWLL-6BERMUDA 230										
3	LFFB	211T2124	DVP	kV line	314303	314278	1	AC	99.02	110.52		549	63.99	2
		DVP_P7-1: LN 212-	DVP -	6HOPEWLL-6BERMUDA 230										
4	DCTL	240_D	DVP	kV line	314303	314278	1	AC	89.49	101.49		549	67.25	

Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

Overloa d		Contingency			В	us			Load	ing %	Rat	ing	MW	Flowgate
			Affected				Circui	Power			Тур	MV	Contributio	Appendi
Number	Type	Name	Area	Facility Description	From	То	t	Flow	Initial	Final	е	Α	n	X
5	LFFB	DVP_P4-2: 562T563	DVP -	6CHESTF B-6BASIN 230 kV	31428	31427	1	AC	110.5	113.3		549	15.11	3
			DVP	line	7	6			9	5				
6	N-1	DVP_P1-2: LN 217	DVP -	6CHESTF B-6BASIN 230 kV	31428	31427	1	AC	106.8	109.3	ER	449	11.25	
			DVP	line	7	6			6	9				

System Reinforcements – Load Flow

New System Reinforcements

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this project generation)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost	AD1-151 Allocation
#1, 2 #3, 4	6BERMUDA-6CHESTF A 230 kV line	PJM Baseline Upgrade: Upgrade #1 Project Id: b2922 Project Description: Rebuild 8 of 11 miles of 230kV Lines #211 and #228 to current standard with a summer emergency rating of 1046 MVA for rebuilt section. Proposed conductor is 2-636 ACSR. Note: This project is already in Service. Upgrade #2 Project Id: b3694.11 Project Description: Reconductor approximately 2.9 miles of 230 kV Line #228 Chesterfield – Hopewell to achieve a minimum summer emergency rating of 1046 MVA. Type: FAC Total Cost: \$7,500,000 New Rating: Rate A: 1047 MVA Rate B: 1047 MVA Rate C: 1204 MVA Projected ISD: 6/1/2026	b2922 b3694.11 b3694.12 b3694.13	-	\$0

6HOPEWLL- 6BERMUDA 230 kV line	Upgrade #3 Project Id: b3694.12 Project Description: Upgrade equipment at Chesterfield substation to not limit ratings on Lines 211 and 228. Projected ISD: 06/01/2026 Upgrade #4 Project Id: b3694.13 Project Description: Upgrade equipment at Hopewell substation to not limit ratings on Lines 211 and 228. Projected ISD: 06/01/2026 Note 1: Although Queue Project AD1-0151 may not have cost responsibility for this upgrade, Queue Project AD1-151 may need this upgrade in-service to be deliverable to the PJM system. If Queue Project AD1-151 comes into service prior to completion of the upgrade, Queue Project AD1-151 will need an interim study.		
	service prior to completion of the upgrade, Queue Project		

Contribution to Previously Identified System Reinforcements

(Overloads initially caused by prior Queue positions with additional contribution to overloading by this project. This project may have a % allocation cost responsibility which will be calculated and reported for the Impact Study)

(Summary form of Cost allocation for transmission lines and transformers will be inserted here if any)

Violation #	Overloaded Facility	Upgrade Description	Network Upgrade Number	Upgrade Cost	AD1-151 Allocation
#5, 6	6CHESTF B- 6BASIN 230 kV line	Chesterfield – Basin 230kV line # 259, replace 0.14 miles of 1109 ACAR with a conductor with a conductor which will increase the line rating to approximately 706 MVA (normal), 706 MVA (emergency), and 812 MVA (load dump). Work completed 6/01/2018.	b2990	-	\$0
		Total Cost(\$)			\$0

Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The IC can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this interconnection request by addressing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

Overloa d	Contingency		Affected		В	us	Circui	Power	Load	ing %	Rat Typ	ting MV	MW Contributio	Flowgate Appendi
Number	Type	Name	Area	Facility Description	From	То	t	Flow	Initial	Final	é	Α	n	×
5	N-1	DVP_P1-2: LN 211	DVP - DVP	6BERMUDA-6CHESTF A 230 kV line	31427 8	31428 6	1	AC	104	116.2 8	ER	449	55.68	
6	N-1	DVP_P1-2: LN 563	DVP - DVP	6CHESTF B-6BASIN 230 kV line	31428 7	31427 6	1	AC	128	131.4 6	ER	449	15.54	
7	N-1	DVP_P1-2: LN 211	DVP - DVP	6HOPEWLL-6BERMUDA 230 kV line	31430 3	31427 8	1	AC	104.0 3	116.3	ER	449	55.68	
8	N-1	DVP_P1-2: LN 228	DVP - DVP	6HOPEWLL-6CHESTF B 230 kV line	31430 3	31428 7	1	AC	95.01	107.8 1	ER	442	57.31	
9	N-1	DVP_P1-2: LN 594	DVP - DVP	8CHANCE-8BRISTER 500 kV line	31490 5	31490 0	1	AC	101.6 8	102.7 1	ER	244 2	28.95	
10	N-1	DVP_P1-2: LN 576	DVP - DVP	8ELMONT-8LADYSMITH 500 kV line	31490 8	31491 1	1	AC	111.8	113.6 5	ER	244 2	48.43	

11	N-1	DVP_P1-2: LN 574	DVP - DVP	8MDLTHAN-8NO ANNA 500 kV line	31491 4	31491 8	1	AC	104.3 9	105.8	ER	244 2	39.5	
12	N-1	DVP_P1-2: LN 575	DVP - DVP	8SPOTSYL-8MORRSVL 500 kV line	31493	31491	1	AC	99.6	100.4	ER	321	22.66	

Short Circuit

(Summary of impacted circuit breakers) New circuit breakers found to be over-duty:

None.

Contributions to previously identified circuit breakers found to be over-duty: None.

New System Reinforcements – Short Circuit

(Upgrades required to mitigate reliability criteria violations, i.e. Network Impacts, initially caused by the addition of this interconnection request)

None.

Steady-State Voltage Requirements

(Summary of the VAR requirements based upon the results of the steady-state voltage studies) None.

Stability and Reactive Power Requirement for Low Voltage Ride Through

(Summary of the VAR requirements based upon the results of the dynamic studies)

The queue project, AD1-151, does not meet the 0.95 lagging power factor requirement and meets the 0.95 leading power factor requirement. An additional 8.62 Mvar would be required for the plant to meet the 0.95 lagging power factor requirement at the high side of the main transformer.

Power Factor Assessment for the AD1-151 Queue Project

Generator	MFO	_	d Power Range	Maximum	Minimum
	(MW)	Lagging	Leading	Lagging (Mvar)	Leading (Mvar)
AD1-151	150.00	0.95	0.95	(Mvar)	(Mivar)
Total React	ive Powe	r Required	l	49.30	-49.30
Reactive Po	war fran	Conorato	.w	Qmax	Qmin
Reactive Po	ower from	i Generato	or	61.18	-61.18
Customer P	Planned C	Compensati	ion	0	0
Reactive Po	wer Loss	es		-20.5	-20.5
Total Avail Side of Mai		40.68	-81.68		
Deficiency i	n Reactiv	8.62	Meet		

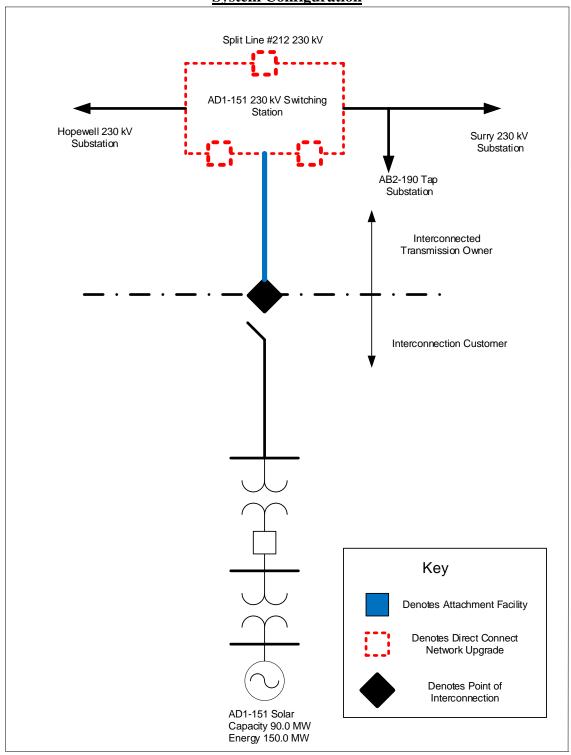
<u>Light Load Analysis in 2021</u>

None.

Affected System Analysis & Mitigation Duke Energy:

None.

System Configuration



Appendices

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. All New Service Queue Requests, through the end of the Queue under study, that are contributors to a flowgate will be listed in the Appendices. Please note that there may be contributors that are subsequently queued after the queue under study that are not listed in the Appendices. Although this information is not used "as is" for cost allocation purposes, it can be used to gage the impact of other projects/generators.

It should be noted the project/generator MW contributions presented in the body of the report and appendices sections are full contributions, whereas the loading percentages reported in the body of the report, take into consideration the commercial probability of each project as well as the ramping impact of "Adder" contributions.

Appendix 1

(DVP - DVP) The 6BERMUDA-6CHESTF A 230 kV line (from bus 314278 to bus 314286 ckt 1) loads from 99.0% to 110.49% (AC power flow) of its load dump rating (549 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 211T2124'. This project contributes approximately 63.99 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 211T2124' /*_ HOPEWELL
OPEN BRANCH FROM BUS 314303 TO BUS 314287 CKT 1 /*L211
HOPEWELL CHESTERFIELD
OPEN BRANCH FROM BUS 314303 TO BUS 314269 CKT 1 /*L2124
END

Bus Number	Bus Name	Full Contribution
315119	1GRAVEL3	3.95
315120	1GRAVEL4	4.
315121	1GRAVEL5	3.95
315122	1GRAVEL6	4.
315074	1HOPCGN1	27.86
315075	1HOPCGN2	27.5
315077	1HOPHCF1	8.22
315078	1HOPHCF2	8.22
315079	1HOPHCF3	8.22
315080	1HOPHCF4	12.48
315076	1HOPPOLC	5.85
315073	1STONECA	23.11
315116	1SURRY 1	39.6
934011	AD1-025 C O1	40.18
934012	AD1-025 E 01	23.8
935161	AD1-151 C O1	38.39
935162	AD1-151 E 01	25.59
LTF	CARR	0.16
LTF	CBM-S1	1.
LTF	CBM-S2	3.07
LTF	CBM-W1	0.65
LTF	CBM-W2	4.79
LTF	CIN	0.17
LTF	CPLE	1.05
LTF	G-007	0.62
LTF	IPL	0.1
LTF	LGEE	0.04
LTF	MEC	0.68
LTF	O-066	3.93
LTF	RENSSELAER	0.13
LTF	WEC	0.05
914231	Y2-077	3.31

924811	AB2-134 C O1	30.63
924812	AB2-134 E O1	30.12
925331	AB2-190 C	47.78
925332	AB2-190 E	20.48
927221	AC1-216 C O1	23.38
927222	AC1-216 E O1	18.39

Appendix 2

(DVP - DVP) The 6HOPEWLL-6BERMUDA 230 kV line (from bus 314303 to bus 314278 ckt 1) loads from 99.02% to 110.52% (AC power flow) of its load dump rating (549 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 211T2124'. This project contributes approximately 63.99 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 211T2124' /*_ HOPEWELL
OPEN BRANCH FROM BUS 314303 TO BUS 314287 CKT 1 /*L211
HOPEWELL CHESTERFIELD
OPEN BRANCH FROM BUS 314303 TO BUS 314269 CKT 1 /*L2124
END

Bus Number	Bus Name	Full Contribution
315119	1GRAVEL3	3.95
315120	1GRAVEL4	4.
315121	1GRAVEL5	3.95
315122	1GRAVEL6	4.
315074	1HOPCGN1	27.86
315075	1HOPCGN2	27.5
315077	1HOPHCF1	8.22
315078	1HOPHCF2	8.22
315079	1HOPHCF3	8.22
315080	1HOPHCF4	12.48
315076	1HOPPOLC	5.85
315073	1STONECA	23.11
315116	1SURRY 1	39.6
934011	AD1-025 C O1	40.18
934012	AD1-025 E 01	23.8
935161	AD1-151 C O1	38.39
935162	AD1-151 E 01	25.59
LTF	CARR	0.16
LTF	CBM-S1	1.
LTF	CBM-S2	3.07
LTF	CBM-W1	0.65
LTF	CBM-W2	4.79
LTF	CIN	0.17
LTF	CPLE	1.05
LTF	G-007	0.62
LTF	IPL	0.1
LTF	LGEE	0.04
LTF	MEC	0.68
LTF	O-066	3.93
LTF	RENSSELAER	0.13
LTF	WEC	0.05

914231	Y2-077	3.31
924811	AB2-134 C O1	30.63
924812	AB2-134 E O1	30.12
925331	AB2-190 C	47.78
925332	AB2-190 E	20.48
927221	AC1-216 C O1	23.38
927222	AC1-216 E O1	18.39

Appendix 3

(DVP - DVP) The 6CHESTF B-6BASIN 230 kV line (from bus 314287 to bus 314276 ckt 1) loads from 110.59% to 113.35% (AC power flow) of its load dump rating (549 MVA) for the line fault with failed breaker contingency outage of 'DVP_P4-2: 562T563'. This project contributes approximately 15.11 MW to the thermal violation.

CONTINGENCY 'DVP_P4-2: 562T563'

/*CARSON

OPEN BRANCH FROM BUS 314902 TO BUS 314923 CKT 1 **MIDLOTHIAN**

/*CARSON TO

OPEN BRANCH FROM BUS 314914 TO BUS 314902 CKT 1 /*CARSON 500.00

- 8SEPTA 500.00 **END**

Bus Number	Bus Name	Full Contribution
315065	1CHESTF6	32.84
315131	1EDGECMA	3.05
315132	1EDGECMB	3.05
315074	1HOPCGN1	5.89
315075	1HOPCGN2	5.81
315077	1HOPHCF1	1.74
315078	1HOPHCF2	1.74
315079	1HOPHCF3	1.74
315080	1HOPHCF4	2.64
315076	1HOPPOLC	1.24
315073	1STONECA	4.88
314557	<i>3BETHELC</i>	0.3
314554	<i>3BTLEBRO</i>	0.3
314572	<i>3EMPORIA</i>	0.22
314578	<i>3HORNRTN</i>	1.43
314314	<i>3LOCKS</i>	0.06
314315	3LOCKS E	0.83
314603	3SCOT NK	1.31
314541	3WATKINS	0.27
314620	6CASHIE	0.31
314594	6PLYMOTH	0.3
932591	AC2-079 C	2.7
932592	AC2-079 E	4.41
932631	AC2-084 C	2.64
932632	AC2-084 E	1.3
933991	AD1-022 C	3.17
933992	AD1-022 E	1.72
934011	AD1-025 C 01	9.49
934012	AD1-025 E 01	5.62
934331	AD1-057 C O1	4.26

934332 AD1-057 E O1 2.27 934521 AD1-076 C O1 19.37 934522 AD1-076 E O1 9.86 934571 AD1-082 C O1 5.2 934572 AD1-082 E O1 2.97 935161 AD1-151 C O1 9.07 935162 AD1-151 E O1 6.05 LTF CARR 0.23 LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
934522 AD1-076 E 01 9.86 934571 AD1-082 C 01 5.2 934572 AD1-082 E 01 2.97 935161 AD1-151 C 01 9.07 935162 AD1-151 E 01 6.05 LTF CARR 0.23 LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CIN 1.7 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
934571 AD1-082 C O1 5.2 934572 AD1-082 E O1 2.97 935161 AD1-151 C O1 9.07 935162 AD1-151 E O1 6.05 LTF CARR 0.23 LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CIN 1.7 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
934572 AD1-082 E 01 2.97 935161 AD1-151 C 01 9.07 935162 AD1-151 E 01 6.05 LTF CARR 0.23 LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CIN 1.7 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
935161 AD1-151 C O1 9.07 935162 AD1-151 E O1 6.05 LTF CARR 0.23 LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CIN 1.7 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
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LTF CBM-S1 3.99 LTF CBM-S2 8.63 LTF CBM-W1 7.45 LTF CBM-W2 20.89 LTF CIN 1.7 LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
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LTF CPLE 2.76 LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
LTF G-007 1.04 LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
LTF IPL 1.08 LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
LTF LGEE 0.37 LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
LTF MEC 4.07 LTF MECS 1.38 LTF O-066 6.63	
LTF MECS 1.38 LTF O-066 6.63	
LTF 0-066 6.63	
THE DENGGET LED 0.10	
LTF RENSSELAER 0.18	
900672 V4-068 E 0.12	
LTF WEC 0.47	
907092 X1-038 E 2.34	
914231 Y2-077 0.7	
916302 Z1-086 E 3.71	
917332 Z2-043 E 0.39	
917342 Z2-044 E 0.22	
917512 Z2-088 E OP1 1.45	
918492 AA1-063AE OP 1.7	
918512 AA1-065 E OP 1.69	
918562 AA1-072 E 0.07	
919692 AA2-053 E 1.6	
919701 AA2-057 C 2.8	
919702 AA2-057 E 1.4	
LTF AA2-074 1.88	
920042 AA2-088 E 4.24	
920592 AA2-165 E 0.18	
920672 AA2-174 E 0.18	
930402 AB1-081 E 1.46	
930861 AB1-132 C 6.74	
930862 AB1-132 E 2.89	
931231 AB1-173 C 1.1	
931232 AB1-173 E 0.52	
931241 AB1-173AC 1.1	

931242	AB1-173AE	0.52
923851	AB2-025 C	0.32
923852	AB2-025 E	0.78
923911	AB2-031 C O1	1.1
923912	AB2-031 E 01	0.54
923991	AB2-040 C O1	3.6
923992	AB2-040 E O1	2.94
924151	AB2-059 C O1	4.01
924152	AB2-059 E O1	2.06
924501	AB2-099 C	0.23
924502	AB2-099 E	0.1
924511	AB2-100 C	6.79
924512	AB2-100 E	3.35
924811	AB2-134 C O1	7.23
924812	AB2-134 E O1	7.11
925051	AB2-160 C O1	3.59
925052	AB2-160 E O1	5.86
925061	AB2-161 C O1	2.28
925062	AB2-161 E O1	3.72
925121	AB2-169 C	2.34
925122	AB2-169 E	2.1
925171	AB2-174 C O1	3.52
925172	AB2-174 E O1	3.18
925331	AB2-190 C	11.28
925332	AB2-190 E	4.84
925591	AC1-034 C	2.6
925592	AC1-034 E	1.96
925821	AC1-061	< 0.01
926071	AC1-086 C	9.93
926072	AC1-086 E	4.52
926201	AC1-098 C	2.46
926202	AC1-098 E	1.47
926211	AC1-099 C	0.83
926212	AC1-099 E	0.49
927021	AC1-189 C	3.2
927022	AC1-189 E	1.59
927141	AC1-208 C	3.74
927142	AC1-208 E	1.66
927221	AC1-216 C 01	5.52
927222	AC1-216 E 01	4.34