

Generation Interconnection System Impact Study Report for

Queue Project AE1-056

RED HOUSE-SOUTH CREEK 115 KV

38.8 MW Capacity / 60 MW Energy

Revision 3 / April 2022

Revision 2 / January 2022

Revised December 2019

August, 2019

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1 Introduction

This System Impact Study (SIS) has been prepared in accordance with the PJM Open Access Transmission Tariff, 205, as well as the Feasibility Study Agreement between Caden Energix Spout Spring LLC, the Interconnection Customer (IC), and PJM Interconnection, LLC (PJM), Transmission Provider (TP). The Interconnected Transmission Owner (ITO) is Virginia Electric and Power Company (VEPCO).

2 Preface

The intent of the System Impact Study is to determine a plan, with approximate cost and construction time estimates, to connect the subject generation interconnection project to the PJM network at a location specified by the Interconnection Customer. As a requirement for interconnection, the Interconnection Customer may be responsible for the cost of constructing: Network Upgrades, which are facility additions, or upgrades to existing facilities, that are needed to maintain the reliability of the PJM system. All facilities required for interconnection of a generation interconnection project must be designed to meet the technical specifications (on PJM web site) for the appropriate transmission owner.

In some instances an Interconnection Customer may not be responsible for 100% of the identified network upgrade cost because other transmission network uses, e.g. another generation interconnection or merchant transmission upgrade, may also contribute to the need for the same network reinforcement. The possibility of sharing the reinforcement costs with other projects may be identified in the Feasibility Study, but the actual allocation will be deferred until the System Impact Study is performed.

The System Impact Study estimates do not include the feasibility, cost, or time required to obtain property rights and permits for construction of the required facilities. The project developer is responsible for the right of way, real estate, and construction permit issues. For properties currently owned by Transmission Owners, the costs may be included in the study.

The Interconnection Customer seeking to interconnect a wind or solar generation facility shall maintain meteorological data facilities as well as provide that meteorological data which is required per Schedule H to the Interconnection Service Agreement and Section 8 of Manual 14D.

3 Revision 3 (April 2022) Summary

This revision is being issued to replace the previously identified network upgrade n6115 with the already approved supplemental project s2614. The scope of s2614 meets the intent of n6115 and addresses the identified overload. The New System Reinforcement table and cost tables were updated to reflect this change

4 Revision 2 (January 2022) Summary

This revision is being issued to incorporate results of a re-tool performed in January of 2022 and the Stability Analysis. No mitigations were found to be required related to project stability.

5 General

The IC has proposed a solar generating facility located in Appomattox County, Virginia. The installed facilities will have a capability of 60 MW with 38.8 MW of this output being recognized by PJM as Capacity. The proposed in-service date for the AE1-056 project is 12/15/2020. This study does not imply an ITO commitment to either in-service date.

| Queue Number | AE1-056 | | |
|--------------------------|--------------------------------|--|--|
| Project Name | RED HOUSE-SOUTH CREEK 115 KV | | |
| Interconnection Customer | Caden Energix Spout Spring LLC | | |
| State | Virginia | | |
| County | Appomattox | | |
| Transmission Owner | Dominion | | |
| MFO | 60 | | |
| MWE | 60 | | |
| MWC | 38.8 | | |
| Fuel | Solar | | |
| Basecase Study Year | 2022 | | |

5.1 Point of Interconnection

AE1-056 will interconnect with the Dominion transmission system via a new three breaker ring bus switching station that connects on the Red House DP – South Creek 115kV line near the South Creek 115 kV substation. See one line in **Attachment 1**.

5.2 Cost Summary

The AE1-056 project will be responsible for the following costs:

| Description | Total Cost |
|--|--------------|
| Attachment Facilities | \$ 1,550,000 |
| Direct Connection Network Upgrade | \$ 5,500,000 |
| Non Direct Connection Network Upgrades | \$ 1,000,000 |
| Total Costs | \$ 8,050,000 |

In addition, the AE1-056 project may be responsible for a contribution to the following costs

| Description | Total Cost |
|---|------------|
| Allocation for New System Upgrades | \$0 |
| Contribution for Previously Identified Upgrades | \$0 |
| Total Costs | \$0 |

<u>Note</u>: PJM Open Access Transmission Tariff (OATT) section 217.3A outline cost allocation rules. The rules are further clarified in PJM Manual 14A Attachment B. The allocation of costs for a network upgrade will start with the first Queue project to cause the need for the upgrade. Later queue projects will receive cost allocation contingent on their contribution to the violation and are allocated to the queues that have not closed less than 5 years following the execution of the first Interconnection Service Agreement which identifies the need for this upgrade.

6 Transmission Owner Scope of Work

6.1 Attachment Facilities

Generation Substation: Install metering and associated protection equipment. Estimated Cost is \$550,000.

<u>Transmission:</u> Construct approximately one span of 115 kV Attachment line between the generation substation and a new AE1-056 Switching Station. The estimated cost for this work is \$1,000,000.

The estimated total cost of the Attachment Facilities is \$1,550,000. It is estimated to take 18-24 months to complete this work. These preliminary cost estimates are based on typical engineering costs. A more detailed engineering cost estimates are normally done when the IC provides an exact site plan location for the generation substation during the Facility Study phase. The total preliminary cost estimate for the Attachment work is given in the table below.

The total preliminary cost estimate for the Attachment work is given in the table below. These costs do not include CIAC Tax Gross-up.

| Description | Total Cost |
|---------------------------------|--------------|
| Substation | \$ 550,000 |
| Transmission | \$ 1,000,000 |
| | |
| Total Attachment Facility Costs | \$ 1,550,000 |

6.2 Direct Connection Cost Estimate

<u>Substation:</u> Establish the new 115 kV AE1-056 Switching Substation (interconnection substation). The estimated cost of this work scope is \$5,500,000. It is estimated to take 24-36 months to complete this work.

The total preliminary cost estimate for the Direct Connection work is given in the table below. These costs do not include CIAC Tax Gross-up.

| Description | Total Cost |
|---|--------------|
| Substation | \$ 5,500,000 |
| | |
| Total Direct Connection Facility Costs | \$ 5,500,000 |

6.3 Non-Direct Connection Cost Estimate

<u>Transmission:</u> Install transmission structure in-line with transmission line to allow the proposed interconnection switching station to be interconnected with the transmission system. Estimated cost is \$1,000,000 and is estimated to take 24-30 months to complete.

Remote Terminal Work: During the Facilities Study, ITO's System Protection Engineering Department will review transmission line protection as well as anti-islanding required to accommodate the new generation and interconnection substation. System Protection Engineering will determine the minimal acceptable protection requirements to reliably interconnect the proposed generating facility with the transmission system. The review is based on maintaining system reliability by reviewing ITO's protection requirements with the known transmission system configuration which includes generating facilities in the area. This review may determine that transmission line protection and communication upgrades are required at remote substations.

The total preliminary cost estimate for the Non-Direct Connection work is given in the table below. These costs do not include CIAC Tax Gross-up.

| Description | Total Cost |
|---|-----------------------------|
| Transmission | \$ 1,000,000 |
| Remote Terminal Work | TBD in the Facilities Study |
| | |
| Total Non-Direct Connection Facility Costs | \$ 1,000,000 |

7 Interconnection Customer Requirements

7.1 System Protection

The IC must design its Customer Facilities in accordance with all applicable standards, including the standards in Dominion's "Dominion Energy Electric Transmission Generator Interconnection Requirements" documented in Dominion's Facility Interconnection Requirements "Exhibit C" located at: https://www.dominionenergy.com/company/moving-energy/electric-transmission-access. Preliminary Protection requirements will be provided as part of the Facilities Study. Detailed Protection Requirements will be provided once the project enters the construction phase.

7.2 Compliance Issues and Interconnection Customer Requirements

The proposed Customer Facilities must be designed in accordance with Dominion's "Dominion's Facility Interconnection Requirements" document located at: https://www.dominionenergy.com/company/moving-energy/electric-transmission-access. In particular, the IC is responsible for the following:

1. The purchase and installation of a fully rated protection device (circuit breaker, circuit switcher, fuse) to protect the IC's GSU transformer(s).

- 2. The purchase and installation of the minimum required Dominion generation interconnection relaying and control facilities as described in the System Protection noted above. This includes over/under voltage protection, over/under frequency protection, and zero sequence voltage protection relays.
- 3. The purchase and installation of supervisory control and data acquisition ("SCADA") equipment to provide information in a compatible format to the Dominion Transmission System Control Center.
- 4. Compliance with the Dominion and PJM generator power factor and voltage control requirements.

The GSU(s) associated with the IC queue request shall meet the grounding requirements as noted in Dominion's "Dominion's Facility Interconnection Requirements" document located at: https://www.dominionenergy.com/company/moving-energy/electric-transmission-access.

The IC will also be required to meet all PJM, SERC, and NERC reliability criteria and operating procedures for standards compliance. For example, the IC will need to properly locate and report the over and under voltage and over and under frequency system protection elements for its units as well as the submission of the generator model and protection data required to satisfy the PJM and SERC audits. Failure to comply with these requirements may result in a disconnection of service if the violation is found to compromise the reliability of the Dominion system.

7.3 Power Factor Requirements

The IC shall design its non-synchronous Customer Facility with the ability to maintain a power factor of at least 0.95 leading (absorbing VARs) to 0.95 lagging (supplying VARs) measured at the high-side of the facility substation transformer(s) connected to the Dominion transmission system.

8 Revenue Metering and SCADA Requirements

8.1 PJM Requirements

The Interconnection Customer will be required to install equipment necessary to provide Revenue Metering (KWH, KVARH) and real time data (KW, KVAR) for IC's generating Resource. See PJM Manuals M-01 and M-14D, and PJM Tariff Section 8 of Attachment O.

8.2 Dominion Requirements

See Section 3.4.6 "Metering and Telecommunications" of Dominion's "Dominion's Facility Interconnection Requirements" document located at: https://www.dominionenergy.com/company/moving-energy/electric-transmission-access.

9 Network Impacts

The Queue Project AE1-056 was evaluated as a 60.0 MW (Capacity 38.8 MW) injection at the South Creek 115kV substation in the Dominion area. Project AE1-056 was evaluated for compliance with applicable reliability planning criteria (PJM, NERC, NERC Regional Reliability Councils, and Transmission Owners). Project AE1-056 was studied with a commercial probability of 100%. Potential network impacts were as follows:

Summer Peak Load Flow

10 Generation Deliverability

(Single or N-1 contingencies for the Capacity portion only of the interconnection)

None

11 Multiple Facility Contingency

(Double Circuit Tower Line, Fault with a Stuck Breaker, and Bus Fault contingencies for the full energy output)

None

12 Contribution to Previously Identified Overloads

(This project contributes to the following contingency overloads, i.e. "Network Impacts", identified for earlier generation or transmission interconnection projects in the PJM Queue)

| ID | FROM BUS# | FROM BUS | FROM BUS AREA | TO BUS# | TO BUS | TO BUS AREA | CKT ID | CONT NAME | Туре | Rating MVA | PRE PROJECT LOADING % | POST PROJECT LOADING % | AC DC | MW IMPACT |
|----|--------------|----------|---------------------|------------|-----------------|-------------------|-----------|------------------------------|---------|---------------|--------------------------------|---------------------------------|-------|--------------|
| 1 | 314702 | 3KERR | DVP | 304102 | 3GW KING TAP | CPLE | 1 | DVP_P7-1: LN 22-90-A | tower | 199.0 | 112.57 | 115.23 | AC | 6.41 |
| 2 | 314702 | 3KERR | DVP | 304102 | 3GW KING TAP | CPLE | 1 | DVP_P4-6: CAROLIN T122 | breaker | 199.0 | 106.9 | 109.54 | AC | 6.49 |
| 3 | 314702 | 3KERR | DVP | 304102 | 3GW KING TAP | CPLE | 1 | DVP_P7-1: LN 22-90-B | tower | 199.0 | 101.37 | 104.03 | AC | 6.41 |

13 Potential Congestion due to Local Energy Deliverability

PJM also studied the delivery of the energy portion of this interconnection request. Any problems identified below are likely to result in operational restrictions to the project under study. The developer can proceed with network upgrades to eliminate the operational restriction at their discretion by submitting a Merchant Transmission Interconnection request.

Note: Only the most severely overloaded conditions are listed below. There is no guarantee of full delivery of energy for this project by fixing only the conditions listed in this section. With a Transmission Interconnection Request, a subsequent analysis will be performed which shall study all overload conditions associated with the overloaded element(s) identified.

| ID | FROM BUS# | FROM BUS | FROM BUS AREA | TO BUS# | TO BUS | TO BUS AREA | CKT ID | CONT NAME | Type | Rating MVA | PRE PROJECT LOADING % | POST PROJECT LOADING % | AC DC | MW IMPACT |
|----|--------------|-------------|---------------------|------------|-----------------|-------------------|-----------|--------------------------------|-----------|---------------|--------------------------------|---------------------------------|-------|--------------|
| 4 | 313867 | 6BREMODIST | DVP | 314765 | 6MTEAGLE | DVP | 1 | DVP_P1-2: LN 2027-B | operation | 662 | 88.95 | 91.39 | AC | 16.2 |
| 5 | 314559 | 3CAROLNA | DVP | 314561 | 6CAROLNA | DVP | 1 | DVP_P1-3: 6CLUBHSE- TX#1 | Operation | 240 | 103.88 | 105.73 | AC | 4.59 |
| 6 | 314562 | 3CLUBHSE | DVP | 314563 | 6CLUBHSE | DVP | 1 | DVP_P1-3: 6CAROLNA- TX#4 | operation | 183 | 130.72 | 132.76 | AC | 4.95 |
| 7 | 314562 | 3CLUBHSE | DVP | 314563 | 6CLUBHSE | DVP | 1 | Base Case | operation | 177 | 102.04 | 103.71 | AC | 4.19 |
| 8 | 314697 | 6SEDGE HILL | DVP | 927250 | AC1-221 TAP | DVP | 1 | DVP_P1-2: LN 556 | operation | 675 | 96.59 | 98.68 | AC | 14.12 |
| 9 | 314702 | 3KERR | DVP | 304102 | 3GW KING TAP | CPLE | 1 | DVP_P1-2: LN 570 | operation | 199.0 | 97.27 | 99.21 | AC | 4.74 |
| 10 | 314747 | 6BREMO | DVP | 313867 | 6BREMODIST | DVP | 1 | DVP_P1-2: LN 2027-B | Operation | 662 | 91.15 | 93.59 | AC | 16.2 |
| 11 | 927250 | AC1-221 TAP | DVP | 304070 | 6PERSON230 T | CPLE | 1 | DVP_P1-2: LN 556 | operation | 718.0 | 105.93 | 107.89 | AC | 14.12 |

14 System Reinforcements

| ID | Facility | Upgrade Description | Network Upgrade Number | Cost | AE1-056 Allocation |
|----|--------------------------------------|---|------------------------------|--------------|-----------------------|
| | | This line is a joint tie line between the Dominion Energy and Duke/Progress transmission systems. Dominion: Rebuild approximately 4.7 miles Line #45 between Kerr Dam to Duke Interconnection with current 115kV standards construction practices (768 ACSS at 250 degree C). New rating: 393/393/452 MVA Expected in service date: 12/31/2022 | s2614 | \$11,000,000 | \$0 |
| 1 | 3KERR-3GW KING TAP 115 kV line | Duke/Progress Energy portion of this line will need to be studied under Duke's FERC tariff process: Project Id: dep0002 Project Description: Reconductor 20 miles with single 795 ACSS-TW per phase, replace breaker, disconnect switches, wave trap, line switches. Time Estimate: 48 Month Cost Estimate: \$80,000,000 Note 1: This is tie line between Duke Energy and Dominion. Note 2: Although Queue Project AE1-056 may not have cost responsibility for this upgrade, it may need this upgrade in-service to be deliverable to the PJM system. If Queue Project AE1-056 comes into service prior to completion of the upgrade, it will need an interim study. Note 3: The Duke/Progress Energy portion of this line is studied under Duke's FERC tariff process. Reference the applicable affected system study for the AE1 cluster | Dep0002 | \$60,000,000 | \$0 |
| | | TOTAL COST | | \$71,000,000 | \$0 |

15 Flow Gate Details

The following appendices contain additional information about each flowgate presented in the body of the report. For each appendix, a description of the flowgate and its contingency was included for convenience. However, the intent of the appendix section is to provide more information on which projects/generators have contributions to the flowgate in question. Although this information is not used "as is" for cost allocation purposes, it can be used to gage other generators impact. It should be noted the generator contributions presented in the appendices sections are full contributions, whereas in the body of the report, those contributions take into consideration the commercial probability of each project.

15.1 Contingency Description

| Contingency Name | Contingency Definition | |
|------------------------|--|--------------------------------------|
| | CONTINGENCY 'DVP_P7-1: LN 22-90-A' | |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314571 CKT 1 | /* 3CAROLNA 115.00 - 3EATON F |
| | 115.00 | |
| | OPEN BRANCH FROM BUS 314571 TO BUS 925780 CKT 1 | /* 3EATON F 115.00 - AC1-054 TAP |
| | 115.00 | |
| | OPEN BUS 314571 /* ISLAND: 3EA | |
| | OPEN BRANCH FROM BUS 314265 TO BUS 314584 CKT 1 | /* 3FIVEFORKSDP115.00 - 3LITTLTN |
| | 115.00 | 4 |
| DVP_P7-1: LN 22-90-A | OPEN BRANCH FROM BUS 314265 TO BUS 314673 CKT 1 | /* 3FIVEFORKSDP115.00 - |
| | 3PALMERSPRNG115.00 | /* 2CADOLNA 445 00 21 CACTN |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314585 CKT 1 115.00 | /* 3CAROLNA 115.00 - 3L GASTN |
| | OPEN BRANCH FROM BUS 314584 TO BUS 314585 CKT 1 | /* 3LITTLTN 115.00 - 3L GASTN 115.00 |
| | | /EFORKSDP115.00 |
| | OPEN BUS 314584 /* ISLAND: 3LIT | |
| | OPEN BUS 314585 /* ISLAND: 3L G | |
| | END | |
| | CONTINGENCY 'DVP_P4-6: CAROLIN T122' /* | CAROLINA 115 KV |
| | OPEN BRANCH FROM BUS 314559 TO BUS 315126 CKT 1 | /* 3CAROLNA 115.00 - 1ROARAP2 |
| | 14.400 | |
| | OPEN BRANCH FROM BUS 314559 TO BUS 315128 CKT 1 | /* 3CAROLNA 115.00 - 1ROARAP4 |
| | 14.400 | |
| | OPEN BUS 315126 /* ISLAND: 1RO | |
| | OPEN BUS 315128 /* ISLAND: 1RO OPEN BRANCH FROM BUS 314559 TO BUS 314571 CKT 1 | |
| | 115.00 | /* 3CAROLNA 115.00 - 3EATON F |
| | OPEN BRANCH FROM BUS 313722 TO BUS 314559 CKT 1 | /* 3OCCONEECHEE115.00 - 3CAROLNA |
| | 115.00 | / JOCCONLICITED SCANOLINA |
| DVP_P4-6: CAROLIN T122 | OPEN BRANCH FROM BUS 314259 TO BUS 314559 CKT Z1 | /* 3CAROL56_1 115.00 - 3CAROLNA |
| | 115.00 | , |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314578 CKT 1 | /* 3CAROLNA 115.00 - 3HORNRTN |
| | 115.00 | |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314585 CKT 1 | /* 3CAROLNA 115.00 - 3L GASTN |
| | 115.00 | |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314600 CKT 1 | /* 3CAROLNA 115.00 - 3PLHITP 115.00 |
| | OPEN BRANCH FROM BUS 314559 TO BUS 314561 CKT 1 | /* 3CAROLNA 115.00 - 6CAROLNA |
| | 230.00 | |
| | OPEN BUS 314559 /* 3CAROLNA 1 | 15.00 KV |
| | END | |

| Contingency Name | Contingency Definition | | | | |
|---------------------------------|---|--------------------------------------|--|--|--|
| | CONTINGENCY 'DVP_P7-1: LN 22-90-B' | | | | |
| | OPEN BRANCH FROM BUS 925780 TO BUS 314702 CKT 1 | /* AC1-054 TAP 115.00 - 3KERR 115.00 | | | |
| | OPEN BRANCH FROM BUS 314265 TO BUS 314584 CKT 1 | /* 3FIVEFORKSDP115.00 - 3LITTLTN | | | |
| | 115.00 | , | | | |
| | OPEN BRANCH FROM BUS 314265 TO BUS 314673 CKT 1 | /* 3FIVEFORKSDP115.00 - | | | |
| | 3PALMERSPRNG115.00 | 7 311721 3111351 113.00 | | | |
| DVP P7-1: LN 22-90-B | OPEN BRANCH FROM BUS 314559 TO BUS 314585 CKT 1 | /* 3CAROLNA 115.00 - 3L GASTN | | | |
| 541 <u>-</u> 1 7 11 214 22 30 5 | 115.00 | 7 36/11/02/1// 113:00 32 6/13/14 | | | |
| | OPEN BRANCH FROM BUS 314584 TO BUS 314585 CKT 1 | /* 3LITTLTN 115.00 - 3L GASTN 115.00 | | | |
| | | VEFORKSDP115.00 | | | |
| | OPEN BUS 314584 /* ISLAND: 3LITTLTN 115.00 | | | | |
| | OPEN BUS 314585 /* ISLAND: 3L GASTN 115.00 | | | | |
| | END | 3A31N 113.00 | | | |
| | | | | | |
| | CONTINGENCY 'DVP_P1-2: LN 2027-B' | /* A C2 1 CF TA D 220 00 CDONAULATAL | | | |
| | OPEN BRANCH FROM BUS 933500 TO BUS 314333 CKT 1 | /* AC2-165 TAP 230.00 - 6POWHATN | | | |
| | 230.00 | /* CHIPEC F 220 00 CMARLTHAN | | | |
| | OPEN BRANCH FROM BUS 314310 TO BUS 314322 CKT 1 | /* 6JUDES F 230.00 - 6MDLTHAN | | | |
| DVP_P1-2: LN 2027-B | 230.00 | /* CUIDES E 222 22 CD01414 TN | | | |
| _ | OPEN BRANCH FROM BUS 314310 TO BUS 314333 CKT 1 | /* 6JUDES F 230.00 - 6POWHATN | | | |
| | 230.00 | | | | |
| | OPEN BUS 314310 /* ISLAND: 6JU | | | | |
| | 1 | OWHATN 230.00 | | | |
| | END | | | | |
| | CONTINGENCY 'DVP_P1-3: 6CLUBHSE-TX#1' | | | | |
| DVP P1-3: 6CLUBHSE-TX#1 | OPEN BRANCH FROM BUS 314562 TO BUS 314563 CKT 1 | /* 3CLUBHSE 115.00 - 6CLUBHSE | | | |
| | 230.00 | | | | |
| | END | | | | |
| | CONTINGENCY 'DVP_P1-3: 6CAROLINA-TX#4' | | | | |
| DVP_P1-3: 6CAROLNA-TX#4 | OPEN BRANCH FROM BUS 314559 TO BUS 314561 CKT 1 | /* 3CLUBHSE 115.00 - 6CLUBHSE | | | |
| | 230.00 | | | | |
| | END | | | | |
| | CONTINGENCY 'DVP_P1-2: LN 556' | | | | |
| | OPEN BRANCH FROM BUS 314686 TO BUS 314906 CKT 1 | /* 6CLOVER 230.00 - 8CLOVER 500.00 | | | |
| | OPEN BRANCH FROM BUS 314686 TO BUS 314906 CKT 2 | /* 6CLOVER 230.00 - 8CLOVER 500.00 | | | |
| DVP_P1-2: LN 556 | OPEN BRANCH FROM BUS 314686 TO BUS 314906 CKT 3 | /* 6CLOVER 230.00 - 8CLOVER 500.00 | | | |
| | OPEN BRANCH FROM BUS 314906 TO BUS 314936 CKT 1 | /* 8CLOVER 500.00 - 8RAWLINGS | | | |
| | 500.00 | | | | |
| | OPEN BUS 314906 /* ISLAND: 8CL | | | | |
| | OPEN BUS 314915 /* ISLAND: 8CL | OVER_STC 500.00 | | | |
| | END | | | | |
| | CONTINGENCY 'DVP_P1-2: LN 570' | | | | |
| | OPEN BRANCH FROM BUS 304183 TO BUS 918500 CKT 1 | /* 8WAKE 500 TT500.00 - AA1-064 TAP | | | |
| | 500.00 | | | | |
| DVP_P1-2: LN 570 | OPEN BRANCH FROM BUS 314935 TO BUS 918500 CKT 1 | /* 8HERITAGE 500.00 - AA1-064 TAP | | | |
| | 500.00 | | | | |
| | OPEN BUS 918500 /* ISLAND: AA1 | 1-064 TAP 500.00 | | | |
| | END | | | | |
| Base Case | N/A | | | | |

15.2 Index 1

| ID | FROM BUS# | FROM BUS | FROM BUS AREA | TO BUS# | TO BUS | TO BUS AREA | CKT ID | CONT NAME | Туре | Rating MVA | PRE PROJECT LOADING % | POST PROJECT LOADING % | AC DC | MW IMPACT |
|----|--------------|-------------|---------------------|------------|-----------------|----------------|--------|-----------------------------|-------|---------------|--------------------------------|---------------------------------|-------|--------------|
| 1 | 314702 | 3KERR | DVP | 304102 | 3GW KING TAP | CPLE | 1 | DVP_P7- 1: LN 22-90-A | tower | 199.0 | 112.57 | 115.23 | AC | 6.41 |

| Bus # | Bus | MW Impact | | |
|--------|--------------|-----------|--|--|
| 315158 | 1KERR 1 | 0.8 | | |
| 315159 | 1KERR 2 | 3.27 | | |
| 315160 | 1KERR 3 | 3.22 | | |
| 315161 | 1KERR 4 | 3.22 | | |
| 315162 | 1KERR 5 | 3.22 | | |
| 315163 | 1KERR 6 | 3.22 | | |
| 315164 | 1KERR 7 | 3.22 | | |
| 936261 | AD2-033 C | 12.6 | | |
| 936262 | AD2-033 E | 8.4 | | |
| 936361 | AD2-046 C O1 | 17.92 | | |
| 936362 | AD2-046 E O1 | 8.24 | | |
| 936481 | AD2-063 C O1 | 16.08 | | |
| 936482 | AD2-063 E O1 | 10.72 | | |
| 938371 | AE1-056 C | 4.14 | | |
| 938372 | AE1-056 E | 2.26 | | |
| 939181 | AE1-148 C O1 | 17.24 | | |
| 939182 | AE1-148 E O1 | 11.49 | | |
| LTF | BLUEG | 1.95 | | |
| LTF | CALDERWOOD | 0.42 | | |
| LTF | CANNELTON | 0.13 | | |
| LTF | CATAWBA | 0.42 | | |
| LTF | CBM-N | 0.01 | | |
| LTF | СНЕОАН | 0.39 | | |
| LTF | COFFEEN | 0.23 | | |
| LTF | COTTONWOOD | 1.38 | | |
| LTF | DUCKCREEK | 0.47 | | |
| LTF | EDWARDS | 0.21 | | |
| LTF | FARMERCITY | 0.17 | | |
| LTF | G-007A | 0.11 | | |
| LTF | GIBSON | 0.08 | | |
| LTF | HAMLET | 0.81 | | |

| Bus # | Bus | MW Impact | | |
|--------|--------------|-----------|--|--|
| LTF | NEWTON | 0.6 | | |
| LTF | NYISO | 0.05 | | |
| LTF | PRAIRIE | 1.26 | | |
| LTF | SMITHLAND | 0.11 | | |
| LTF | TATANKA | 0.28 | | |
| LTF | TILTON | 0.25 | | |
| LTF | TRIMBLE | 0.21 | | |
| LTF | TVA | 1.16 | | |
| LTF | UNIONPOWER | 0.58 | | |
| LTF | VFT | 0.28 | | |
| 924021 | AB2-043 C O1 | 0.65 | | |
| 924022 | AB2-043 E O1 | 6.02 | | |
| 924161 | AB2-060 C O1 | 1.84 | | |
| 924162 | AB2-060 E O1 | 4.91 | | |
| 924301 | AB2-077 C O1 | 0.42 | | |
| 924302 | AB2-077 E O1 | 1.58 | | |
| 924311 | AB2-078 C O1 | 0.42 | | |
| 924312 | AB2-078 E O1 | 1.58 | | |
| 924321 | AB2-079 C O1 | 0.42 | | |
| 924322 | AB2-079 E O1 | 1.58 | | |
| 925611 | AC1-036 C | 0.15 | | |
| 925612 | AC1-036 E | 1.43 | | |
| 925781 | AC1-054 C O1 | 15.6 | | |
| 925782 | AC1-054 E O1 | 7.19 | | |
| 926271 | AC1-105 C O1 | 2.87 | | |
| 926272 | AC1-105 E O1 | 1.43 | | |

Affected Systems

16 Affected Systems

16.1 Duke Energy Progress

Potential constraints were identified by PJM on the following Dominion – Duke Energy/Progress (DEP) tie lines. Duke/Progress Energy portion of this line will need to be studied under Duke's FERC tariff process.

The following facilities were identified in this report:

• Henderson-Kerr Dam 115 kV line

Short Circuit

17 Short Circuit

The following Breakers are overduty

None

Stability Analysis

18 Stability Analysis

18.1 Executive Summary

Generator Interconnection Request AE1-056 is for a 60 MW Maximum Facility Output (MFO) solar generation plant. AE1-056 consists of 28 x 2.163 MW SMA Sunny Central 2500-US 2.5 MVA solar inverters. The Point of Interconnection (POI) is a tap to be built on Red House DP to South Creek 115 kV circuit in the Dominion Virginia Power (DVP) transmission system, Appomattox County, Virginia.

This report describes a dynamic simulation analysis of AE1-056 as part of the overall system impact study.

The load flow scenario for the analysis was based on the RTEP 2022 peak load case, modified to include applicable queue projects. AE1-056 has been dispatched online at maximum power output, with 1.0 p.u. voltage at the generator bus.

AE1-056 was tested for compliance with NERC, PJM, Transmission Owner and other applicable criteria. Steady-state condition and 23 contingencies were studied, each with a 20 second simulation time period. Studied faults included:

- a) Steady state operation (30 second);
- b) Three phase faults with normal clearing time;
- c) Single phase faults with stuck breaker;
- d) Single-phase faults placed at 80% of the line with delayed (Zone 2) clearing at line end remote from the fault due to primary communications/relay failure;

No relevant bus fault, multiple-circuit tower line faults and high-speed reclosing (HSR) contingencies were identified for this study.

For all simulations, the queue project under study along with the rest of the PJM system were required to maintain synchronism and with all states returning to an acceptable new condition following the disturbance.

For all of the fault contingencies tested on the 2022 peak load case:

- a) AE1-056 was able to ride through the faults (except for faults where protective action trips a generator(s)),
- b) The system with AE1-056 included is transiently stable and post-contingency oscillations were positively damped with a damping margin of at least 3% for interarea modes and 4% for local modes.
- c) Following fault clearing, all bus voltages recovered to a minimum of 0.7 per unit after 2.5 seconds (except where protective action isolates that bus).
- d) No transmission element tripped, other than those either directly connected or designed to trip as a consequence of that fault.

Based on the Impact Study data provided, the reactive power capability of AE1-056 meets the 0.95 lagging and leading PF requirement at the high side of the main transformer.

Fictitious frequency response at AE1-056 POI tripped the Queue Project due to under-frequency during P1 fault application at Pamplin 115 kV Substation (P1.04 – P1.08). After the frequency protection was disabled at AE1-056 the tripping issues were resolved.

The initial results showed inadequate voltage recovery at AE1-056 POI, South Creek, Red House, and Pamplin 115 kV for contingencies P4.10 and P4.11. It was found that this was due to AE1-056 utilizing Q control rather than voltage control. Changing the control mode to voltage control resolved the voltage recovery issues.

With control mode changed to V control, a slower post fault reactive power recovery was observed for all contingencies. This does not affect the stability of the system and can be mitigated with further model tuning if required.

No mitigations were found to be required.

Attachment 1

System Configuration

